

BOARD MEETING DATE: September 7, 2007

AGENDA NO. 39

PROPOSAL: Annual Status Report on Rule 1113 – Architectural Coatings

SYNOPSIS: This final annual report for Rule 1113 describes program achievements with respect to the Workplan Objectives established by the Board in 1999. Rule-compliant architectural coatings are available in the marketplace and continue to demonstrate quality performance. Findings of the technology assessment for the Flat coatings category limit, whose future compliance date is July 1, 2008, are discussed.

COMMITTEE: Stationary Source, July 27, 2007

RECOMMENDED ACTION:  
Receive and file.

Barry R. Wallerstein, D.Env.  
Executive Officer

EC:LT:LL:DB:HF

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### **Background**

Architectural coatings are the single largest source category of volatile organic compound (VOC) emissions under the regulatory authority of the South Coast Air Quality Management District (AQMD) and one of the largest non-mobile source of VOC emissions in the South Coast Air Basin (Basin). The VOC emissions from architectural coatings are a significant source of ozone formation in the Basin and continue to be a critical component for attainment of Federal and State standards. In 1997, architectural coatings were responsible for 50.9 tons of VOC emissions per day in the Basin on an annual average basis. Although the population has grown, as has the usage of architectural coatings, the 2005 annual average emissions were 38.8 tons per day, and are forecast to be reduced to 23.1 tons per day by the year 2010 according to the 2007 Air Quality Management Plan (AQMP). Through the

regulatory limits adopted in Rule 1113, the AQMD has made great strides in reducing emissions from architectural coatings, thereby decreasing ground level ozone formation and improving the overall quality of the air and the health of the greater than 16 million people residing in the AQMD.

To assist with the implementation of Rule 1113 – Architectural Coatings, the Board approved a Workplan on August 13, 1999 that required submittal of annual status reports through the year 2007, to provide the Board with a summary of technical assessments, new developments in coatings technology, market trends and outreach and training programs. The first report, submitted on July 21, 2000, has been followed each year by new information on the implementation of future VOC limits, the averaging compliance option, and other related programs. In addition to rule requirements for technology assessments of specific coating categories, a Board approved resolution in December 2002, ensured the continuance of annual reports with a focus on the progress towards achieving the 2006 VOC limits found in the rule. This is the seventh and final such report that staff will have presented to the Board.

The main focus of this final annual report, provided in Attachment B, is to furnish the latest information on the availability and performance of Flat coatings which are subject to a future compliance limit of 50g/l on July 1, 2008. The results of surveys, internet data searches, laboratory testing and evaluation of coatings, in-situ coating performance reviews and available compliance options built into the rule are some of the topics covered in this report.

### **Flat Coating Technology Assessment**

Staff relied on a number of key sources of data and information for determining the availability and performance of Flat coatings formulated to meet the future VOC limit of 50g/l. These include:

- 1. Flat Coating Laboratory Performance Study.** Staff has contracted with industry experts to conduct laboratory studies to assess the performance characteristics of Flat coatings to determine whether key characteristics are compromised when formulated to comply with the future VOC limit of 50g/l. A review of these studies supports staff conclusions that overall, future-compliant and even super-compliant coatings meet or exceed expected characteristic performance standards when compared to products that have a much higher VOC content.

On the whole, results of the recent architectural coatings laboratory-based evaluation by the University of Missouri at Rolla, continues to support staff's conclusions. Commercially available interior and exterior Flat coatings that meet the 2008 VOC limit of 50g/l have performance characteristics that are similar to and in many cases better than their

higher-VOC counterparts. The results of the findings are summarized in the report with the empirical data and are available for review in Appendix B.

- 2. Compliant Products Found in Internet Searches.** Staff continues to search for and find future compliant and super-compliant Flat coatings listed by large and small manufacturers on their websites. Staff verifies product characteristics by examining Technical Data Sheets and Material Safety Data Sheets for each coating listed, as well as discussing the performance capabilities with manufacturers. (See Appendix A.)
- 3. Store Shelf Survey.** Staff conducted a survey of local store inventories in the first quarter of 2007. The primary purpose of the survey was to obtain a snapshot of the currently available architectural products being sold at various points of distribution. A secondary benefit of the survey was to alert store owners to the future rule requirements. This limited survey indicates that products meeting the current and future VOC limit are currently available and being sold to consumers in all categories, including Flat coatings.
- 4. Meetings with Local Manufacturers (Large and Small).** Staff continues to visit local paint manufacturers individually to inquire about their successes and any failures in formulating Flat coatings to meet the July 2008 VOC limit of 50g/l. Manufacturers indicate that compliant products are available and that they exhibit acceptable performance characteristics for their markets.
- 5. Further Studies.** Additional studies include staff's documentation of low-VOC flat coating projects at a local university, addition of more flat coatings to the list of manufacturers producing super-compliant coatings, and research of articles on new technologies in low-VOC coatings.

#### **Additional Technical Programs and Studies**

- 1. Draft California Air Resources Board (CARB) 2005 Architectural Coatings Survey.** The most recent sales data provided by the coating manufacturers and included in the latest draft CARB survey, indicate an increase in the overall sales volume of lower-VOC products in many categories in comparison to the sales data from previous CARB surveys. The information contained in the most recent draft CARB survey represents sales data from 2004; this is four years prior to the lower-VOC limit for Flat coatings taking effect. This data demonstrates that manufacturers are developing and marketing coatings compliant with the future VOC limits in Rule 1113.

2. **CARB/AQMD Reactivity Study.** Staff will continue to monitor reactivity-related research and assess the reactivity and availability of solvents typically used in the formulation of architectural coatings
3. **Alternate Means of Compliance Provided by the Rule.** By examining the number of manufacturers who have taken advantage of alternate means of compliance allowed by Rule 1113, staff has concluded that these flexibilities in the rule have allowed manufacturers additional time for product reformulation. These alternate methods include the averaging compliance and sell-through options, as well as the small container exemption.
4. **Past Studies.** Staff also summarizes previous technology assessments conducted relative to coatings research and VOC limits within Rule 1113.
5. **Future Programs.** Staff will continue to research new technologies in the development of lower-VOC products and continue the strong working relationship with members of the coatings industry. Among the future plans are a Roundtable discussion on reactivity, an Architectural Coatings Technology Symposium, and a Clean Coating Certification Program.

### **Conclusions**

As detailed in this report, AQMD staff research of technical information from many coating manufacturers, coating performance studies, assessments of sales data, marketing brochures, Material Safety Data Sheets and other sources, clearly shows an ever-increasing number and volume of products that perform well and meet the future proposed limits.

### **Attachments**

- A. Key Contacts
- B. Annual Status Report on Rule 1113- Architectural Coatings

ATTACHMENT A

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KEY CONTACTS LIST

The following lists of key contacts are individuals that the AQMD has had direct contact with over the years. AQMD staff appreciates all of their help and assistance with the implementation of Rule 1113.

| <b><u>KEY CONTACTS LIST</u></b> |                                    |
|---------------------------------|------------------------------------|
| Kevin R. Merlo                  | Air Products Polymers              |
| Christine Stanley               | Ameron Protective Coatings Systems |
| John Woods                      | Ameron Protective Coatings Systems |
| Norm Mowrer                     | Ameron Protective Coatings Systems |
| Brian Turk                      | BASF                               |
| Kathy Allen                     | Bayer Material Science             |
| Michael Butler                  | BEHR Process Corporation           |
| Parker Pace                     | BEHR Process Corporation           |
| Kip Cleverly                    | Benjamin Moore Paints              |
| Ron Widner                      | Benjamin Moore Paints              |
| Gerald Thompson                 | BonaKemi USA, Inc.                 |
| Dane Jones, Ph.D.               | Cal Poly, SLO                      |
| Max Wills, Ph.D.                | Cal Poly, SLO                      |
| Andy Rogerson                   | Caltrans                           |
| Monique Davis                   | CARB                               |
| Jim Nyarady                     | CARB                               |
| Christian Hurley                | CARB                               |
| Barry Barman                    | CSI Services, Inc.                 |
| Bud Jenkins                     | CSU Pomona                         |
| Charles Milner Ph.D.            | CSU Pomona                         |
| Dennis St. Laurent              | CYTEC                              |
| Lloyd Haanstra                  | Deft Coatings                      |
| Randall J, Brady                | Deft Coatings                      |
| Marc N. Hiraoka                 | Disneyland Resort                  |
| Raymond Russell                 | Diversified Coatings, Inc.         |
| Robert Wendoll                  | Dunn-Edwards Paints                |
| Gil B. Mislant                  | Dunn-Edwards Paints                |
| Kevin McCreight                 | Eastman Chemical Company           |
| Ronald J. Regan                 | Eastman Chemical Company           |
| Joseph Tashjian                 | Ellis Paint Company                |
| Howard Berman                   | DUTKO Worldwide                    |
| Robert Henderson                | EPMAR                              |
| Dave/Adam Fuhr                  | Fuhr International                 |
| Richard Hart                    | Hart Polymers                      |
| Jim Kantola                     | ICI Dulux Sinclair                 |
| Jeffrey P. Mulford              | Lifeguard                          |

**KEY CONTACTS LIST, CONT'D**

|                               |                                       |
|-------------------------------|---------------------------------------|
| David Sibbrel                 | Life Paint Company                    |
| Daniel B. Pourreau, Ph.D      | Lyondell                              |
| Barry Law                     | Master Painters Institute®            |
| Bob Coleman                   | Merecole, Inc.                        |
| Tony Khalil                   | Monopole, Inc.                        |
| Stephen Murphy                | Murphy Industrial Coatings            |
| Carol Kaufman                 | MWD                                   |
| John Wallace                  | MWD                                   |
| David Darling                 | National Paint & Coatings Association |
| Tony Olson                    | NBC Universal                         |
| Dinkar Naik                   | Pacific Polymers                      |
| Michelle Richards             | Paramount Studios                     |
| Robert Gross                  | PPG Industries, Inc.                  |
| Claude Florent                | Rainguard                             |
| Aqua Mix                      | Real Bourdage                         |
| Brough Richey, Ph.D.          | Rohm and Hass Company                 |
| Clare Doyle                   | Rohm and Hass Company                 |
| William H. Hill               | Rohm and Hass Company                 |
| Madelyn Harding               | Sherwin-Williams Company              |
| Albert G. Silvertown          | Silvertown Products, inc.             |
| Darin A. Shields              | Specialty Polymers, Inc.              |
| Tony Hobbs                    | Tnemec Corporation                    |
| Kathryn Sandefur              | UMR Coatings Institute                |
| Michael R. Van De Mark, Ph.D. | UMR Coatings Institute                |
| Don Sudduth                   | UV Chemistry Company, Inc             |
| Duncan Gamble                 | UV Chemistry Company, Inc.            |
| Hamid Pourshirazi             | Vista Paint                           |
| Jerome Fischer                | Vista Paint                           |
| John Long                     | Vista Paint                           |

ATTACHMENT B

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ANNUAL STATUS REPORT ON RULE 1113 – ARCHITECTURAL COATINGS

SOUTH COAST AIR QUALITY MANAGEMENT DISTRICT

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**ANNUAL STATUS REPORT ON RULE 1113 – ARCHITECTURAL COATINGS**

Dated: September 7, 2007

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**SOUTH COAST AIR QUALITY MANAGEMENT AQMD**  
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Speaker of the Assembly Appointee

Vice Chair: S. ROY WILSON, Ed.D.  
Supervisor, Fourth District  
Riverside County Representative

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Los Angeles County Representative

BILL CAMPBELL  
Supervisor, Third District  
Orange County Representative

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GARY OVITT  
Supervisor, Fourth District  
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JAN PERRY  
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Cities Representative, Los Angeles County, Western Region

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Councilmember, City of Long Beach  
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DENNIS YATES  
Mayor, City of Chino  
Cities Representative, San Bernardino County

**EXECUTIVE OFFICER**

BARRY R. WALLERSTEIN, D.Env.

## ACKNOWLEDGEMENT

AQMD staff would like to recognize the contributions of and thank the past and current Rule 1113 Technical Advisory Committee (TAC) members for the valuable input and guidance they provided in designing and executing past technology assessments. Staff would especially like to recognize posthumously, former TAC member Dr. John A. Gordon, for his dedication, wealth of knowledge and integrity. Dr. Gordon was instrumental in introducing the concept of forming a committee comprised of members of industry, academia, and AQMD staff which became the TAC. Staff is looking forward to continuing the productive working relationship with the TAC in the future, including relying on NPCA to facilitate participation in the upcoming AQMD Architectural Coatings Technology Symposium.

Current Technical Advisory Committee Members:

|                      |                                       |
|----------------------|---------------------------------------|
| Barry Barman         | CSI Services, Inc.                    |
| Charles Milner Ph.D. | CSU Pomona                            |
| Christian Hurley     | CARB                                  |
| David Darling        | National Paint & Coatings Association |
| Jim Nyarady          | CARB                                  |
| Madelyn Harding      | Sherwin-Williams Company              |
| Raymond Russell      | Diversified Coatings, Inc.            |
| Robert Henderson     | EPMAR                                 |
| Robert Wendoll       | Dunn-Edwards Paints                   |
| Stephen Murphy       | Murphy Industrial Coatings            |
| Bud Jenkins          | CSU Pomona                            |
| David/Adam Fuhr      | Fuhr International                    |

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## PURPOSE OF THIS REPORT

This report is the final annual progress report required in accordance with the 1999 Board approved Workplan for Implementation of Rule 1113 – Architectural Coatings. The report includes the findings of the required technology assessment for the Flat coatings category, future activities to encourage technology advancements by coating manufacturers and actions to enhance on-shelf and in-use compliance with the rule. This report also includes the following:

- Information on the increasing number of compliant and super-compliant products already available in the market;
- A detailed report including empirical data for the most recent laboratory study;
- Progress on the reactivity and availability assessment of solvents found in architectural coatings, and
- Conclusions to be drawn from the technology assessment.

As part of the Flat coating technology assessment, the South Coast Air Quality Management District (AQMD) contracted with the University of Missouri – Rolla Coatings Institute (UMR) to conduct the most recent laboratory study. This report includes the results of the completed testing, staff conclusions and recommendations.

## BACKGROUND

Architectural coatings are the single largest source category of volatile organic compound (VOC) emissions under the regulatory authority of the AQMD and one of the largest non-mobile source of VOC emissions in the South Coast Air Basin (Basin). The VOC emissions from architectural coatings are a significant source of ozone formation in the Basin and continue to be a critical component for attainment of Federal and State standards. In 1997, architectural coatings were responsible for 50.9 tons of VOC emissions per day in the Basin. Although the population has grown, as has the usage of architectural coatings, the 2005 annual average emissions were 38.8 tons per day, and the emissions are forecast to be reduced to 23.1 tons per day by the year 2010 according to the 2007 Air Quality Management Plan (AQMP). Through the regulatory limits adopted in Rule 1113, the AQMD has made great strides in reducing emissions from architectural coatings, thereby decreasing ground level ozone formation and improving the overall quality of the air and the health of the greater than 16 million people residing in the AQMD.

To assist with the implementation of Rule 1113 – Architectural Coatings, the Board approved a Workplan on August 13, 1999 that required submittal of annual status reports through the year 2007 summarizing technical assessments, new developments in coatings technology, market trends and outreach and training programs. The first report, submitted on July 21, 2000, has been followed each year by new information on the implementation of future VOC limits in the rule. In addition to rule requirements for technology assessments of specific coating categories, a Board approved resolution in December of 2002, ensured the continuance of annual reports with a focus on the

progress towards achieving the 2006 VOC limits found in the rule. This is the seventh and final such report that staff will have presented to the Board.

The focus of this annual report is to provide the latest information on the availability and performance of Flat coatings which are subject to a future compliance limit of 50g/l on July 1, 2008. The results of surveys, internet data searches, laboratory testing and evaluation of coatings, in-situ coating performance and available compliance options built into the rule are some of the topics covered in this report. The information contained in this report also includes the following:

- Technical information from Technical Data Sheets (TDS), Material Safety Data Sheets (MSDS), and technical papers that demonstrate that Flat coatings meeting the future VOC limits are in use and available to all consumers.
- Product surveys and laboratory test results that show an increase in availability of quality compliant and super-compliant coatings meeting the 2008 VOC limit for Flat coatings.
- Information gathered from meetings with manufacturers with respect to their preparation for making compliant flat coatings.

## **TECHNICAL COMMITTEES**

To assist with the assessments included in this annual report, AQMD staff relies upon technical expertise and valuable feedback on all aspects of architectural coatings from a Technical Advisory Committee (TAC). The TAC was first formed in February 1998 to provide technical oversight of the Phase II Assessment Study and future technology assessments, including selection of coatings, relevant testing, and the report formats. The current makeup of the TAC includes representatives of several large and small manufacturing companies, the California Air Resources Board (CARB), the National Paint and Coatings Association (NPCA), a consulting and engineering firm, a painting contractor and several members from academia. This past year, the TAC assisted staff designing and implementing the laboratory performance study for flat coatings and in developing a performance ranking system for the Flat coating technology assessment based on discussions and recommendations from the ad hoc committee for architectural coatings.

In addition to the TAC, in early 2005, at the request of Governing Board Chairman William Burke, an ad hoc committee was formed for the purpose of providing an open forum to discuss key regulatory issues relative to the coatings industry. This committee is made up of AQMD Board Members Michael Antonovich and Jan Perry, AQMD Management representatives Dr. Barry Wallerstein and Dr. Laki Tisopulos, and industry representatives Christine Stanley of Ameron and Ron Widner of Benjamin Moore. Steve Sanchez of U.S. Can Company is an industry alternate. One key recommendation of this committee was for staff to work closely with the TAC to develop the performance ranking and scoring system as a basis for judging the quality of coatings with respect to key performance characteristics.

## **FLAT COATING TECHNOLOGY ASSESSMENT**

### **A. Flat Coating Laboratory Performance Study**

The requirements under Rule 1113 state that a technology assessment for Flat coatings shall be completed prior to July 1, 2007. In February 2007, the AQMD contracted with University of Missouri - Rolla Coatings Institute (UMR) to conduct laboratory tests on recently developed and commercially available Flat coatings.

The results of this most recent architectural coatings laboratory evaluation have shown that the 2008 VOC limit of 50g/l for Flat coatings is technically feasible and that many already commercially available compliant products have performance characteristics that are similar to and in many cases better than their higher-VOC counterparts. The findings are summarized on the following pages, with the empirical data available for review in Appendix B of this report.

The flat coatings included in the UMR study were selected and approved by the TAC and AQMD staff. A total of twenty Flat coatings were tested; eight of the coatings selected have a VOC content greater than 50g/l but less than or equal to 100g/l. The remaining twelve coatings have a VOC content meeting our future limit of less than or equal to 50g/l. The coatings were separated into the following categories: seven interior, seven exterior and two interior/exterior coatings and tested for a range of properties and then ranked according to the test results. The coatings that were tested are not coatings that are solely available in the AQMD. Depending on the manufacturer, some are marketed and sold throughout California if not throughout the country. The following pages summarize the UMR testing results.

Included with this study are the results of the weighting and rating system developed by the TAC as a result of the ad hoc committee discussions. The rating was designed to be a numerical representation of how well the coating performed for each individual test. The weighting factor was designed to assign the importance of each test relative to industry expectations for the different characteristics of Flat coatings. The concept of this rating and weighting system is to condense the results of the performance test of each coating to a single number. This then allows for a direct comparison on the overall performance of the coatings. Table 1 shows the system that was developed.

**Table 1**  
Weighting System for Flat Coating Laboratory Performance Study

| Property                                   | Standard Test           | Weighting Factor (1-10) <sup>1</sup> |
|--|-------------------------|--------------------------------------|
| <b>Interior and Exterior</b>               |                         |                                      |
| VOC Content                                | Method 24 & ASTM D 6886 | Pass/Fail                            |
| Gloss at 60° & 85°                         | ASTM D523               | Pass/Fail                            |
| Stability - Viscosity Change               | ASTM D1849              | 8                                    |
| Stability - Overall Character <sup>1</sup> | ASTM D1849              | 8                                    |
| Stability -pigment / colorant float        | Industry Protocol       | 8                                    |
| Open Time / Wet Edge                       | Industry Protocol       | 9                                    |
| Freeze/thaw resistance                     | ASTM D2243              | 5                                    |
| Flow & Leveling                            | ASTM D4062              | N/A                                  |
| Sag Resistance                             | ASTM D 4400             | N/A                                  |
| Dry Time                                   | ASTM D5895              | N/A                                  |
| Hide                                       | Spectrophotometer       | 10                                   |
| Adhesion                                   | ASTM D3359              | 10                                   |
| <b>Interior Only</b>                       |                         |                                      |
| Scrub Resistance                           | ASTM D2486              | 8                                    |
| Stain Resistance <sup>2</sup>              | ASTM D4828              | 8                                    |
| Touch up                                   | ASTM D3928              | 9                                    |
| <b>Exterior Only</b>                       |                         |                                      |
| Tannin Stain Blocking                      | ASTM D6686              | 6                                    |
| Alkalinity Resistance                      | Industry Protocol       | 7                                    |

N/A = not applicable

1. Skinning, pressure, corrosion of the container, and odor of spoilage.
2. Modified to reflect common materials to architectural coatings.

### Performance Summary

One of the coatings selected to be included in this study, Coating E, tested outside of the AQMD definition of a Flat coating even though it was listed by The Masters Painters Institute™ (MPI) at a gloss level 1, which is stricter than the Rule 1113 definition of a Flat coating. This coating has been re-categorized by MPI since our coating selection began and is in a category consistent with the gloss level tested at UMR. All of the following calculations, tables and charts exclude this coating.

### ***Stability***

The stability of the coatings was analyzed by ASTM D 1849, in this test the coatings are held at an elevated temperature for 30 days. Two different parameters are evaluated, the change in viscosity and the overall character rating which is a measure of the separation, can corrosion, skinning, and odor. Both of these parameters were assigned an 8 on the weighting scale indicating equal importance. While the overall character average for the  $\leq 50\text{g/l}$  coatings was lower than the  $\leq 100\text{g/l}$  coatings (7.3 to 5.8), the viscosity change was just the opposite with the average of the  $\leq 50\text{g/l}$  coatings outperforming the  $\leq 100\text{g/l}$  coatings (7.0 to 4.0). The four lowest rated coatings for viscosity change are the  $\leq 100\text{g/l}$  coatings, leading AQMD staff to conclude that the stability of the coatings is independent of the VOC level.

Further, the differences in the overall character ratings for the coatings were primarily due to in-can settling. Upon stirring the coatings, they were restored to an acceptable homogeneous state.

*Staff conclusion: Overall character average rating was lower for the low-VOC coatings tested; however, they were restored to an acceptable level after stirring. Average viscosity change showed low-VOC coatings outperforming higher-VOC coatings.*

### ***Pigment Float***

The pigment float test also measures stability, in this test the coatings are held at an elevated temperature for 10 days and then the separation and settling of the pigment is measured. Pigment float was assigned an 8 on the weighting scale. The testing that was conducted by UMR showed no discernable difference between any of the coatings in regard to pigment float.

*Staff conclusion: All coatings performed well.*

### ***Open Time/Wet Edge***

The open time or wet edge test measures the time in which a coating remains in a fluid state such that a brush can go over the surface without leaving brush marks. This is an important characteristic for the application of coatings. In the past, this characteristic was commonly cited as problematic for low-VOC coatings. Open time/wet edge was assigned a 9 on the weighting scale. The UMR testing revealed that although four of the  $\leq 50\text{g/l}$  coatings ranked lower compared to the other coatings tested, all of the coatings actually performed quite well. The testing was conducted in a laboratory setting under ambient conditions which do not represent the more extreme conditions that at times exist in the Basin. The ranking system that the TAC developed was based on a 0 to 10 scale for open time from 0 to 10 minutes. Three of the coatings scored an 8 and one coating scored a 9 with the remaining being at 10 or 10+ for greater than ten minutes of open time. All but two of the coatings that scored less than a 10 were coatings that AQMD staff would define as super-compliant coatings because they have a VOC content of

≤10g/l. One of the super-compliant coatings tested (Coating N) scored a 10+ proving that even a coating with virtually zero-VOCs can have an open time equal to or better than a higher-VOC coating.

*Staff conclusion: Although all coatings performed well, some of the super-compliant coatings scored slightly lower than their higher-VOC counterparts.*

### ***Freeze/Thaw***

The freeze/thaw test measures how many times a coating can endure a freeze/thaw cycle and still remain a viable coating. This is a parameter that tends to be inferior for low and ultra low-VOC coatings. Fortunately due to the favorable and mild climatic conditions, freeze/thaw is not a major issue in the Basin; however, it was deemed important enough by several TAC members that it was included in the laboratory performance study. Manufacturers cite freeze/thaw as an issue when shipping coatings in or out of the Basin and also wanted the test to be included because other air quality agencies look to the AQMD technology assessments in establishing their VOC limits. Freeze/thaw was assigned a 5 on the weighting scale. The statistical evaluation that follows this discussion contains data both with and without the freeze/thaw results included.

In this technology assessment, the interior coatings at ≤100g/l performed almost as poorly as the ≤50g/l coatings with only one of the higher-VOC coatings passing a single freeze/thaw cycle. The higher-VOC exterior coatings performed considerably better with only one of the ≤100g/l unable to pass even a single freeze/thaw cycle while the other three passed all 5 cycles. However, the UMR tests also indicated that two of the ≤50g/l scored quite well, with Coating H passing four of the five cycles and Coating I passing all five of the cycles. This is evidence that formulators have made progress in addressing freeze/thaw issues in Flat coatings with a VOC of ≤50g/l.

*Staff conclusion: 75% of low-VOC coatings failed after 1st cycle; however, 1 of the low-VOC coatings passed 4 cycles and 1 passed all 5 cycles.*

### *Adhesion*

The adhesion test measures how well a coating will stick to a substrate and was assigned a 10 on the weighting scale. The substrate used to test the exterior coatings was glass and the substrate used to test the interior coatings was a Leneta test chart, which are sealed paper charts used to test coatings in laboratory settings. Three out of the seven  $\leq 50\text{g/l}$  interior and interior/exterior coatings tested on Leneta charts exhibited poor adhesion, in that there was adhesion failure not substrate failure on the cross hatch adhesion test. The remaining four low-VOC coatings performed comparably to the  $\leq 100\text{g/l}$  coatings, including Coating N which is a super-compliant coating with a VOC content measured at only  $3\text{g/l}$ .

Based on discussions with the TAC and UMR after the testing was completed, the Leneta cards may not have been the best substrate for testing the adhesion of interior coatings. Most of the coatings experienced substrate failure; the paint adhered to the Leneta card but the top layer of the Leneta card was removed during the test. This is a substrate failure and not a coating failure but it makes distinguishing adhesion differences between those coatings impracticable.

*Staff conclusion: Only 3 out of 7 low-VOC coatings showed adhesion failure, others performed comparably.*

### *Scrub Resistance*

The scrub test measures how many times a brush can cycle back and forth over a coating before the paint film is removed. This test is designed to mimic the erosion that occurs when walls are washed or scrubbed. This coating characteristic was only tested on the interior coatings where the TAC committee concluded it is more critical; it was assigned an 8 on the weighing scale. The repeatability and reproducibility of this test is fairly high for an ASTM test method (30 and 50%, respectively) and the differences in replicate test panels for this test were at times significant. Coating M at  $\leq 100\text{g/l}$  performed far superior to the rest of the Flat coatings tested for scrub resistance. It surpassed 2106 scrub cycles, almost twice as many as the next best performer. The next best performer was Coating T, one of the  $\leq 50\text{g/l}$  coatings, and it lasted for 1231 scrub cycles. Further, several of the super-compliant coatings performed quite well with a scrub resistance at the median of the test results, around 900 scrub cycles. From these results it is clear that low-VOC coatings can be formulated to have good scrub resistance.

*Staff conclusion: The best score was one of the higher-VOC coatings with the next best being a low-VOC coating. Several of the super-compliant coatings performed at the median of the test results, around 900 scrub cycles.*

### *Alkalinity Resistance*

Concrete masonry surfaces are naturally alkaline which can lead to color change. The alkalinity resistance test measures how well a coating will withstand this alkaline environment such as fresh concrete, stucco or other masonry and is an important characteristic for coatings designed to be applied to those substrates. Not all exterior coatings are specified for application to masonry; hence not all are designed to be resistant to an alkaline environment. Alkalinity resistance was assigned a 7 on the weighting scale.

This test is extremely aggressive in that the coatings are not given time to fully cure and form a film before being immersed in water and exposed to UV. There is no ASTM test method, so the test method was provided by Dunn Edwards along with the necessary panels and pigment additives for the testing. Although there is no repeatability or reproducibility data for this test, the members of the TAC came to a consensus that it is an appropriate method to measure alkalinity resistance. For this test, fresh concrete panels were painted with coatings that contain two different pigment packages; one that is alkali-resistant and one that is alkali-sensitive. The panels are initially pink and then change to yellow if the coatings are unable to withstand the alkalinity. The result of this test was that all of the coatings experienced a severe color change to yellow, either entirely or in splotches. In evaluating the results, the different degree of failure is being rated.

This test is essentially evaluating the ability of the coatings to stabilize the pigments that were used. An additional variable to this test is the ability of each coating to stabilize the particular pigment independent of the alkalinity. The change in color of the coatings does not necessarily indicate film failure. A more accurate measurement of coating failure would be loss of adhesion resulting from the alkaline environment.

Of all of the coatings, two of the  $\leq 100\text{g/l}$  and one of the  $\leq 50\text{g/l}$  coatings performed moderately better than the rest based on the visual rating conducted by UMR. According to the TDS, these three coatings are the only ones in this study that were specifically designed for masonry tilt-up construction. Additionally, the remaining coatings all list properly prepared concrete, masonry and stucco on their TDS as recommended uses, but they do not recommend and were not formulated to withstand the demanding alkaline environment of freshly poured concrete. Further, all of the coatings tested specify an alkaline resistant primer when the coatings are to be applied to concrete and masonry, including the coatings that had relatively lower delta E readings. However, under the Dunn Edwards test method, no primers were used. In addition, as stated earlier, the coatings were not fully cured as recommended by the manufacturer. Thus, this test has limitations and does not represent recommended painting practices.

The two worst performers were the dual-use interior/exterior low-VOC coatings. These two coatings tended to perform worse than the coatings that were specifically designed for exterior exposures, but performed quite well compared to the coatings designed for interior applications.

*Staff conclusion: All coatings failed this stringent test. This test does not follow recommended painting practices and only a few of the tested coatings were specifically designed to withstand an alkaline environment. Coating manufacturers specify an alkaline resistant primer which was not used in the testing.*

### ***Tannin Blocking***

The tannin blocking test measures the ability of a coating to resist tannin bleed-through from the wood. This is an important characteristic for coatings applied to wood and was assigned a 6 on the weighting scale. On average the  $\leq 50\text{g/l}$  coatings performed twice as well on Tannin Blocking than their higher-VOC counterparts. Tannin Blocking was given a rating of 6 by the TAC committee making it a characteristic considered almost as important as alkalinity resistance (weighted as 7). The top three performers for this coating characteristic were the  $\leq 50\text{g/l}$  coatings.

*Staff conclusion: Low-VOC coatings outperformed the higher-VOC coatings.*

### **Statistical Analysis**

The following tables show how each coating was rated and then the final result once the weighting factors were applied. Table 2 contains the results of the exterior coatings and Table 3 contains the results of the interior coatings. Both tables contain the two interior/exterior coatings. The totals at the bottom were calculated with and without the freeze/thaw results because AQMD staff does not consider this to be an important characteristic in the Basin.

**Table 2**  
Exterior Flat Coating Performance Summary

| Property                             | Weighting Factor | Exterior ≤100g/L                          |            |            |            | Exterior ≤50g/L |            |            |            | Ext/Int ≤50g/L |            |
|--------------------------------------|------------------|---|------------|------------|------------|-----------------|------------|------------|------------|----------------|------------|
|                                      |                  | A   | B          | C          | D          | F               | G          | H          | I          | S              | T          |
| VOC Content                          | Pass/Fail        | 80  | 91         | 100        | 90         | 46              | 35         | 45         | 46         | 0              | 50         |
| Gloss 60°                            | Pass/Fail        | Pass                                      | Pass       | Pass       | Pass       | Pass            | Pass       | Pass       | Pass       | Pass           | Pass       |
| Sheen 85°                            | Pass/Fail        | Pass                                      | Pass       | Pass       | Pass       | Pass            | Pass       | Pass       | Pass       | Pass           | Pass       |
|                                      |                  | <b>Rating (0 - 10 from worst to best)</b> |            |            |            |                 |            |            |            |                |            |
| Stability - Viscosity Change         | 8                | 6   | 8          | 0          | 8          | 4               | 10         | 9          | 8          | 5              | 9          |
| Stability - Overall Character        | 8                | 8   | 6          | 8          | 8          | 8               | 6          | 6          | 6          | 6              | 4          |
| Colorant /Pigment Float              | 8                | 9   | 9          | 9          | 9          | 9               | 9          | 9          | 9          | 9              | 9          |
| Open Time/Wet Edge                   | 9                | 10  | 10         | 10         | 10         | 10              | 10         | 10         | 10         | 10             | 10         |
| Freeze/Thaw                          | 5                | 8   | 8          | 0          | 8          | 0               | 2          | 6          | 8          | 0              | 0          |
| Flow & Leveling <sup>1</sup>         | N/A              | 0   | 0          | 0          | 0          | 0               | 0          | 0          | 0          | 0              | 0          |
| Sag <sup>1</sup>                     | N/A              | 12  | 12         | 12         | 12         | 12              | 12         | 12         | 12         | 12             | 12         |
| Dry Time <sup>1</sup>                | N/A              |   |            |            |            |                 |            |            |            |                |            |
| Hide                                 | 10               | 6   | 6          | 6          | 6          | 8               | 4          | 6          | 6          | 6              | 4          |
| Adhesion                             | 10               | 3   | 4          | 2          | 4          | 2               | 2          | 4          | 4          | 2              | 3          |
| Tannin Stain Blocking                | 6                | 9   | 3          | 4          | 2          | 13              | 8          | 10         | 11         | 7              | 7          |
| Alkalinity Resistance                | 7                | 0   | 1          | 0          | 1          | 0               | 1          | 0          | 0          | 0              | 0          |
| Total                                |                  | 59  | 55         | 39         | 56         | 54              | 52         | 60         | 62         | 45             | 46         |
| <b>Adjusted for Weighting Factor</b> |                  | <b>458</b>                                | <b>439</b> | <b>330</b> | <b>449</b> | <b>436</b>      | <b>415</b> | <b>472</b> | <b>480</b> | <b>372</b>     | <b>378</b> |
| <i>Without Freeze/thaw</i>           |                  | 418                                       | 399        | 330        | 409        | 436             | 405        | 442        | 440        | 372            | 378        |
| <b>Maximum Possible Score: 678</b>   |                  |   |            |            |            |                 |            |            |            |                |            |

N/A = not applicable

1. Flow and leveling, sag and dry time were not included in the totals for the coatings performance.

**Table 3**  
Interior Flat Coating Performance Summary

| Property                                  | Weighting Factor | Interior ≤100g/L |            |            |            | Interior ≤50g/L |            |            |            | Ext/Int ≤50g/L |            |            |
|---|------------------|------------------|------------|------------|------------|-----------------|------------|------------|------------|----------------|------------|------------|
|   |                  | J                | K          | L          | M          | N               | O          | P          | Q          | R              | S          | T          |
| VOC Content                               | Pass/Fail        | 100              | 95         | 92         | 91         | 0               | <10        | <15        | 0          | 37             | 0          | 50         |
| Gloss 60°                                 | Pass/Fail        | Pass             | Pass       | Pass       | Pass       | Pass            | Pass       | Pass       | Pass       | Pass           | Pass       | Pass       |
| Sheen 85°                                 | Pass/Fail        | Pass             | Pass       | Pass       | Pass       | Pass            | Pass       | Pass       | Pass       | Pass           | Pass       | Pass       |
| <b>Rating (0 - 10 from worst to best)</b> |                  |                  |            |            |            |                 |            |            |            |                |            |            |
| Stability - Viscosity Change              | 8                | 1                | 0          | 0          | 9          | 9               | 7          | 8          | 7          | 1              | 5          | 9          |
| Stability - Overall Character             | 8                | 10               | 8          | 6          | 4          | 6               | 6          | 4          | 6          | 6              | 6          | 4          |
| Colorant/Pigment Float                    | 8                | 9                | 8          | 8          | 9          | 9               | 8          | 9          | 9          | 9              | 9          | 9          |
| Open Time / Wet Edge                      | 9                | 10               | 10         | 10         | 10         | 10              | 9          | 8          | 8          | 8              | 10         | 10         |
| Freeze/Thaw                               | 5                | 0                | 2          | 0          | 0          | 0               | 0          | 0          | 0          | 0              | 0          | 0          |
| Flow & Leveling <sup>1</sup>              | N/A              | 5                | 1          | 0          | 0          | 0               | 3          | 0          | 0          | 0              | 0          | 0          |
| Sag <sup>1</sup>                          | N/A              | 10               | 12         | 12         | 12         | 12              | 12         | 12         | 12         | 12             | 12         | 12         |
| Dry Time <sup>1</sup>                     | N/A              |                  |            |            |            |                 |            |            |            |                |            |            |
| Hide                                      | 10               | 8                | 6          | 6          | 6          | 8               | 6          | 6          | 6          | 8              | 6          | 4          |
| Adhesion                                  | 10               | 4                | 4          | 3          | 5          | 4               | 3          | 3          | 2          | 4              | 4          | 5          |
| Scrub Resistance                          | 8                | 6                | 4          | 3          | 10         | 3               | 3          | 4          | 4          | 3              | 1          | 6          |
| Stain Resistance                          | 8                | 7                | 6          | 5          | 6          | 6               | 6          | 5          | 5          | 5              | 3          | 4          |
| Touch up                                  | 9                | 10               | 10         | 10         | 10         | 10              | 10         | 10         | 10         | 10             | 10         | 10         |
| Total                                     |                  | 65               | 58         | 51         | 69         | 65              | 58         | 57         | 57         | 54             | 54         | 61         |
| <b>Adjusted for Weighting Factor</b>      |                  | <b>561</b>       | <b>496</b> | <b>448</b> | <b>592</b> | <b>562</b>      | <b>499</b> | <b>488</b> | <b>486</b> | <b>470</b>     | <b>474</b> | <b>526</b> |
| <i>Without Freeze/thaw</i>                |                  | <i>561</i>       | <i>486</i> | <i>448</i> | <i>592</i> | <i>562</i>      | <i>499</i> | <i>488</i> | <i>486</i> | <i>470</i>     | <i>474</i> | <i>526</i> |

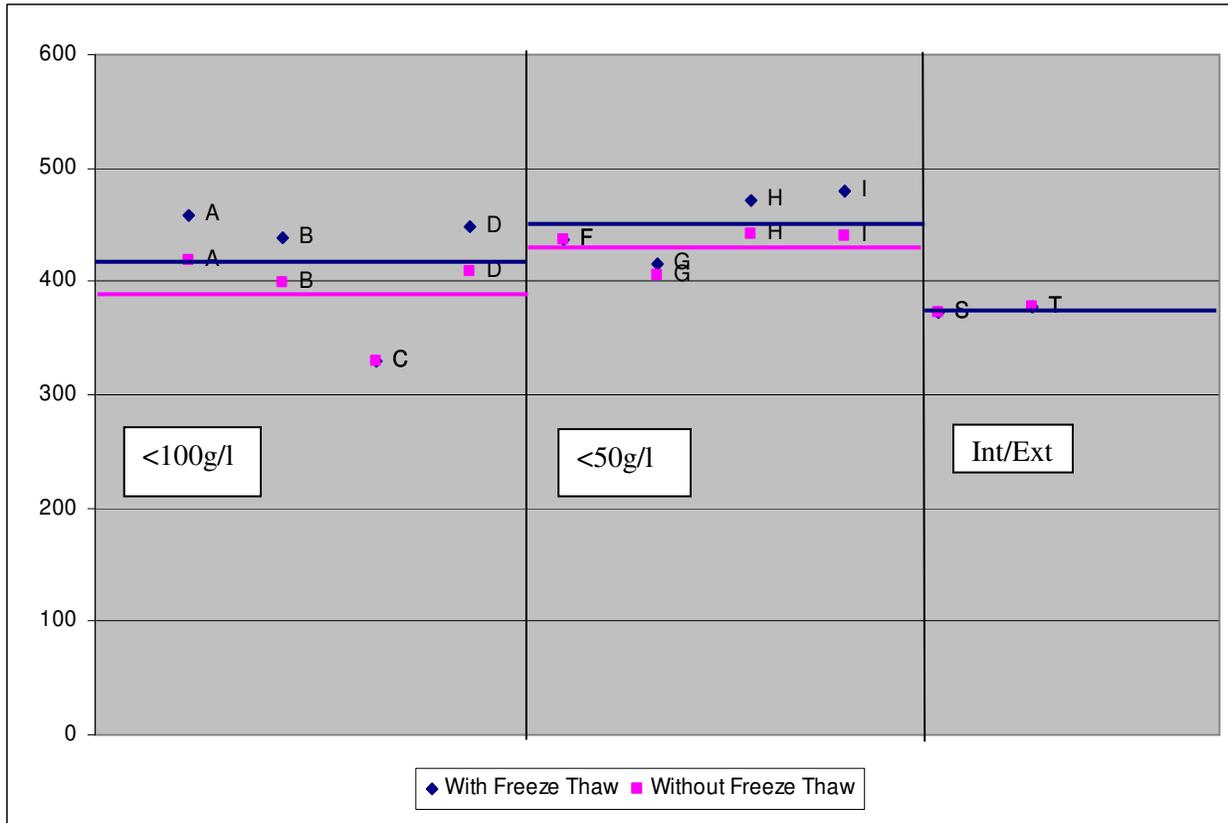
Maximum Possible Score: 780

N/A = not applicable

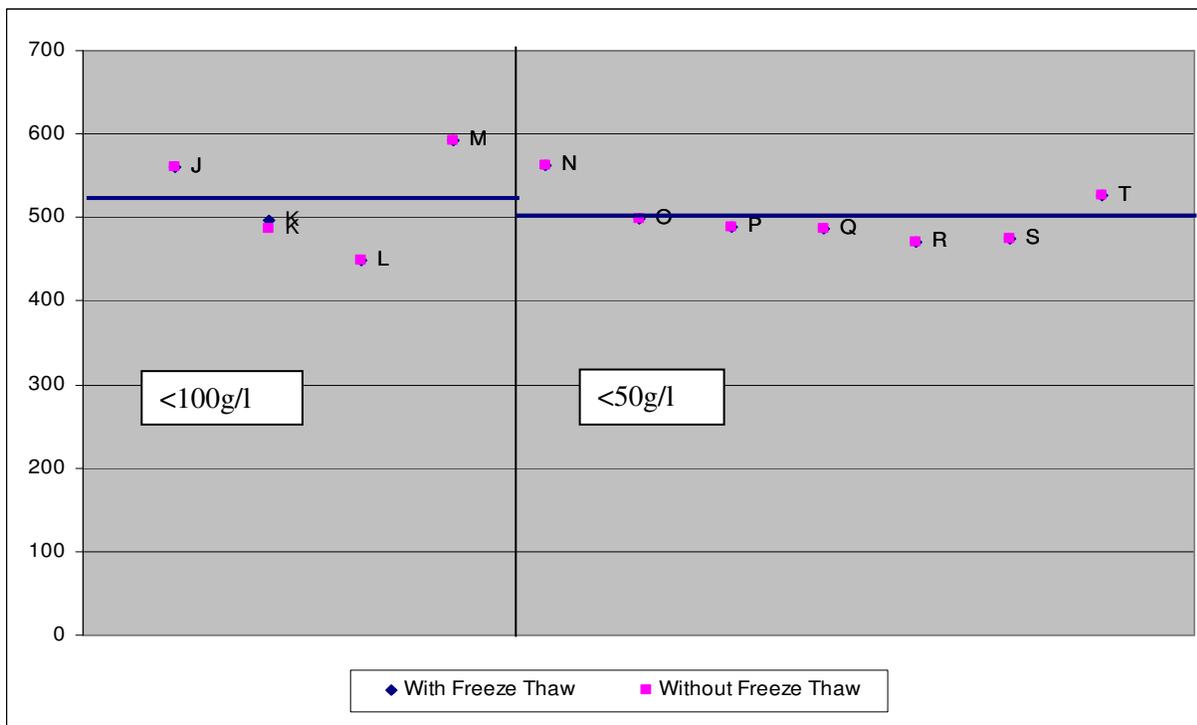
1. Flow and leveling, sag and dry time were not included in the totals for the coatings performance.

Graph 1 and 2 give a visual depiction of the final score, with and without freeze/thaw. The horizontal lines represent the average scores for each category; a separate average line was not included on the interior plot for the two interior/exterior coating because the average remained the same with or without the inclusion of those coatings.

**Graph 1**  
Scatter plot of Exterior Coatings



**Graph 2**  
Scatter plot of Interior Coatings



Comments

AQMD staff worked closely with TAC members prior to the start, during and following the completion of the UMR Flat coatings technological assessment. Several meetings were scheduled at the AQMD and many conference calls were conducted prior to and during the study, including extensive e-mail correspondence.

UMR's Project Manager, Dr. Michael R. Van de Mark, prepared a Draft Final report in June of 2007, which staff distributed to the TAC members for review and comment. Staff received only one comment letter dated July 18, 2007 from NPCA. In the letter, NPCA asserted that the test results for performance characteristics that included stability, open time, freeze/thaw, adhesion, scrub resistance and alkalinity resistance, demonstrated that the lower-VOC coatings did not perform as well as their higher-VOC counterparts and recommended revising the current VOC limits. NPCA also stated that Flat coatings formulated to meet the 50g/l limit are unique and may not perform adequately in other regions of California and the rest of the country.

AQMD staff has reviewed the comments from NPCA and strongly disagrees with NPCA's overall conclusions. A thorough evaluation of the performance testing results summarized in prior sections of this report indicates the comparable overall performance between low-VOC coatings and their higher-VOC counterparts. Moreover, the similarity in the overall performance between the two sets of coatings becomes even more evident if one utilizes the weighting and rating scale developed by the TAC. Based upon this empirical data, AQMD staff believes that the lower-VOC coatings perform equal to and in some instances better than their higher-VOC counterparts. Further, staff disagrees with the claim of NPCA regarding the coatings inability to perform outside of the Basin. The coatings tested are not solely available in the Basin. Depending on the manufacturer, some are marketed and sold throughout California and a few are sold throughout the country. However, relative to the freeze/thaw issue, AQMD staff recognizes that some areas outside of Southern California may have problems associated with this coating characteristic. As mentioned previously, a few of the low-VOC coatings did perform well in the freeze/thaw testing, demonstrating technology improvements relative to this coating characteristic. Regardless of the interpretation of the results however, the AQMD focuses its technology assessments on environmental conditions in the Basin and does not state that these conclusions necessarily apply to areas outside of the AQMD. Thus staff recommends maintaining the VOC limits adopted by the Board in the AQMD.

NPCA also commented in the letter that higher-VOC coatings are necessary for applications under ambient conditions of high heat and low humidity. This concern had been introduced during earlier meetings with the TAC, which AQMD staff attempted to address. A considerable effort went into developing a draft protocol and cost analysis including the hiring of a paint contractor, for performing a field study to evaluate the applicability of future compliant Flat coatings under non-ideal application conditions, such as, high heat accompanied by low humidity, representative of desert areas and low temperatures accompanied by high humidity typically found in coastal areas. However, the focus of the TAC was diverted to the laboratory performance study, and this study

was not pursued. AQMD staff has received feedback from a member of the TAC committee who has performed field application of ultra-low VOC flat coatings under hot dry conditions. There was no report of application problems under these conditions. Details on this project can be found in section E. Cal. Poly Pomona's House Painting Project. Further, AQMD staff supports the results of the laboratory studies as a reliable reflection of performance of the coatings in the field. In addition, staff supports testing coatings according to the manufacturers' recommendations, and not under extreme conditions.

As discussed earlier in this report, AQMD staff continues to evaluate field applied applications of low-VOC coatings that include flats in all areas of the Basin and have not encountered any negative application comments to date. Staff is committed to a continued effort in the analysis of coating application and performance over the long-term at projects throughout the Basin using low-VOC flat coatings. Manufacturers and applicators are encouraged to contact AQMD staff in order to document projects as they occur.

### Conclusions

The overall results show that the lower-VOC coatings, even the super-compliant coatings tested, performed comparably to their higher-VOC counterparts. As with all architectural coatings, some coatings are formulated for, and therefore perform better in certain areas; however, overall the coatings at the 50g/l limit or less performed very well.

### **B. Compliant Products Found in Internet Searches**

Staff analyzed the TDS and the MSDS published by coating manufacturers to assess the availability of Flat coatings at the future VOC limit of 50g/l. Table 4 summarizes the internet-based search for available coatings with more complete details of those findings presented in Appendix A of this report. The TAC has also contributed to and reviewed this list for accuracy.

**Table 4**  
Internet Search for Available Future Compliant Flat Coatings  $\leq 50\text{g/l}$

| Coating Category | No. of Products | Exterior(E),<br>Interior(I),<br>Dual(D) | Substrates  |
|------------------|-----------------|---|---|
| Flats            | 113             | 23-E<br>80-I<br>10-D                    | Formulated for use on most substrates, commonly used on plaster, drywall, concrete block, wood, brick and stucco. |

In addition to TDS and MSDS review, staff continues to visit sites where architectural coatings are applied, and has conducted follow-up visits to previously documented applications of low- and near zero-VOC coatings. The data gathered is used to

substantiate the availability, use and especially the continued performance of low-VOC coating products.

### C. Store Shelf Survey

In early 2007, AQMD staff conducted a survey of coatings being offered for sale at a variety of stores, including 'big box' stores, company owned stores and small paint and hardware stores in order to assess availability of coatings meeting current and future VOC limits.

Table 5 shows the availability of Flat coatings with their respective percentage compliance for 'big box' stores and company owned stores. Many of the smaller paint stores do not have a high turnover of products, so they are less likely to stock the latest paint formulations. Flexibility written into Rule 1113 allows for a 3 year sell-through of coatings manufactured prior to the implementation of a lower-VOC limit; therefore, it is not uncommon to find older paints on store shelves that exceed the current VOC limit. The numbers listed in the table below do not necessarily represent unique coatings and no attempt was made to eliminate duplicate coatings surveyed at different stores, and simply provides a snapshot of available coatings.

**Table 5**  
Store Shelf Survey of Available Future Compliant Flat Coatings  $\leq 50\text{g/l}$

| Flat Coatings                | All Stores Surveyed | Big Box Stores | Company Owned Stores |
|------------------------------|---------------------|----------------|----------------------|
| Number of Compliant Coatings | 28                  | 9              | 7                    |
| Number of Coatings Surveyed  | 175                 | 40             | 26                   |
| Percentage Compliance        | 16%                 | 23%            | 27%                  |

This shelf survey indicates a higher percentage of compliance for Flat coatings than the 2005 Draft CARB Architectural Coating Survey, especially for the big box stores and company owned stores. As indicated earlier in this report, CARB's draft survey found the number of future compliant Flat coatings at 15% in the year 2004.

### D. Meetings with Manufacturers

AQMD staff met with several large and small paint manufacturers during 2006 and 2007 to discuss issues that they were experiencing and recent technological advances in coatings formulations. The discussions included many of the coating categories listed on the Table of Standards, including Flat coatings. No major technological difficulties were mentioned in regard to formulating Flat coatings at the future limit of 50g/l. Freeze/thaw was cited as one area that needs improvement, though it is a characteristic that is not considered critical, especially in Southern California. The manufactures were cautiously optimistic due to recent technological advances in this area. Based on these meetings, AQMD staff believes that manufacturers will not experience any hardships in bringing quality Flat coatings to the marketplace meeting the July 2008 VOC limit.

### **E. Cal Poly Pomona's House Painting Project**

California Polytechnic University (Cal Poly) in Pomona has a Paint and Coatings Institute within their Chemistry Department where students learn about, formulate and test near zero-VOC containing coatings. Starting in 2004, the Paint and Coatings Institute, under the direct supervision of the professors, teamed up with a Pomona based charitable organization that provides assistance to needy families in the community, to identify annually a neglected home in need of paint. The students then volunteer their time to paint the selected house which serves not only to help a needy family, but also gives the students an opportunity to test their paints in a real life situation, far different from testing the paint on small panels in a laboratory setting. This project has become an annual event resulting in four houses now painted with near zero-VOC coatings. The professors are able to monitor the environmental exposure over time for any signs of weathering, UV deterioration, dirt pick up, and color or gloss loss.

AQMD staff had an opportunity to document the most recent project during the preparation and painting phases and viewed the previous three projects dating back to 2004. Each project underwent minimum surface preparation that included the use of a garden hose and a broom, with the most recent jobs utilizing a small pressure washer. The houses were in very poor condition with peeling paint, weathered wood, and deteriorating stucco. Although each project was completed by students and teachers, equipped with only brushes and rollers and no primers were used, the previously painted homes have held up well over the years. Also, the painting was conducted in Pomona, California during the summer when the ambient conditions are typically hot and dry. The professors did not observe any application problems such as brush marks or lap marks, even with untrained applicators.

The coatings formulations used are from manufacturer donations, are relatively simple, and contain no tannin blocking or rust preventative additives. Each painting project viewed by staff continues to exhibit good adhesion, flexibility and show no signs of dirt pick up or other failures. In a few locations on the houses where the substrate was failing and no preparatory work was done, there are signs of adhesion failure due to the distressed condition of the stucco prior to painting. Remarkably, even with minimal preparation and non-professional application, these near zero-VOC coatings are performing very well.

**F. Super-compliant Coatings**

Architectural coating manufacturers continue to improve the coating characteristics of their products while lowering the VOC content by introducing new types of resins and other paint constituents that are extremely low in VOC and even approach zero-VOC. Table 6, updated from previous annual reports to the Board, reflects a portion of super-compliant coatings currently available. Staff has given the nomenclature “Super-compliant coatings” to those coatings that are well below the current and/or future limits for the applicable coatings categories as set forth in the Table of Standards and are indicated by the manufacturer as having less than 10g/l of VOC. These also include those coatings that meet future limits in advance of their effective date. This list can be found at:

[http://www.aqmd.gov/prdas/brochures/Super-Compliant\\_AIM.pdf](http://www.aqmd.gov/prdas/brochures/Super-Compliant_AIM.pdf).

**Table 6**  
**Super-compliant Architectural Coating Manufacturers\***

| Manufacturer  | Type of Coatings         | Interior | Exterior | Phone Number                 |
|---|--------------------------|----------|----------|------------------------------|
| Alistagen Corporation<br><a href="http://www.caliwel.com">http://www.caliwel.com</a>  | PSU, F                   | YES      | NO       | 866-280-0001<br>305-936-8691 |
| American Formulators Mfg<br><a href="http://www.safecoatpaint.com">http://www.safecoatpaint.com</a>   | F, NFE, NFSG             | YES      | NO       | 619-239-0321                 |
| Anchor Paint<br><a href="http://www.anchorpaint.com">http://www.anchorpaint.com</a>   | WPC/MS                   | NO       | YES      | 918-836-4626                 |
| Benjamin Moore & Co<br><a href="http://www.benjaminmoore.com">http://www.benjaminmoore.com</a>  | PSU, F, NFS, NFE, NFSG   | YES      | NO       | 201-573-9600                 |
| Cloverdale Paint Inc<br><a href="http://www.cloverdalepaint.com">http://www.cloverdalepaint.com</a>   | PSU, NF, IM              | YES      | YES      | 604 596 6261                 |
| Coronado Paint Co<br><a href="http://www.coronadopaint.com">http://www.coronadopaint.com</a>  | F, NF, PSU               | YES      | NO       | 386-428-6461 x115            |
| Diamond Vogel<br><a href="http://www.diamondvogel.com">http://www.diamondvogel.com</a>  | F, NF, P                 | YES      | NO       | 800-728-6435                 |
| Dunn Edwards<br><a href="http://www.dunnedwards.com">http://www.dunnedwards.com</a>   | F, NF                    | YES      | NO       | 888-337-2468                 |
| E-3 Coatings, Inc<br><a href="http://www.envirolast.com">http://www.envirolast.com</a>  | S                        | NO       | YES      | 530-308-2189                 |
| Frazee Industries<br><a href="http://www.frazeepaint.com">http://www.frazeepaint.com</a>  | PSU, F, NFS, NFE, NFSG   | YES      | NO       | 858-626-3490                 |
| Fuhr International, LLC<br><a href="http://www.fuhrinternational.com">http://www.fuhrinternational.com</a>  | PSU, F, NF               | YES      | YES      | 800-558-7437<br>816-809-4403 |
| ICI Paints<br><a href="http://www.iciduluxpaints.com">http://www.iciduluxpaints.com</a> Pro painters<br><a href="http://www.devoecoatings.com">http://www.devoecoatings.com</a> IM coatings<br><a href="http://www.duspec.com">http://www.duspec.com</a> MSDS & PDS<br><a href="http://www.glidden.com">http://www.glidden.com</a> Retail for homeowners<br><a href="http://www.ici.com">http://www.ici.com</a> Corporate | PSU, F, NFS, NFE, NFSG** | YES      | YES      | 440-826-5519                 |
| Kryton<br><a href="http://www.kryton.com">http://www.kryton.com</a>   | WPS                      | YES      | YES      | 246-437-3202                 |
| Miller Paint<br><a href="http://www.millerpaint.com">http://www.millerpaint.com</a>   | PSU, F, NFE, NFS         | YES      | NO       | 503-407-2532                 |
| Monopole Inc.<br><a href="http://www.monopoleinc.com">http://www.monopoleinc.com</a>  | IM, WPS, WPC/MS          | YES      | YES      | 818-500-8585                 |
| PPG Industries - Architectural Finishes<br><a href="http://www.pittsburghpaints.com">www.pittsburghpaints.com</a>   | PSU, F, NFE, NFSG        | YES      | NO       | 800-441-9695                 |
| Polibrid Coatings<br><a href="http://www.polibrid.com">http://www.polibrid.com</a>  | F, NF, PSU               | YES      | YES      | 956-831-7818                 |
| Richards Paints<br><a href="http://www.richardspaint.com/">http://www.richardspaint.com/</a>  | F, NFR, NFS              | YES      | NO       | 800-432-0983                 |
| Rodda Paints<br><a href="http://www.rodgapaint.com/">http://www.rodgapaint.com/</a>   | PSU, F, NFE, NFS         | YES      | NO       | 503-737-6031 x6051           |
| Sampson Coatings, Inc.<br><a href="http://www.sampsoncoatings.com">http://www.sampsoncoatings.com</a>   | PSU, F, NF               | YES      | YES      | 804-359-5011                 |
| Samuel Cabot, Inc<br><a href="http://www.cabotstain.com">http://www.cabotstain.com</a>  | WPS                      | NO       | YES      | 800-877-8246                 |
| Seal-Krete Inc.<br><a href="http://www.seal-crete.com">http://www.seal-crete.com</a>  | PSU, F                   | YES      | YES      | 800-323-7357 x541            |
| Sierra Performance by Rust-Oleum<br><a href="http://www.rustoleum.com">http://www.rustoleum.com</a>   | PSU, F, NF               | YES      | YES      | 800-553-8444                 |
| Silvertown Products<br><a href="http://www.rhinoguard.com">http://www.rhinoguard.com</a>  | S, CWF                   | NO       | YES      | 909-986-7061                 |
| Spectra-Tone Paint<br><a href="http://www.spectra-tone.com/">http://www.spectra-tone.com/</a>   | F, NFE, NFSG             | YES      | NO       | 800-272-4687                 |
| TPR <sup>2</sup> - Thermal Product Research<br><a href="http://www.tpr2.com/">http://www.tpr2.com/</a>  | NF-FR, PSU-FR            | YES      | YES      | 203-756-8772                 |
| Tried & True Wood Finishes<br><a href="http://www.triedandtruewoodfinish.com">http://www.triedandtruewoodfinish.com</a>   | CWF                      | YES      | NO       | 607-387-9280                 |
| VOC Free<br>No Website  | FLOOR SEALER, PSU, F, NF | YES      | YES      | 201-457-1221                 |

**Table 6 Cont'd**  
**Super-compliant Architectural Coating Manufacturers\***

| Industrial Maintenance Coatings  |                  |          |          |               |
|--|------------------|----------|----------|---------------|
| Manufacturer   | Type of Coatings | Interior | Exterior | Phone Number  |
| Ameron, Intl.<br><a href="http://www.ameroncoatings.com/welcome.cfm">http://www.ameroncoatings.com/welcome.cfm</a>           | VARIOUS SYSTEMS  | YES      | YES      | 800-926-3766  |
| Duromar<br><a href="http://www.duromar.com/">http://www.duromar.com/</a>   | VARIOUS SYSTEMS  | YES      | YES      | 781-826-2525  |
| JFB Hart Polymers<br><a href="http://www.jfbhartcoatings.com/">http://www.jfbhartcoatings.com/</a>                           | VARIOUS SYSTEMS  | YES      | YES      | 630-574-1729  |
| Novocoat<br>(Formerly) Superior Environmental Products, Inc<br><a href="http://www.novocoat.com">http://www.novocoat.com</a> | VARIOUS SYSTEMS  | YES      | YES      | 972-490-0566  |
| Pacific Polymer<br><a href="http://www.pacpoly.com/">http://www.pacpoly.com/</a>   | VARIOUS SYSTEMS  | YES      | YES      | 800-888-8340  |
| Specialty Products Inc.<br><a href="http://www.specialty-products.com">http://www.specialty-products.com</a>                 | VARIOUS SYSTEMS  | YES      | YES      | 253- 983-7530 |
| United Coatings<br><a href="http://www.unitedcoatings.com/">http://www.unitedcoatings.com/</a>                               | VARIOUS SYSTEMS  | YES      | YES      | 800-541-4383  |

|       |  |
|-------|--|
| CWF   | Clear Wood Finish                      |
| F     | Flats                                  |
| NF    | Non-flat                               |
| NFS   | Non-flat - satin                       |
| NFE   | Non-flat - eggshell                    |
| NFSG  | Non-flat - semi-gloss                  |
| PSU   | Primers, sealers, and undercoaters     |
| S     | Stains                                 |
| WPS   | Waterproofing Sealer                   |
| WPCMS | Waterproofing Concrete/Masonry Sealers |

\* Super-compliant coatings are defined as those coatings that have a VOC content less than the VOC content limits set forth for the current and/or future limits in the Table of Standards found in paragraph (c)(2) of Rule 1113 and specify a VOC content less than 10 g/L.

\*\* Not available for exterior use.

This is not an all-inclusive list of super-compliant coatings available from manufacturers/suppliers who have informed SCAQMD that they can provide the super-compliant products listed.

The SCAQMD in no way endorses any of these companies nor does it certify their ability to meet the requirements of Rule 1113 Architectural Coatings. If you want your company included in this page, please send your request to [hfarr@aqmd.gov](mailto:hfarr@aqmd.gov) or call Heather Farr at (909) 396-3672.

### **G. Master Painters Institute® (MPI)**

MPI is a Canadian based organization founded to develop performance-based standards in conjunction with paint manufacturers and paint technologists. The performance based standards are widely accepted and are approved by the US Navy, Army, and Air Force as well as other US and Canadian agencies. MPI develops lists of approved products in almost 200 categories. In 2005, MPI developed a Green Performance Standard (GPS-1) which sought to consider not only the VOC content of a coating but also the performance of the coating. More recently, MPI developed a more stringent Green Performance Standard (GPS-2) for coatings with a maximum VOC content of 50g/l. MPI's Green Performance Standards and approved product lists are the only green certification program to include performance based testing along with VOC content. The MPI approved product lists are an excellent resource for high quality coatings that have been tested in a laboratory using widely accepted test methods with regard to each category type. MPI has 10 categories for Flat coatings<sup>1</sup> containing 61 approved products meeting the AQMD's future VOC limit of 50g/l and they have a category for Institutional Low Odor/VOC Interior Latex (MPI#143) for coatings with a VOC content less than 10g/l containing 26 approved products.

The lists of products meeting MPI Green Performance Standards can be found at:

[www.specifygreen.com](http://www.specifygreen.com)

### **H. Papers Presented at Recent Conference in 2007**

In addition to the articles researched relative to the development of lower-VOC architectural coatings, recent papers and presentations made at coatings symposiums indicate the availability and support from resin and additive suppliers of low-VOC coating components that meet or are lower than future VOC limits in Rule 1113.

The Federation of Societies for Coatings Technology (FSCT) sponsors an annual event that is the largest North American exposition in the coatings industry, the International Coatings Expo (ICE). Included in the exposition is a technical forum featuring three days of lectures. Both the 2006 and the upcoming 2007 forums feature a track that focuses exclusively on green chemistry and include the developments of innovative resins and additives that enable formulating of low-VOC to near zero-VOC coatings.

The upcoming Western Coatings Symposium sponsored by the Los Angeles Society for Coatings Technology also features a lecture series on green chemistry including new resin and additive technologies. Clearly there is an increasing interest in green coatings to meet regulations, but also as a tool for marketing coatings.

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<sup>1</sup> Gloss level 1 defined as a coating that registers a gloss of <5 at 60° and <10 at 85° meeting the Rule 1113 definition of a Flat coating.

## ADDITIONAL TECHNICAL PROGRAMS AND STUDIES

### A. Draft CARB 2005 Architectural Coatings Survey

Rule 1113 requires AQMD technology assessments to consider any applicable CARB surveys on architectural coatings. Approximately every four or five years since 1976, CARB has conducted architectural coating surveys. The survey methodology serves as a tool to obtain information such as VOC content and sales volume of coatings from manufacturers that offer products for sale in California. Draft data obtained from the 2005 Architectural Survey represents a comprehensive evaluation of sales data and coating chemistries from the 2004 calendar year based on the latest information available from participating manufacturers. A more thorough evaluation of the CARB survey will be conducted once the survey is finalized and the data is released this fall.

The sales data obtained for 2004 separates architectural coatings statewide into 48 categories, identifying more than 111 million gallons of architectural coatings sold in California in 2004, with 88% of that volume coming from waterborne products, an increase from the 83% reported in 2000. However, waterborne products contributed to only 48% of the total emissions, while the remaining 12% solvent-based volume reported, contributed to 52% of the total emissions. The sales of architectural coatings in the AQMD are based on an estimated population representing 45% of all coatings sold statewide. Table 7 summarizes the use and contribution of waterborne and solvent-based coatings from the most recent CARB survey.

**Table 7**  
CARB Survey - California

| Survey Results              | Waterborne | Solvent-Based |
|-----------------------------|------------|---------------|
| Total Volume (%)            | 88         | 12            |
| Total Emissions (%)         | 48         | 52            |
| Annual Volume (Gal/Yr)      | 97,365,588 | 13,311,087    |
| AQMD Annual Volume (Gal/Yr) | 43,814,515 | 5,989,989     |

When comparing this recent data relative to the overall sales volume of lower-VOC products with data from previous CARB surveys, sales information indicates an increase in manufactured products that meet or are lower than current VOC limits in Rule 1113.

CARB has also calculated the associated emissions using this data. Table 8 shows coating volume and emission trends. Please note that the surveys have varied in content and format; therefore, it is not always possible to make a direct comparison between results from different survey years.

**Table 8**  
CARB Architectural Coatings Volume and Emissions Trends

| Survey Year | Sales Volume (gallons) | Emissions (lbs) <sup>1</sup> | California's Population <sup>2</sup> | Pounds of VOC Emissions per capita | # of Surveys Mailed Out | # of Companies Reporting Sales |
|-------------|------------------------|------------------------------|--------------------------------------|------------------------------------|-------------------------|--------------------------------|
| 1975*       | 48,206,000             | 82,490,000                   | 21,538,000                           | 3.8                                | N/A                     | N/A                            |
| 1980*       | 60,489,756             | 99,791,000                   | 23,782,000                           | 4.2                                | N/A                     | N/A                            |
| 1984        | 58,481,000             | 97,747,000                   | 25,816,000                           | 3.8                                | ~400                    | 143                            |
| 1988        | 77,876,000             | 84,096,000                   | 28,393,000                           | 3.0                                | N/A                     | 130                            |
| 1990        | 77,056,000             | 77,380,000                   | 29,828,000                           | 2.6                                | N/A                     | 174                            |
| 1996        | 87,496,000             | 72,562,000                   | 31,963,000                           | 2.3                                | >700                    | 152                            |
| 2000        | 98,455,172             | 80,081,000                   | 34,099,000                           | 2.3                                | 700                     | 183                            |
| 2004        | 110,676,675            | 69,423,000                   | 36,522,000                           | 1.9                                | 900                     | 197                            |

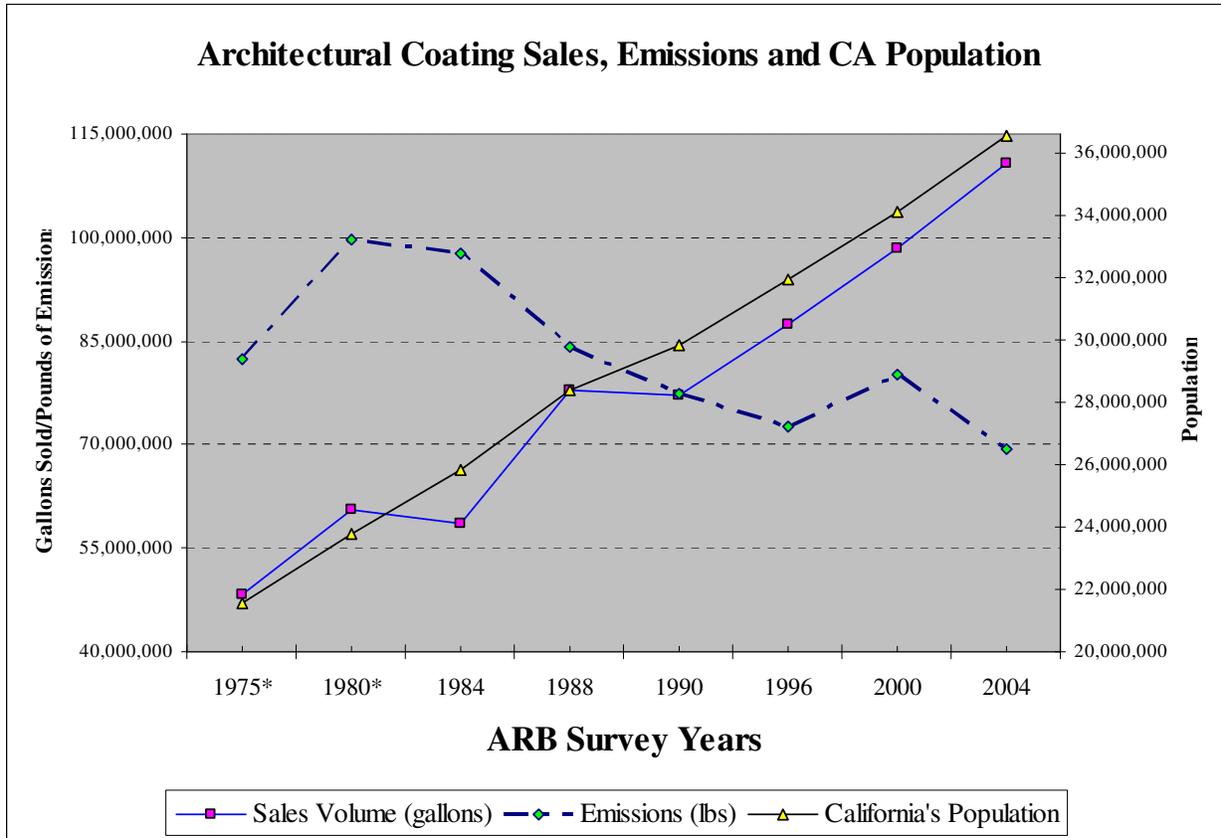
\* Incomplete surveys

N/A = Not Available

1. Thinning and clean-up or additive emissions not included because CARB changed the methodology for calculating cleanup solvents in 2004.
2. Population data from CA Department of Finance, Demographic Research Unit, Dec. 2006.
3. Staff is studying whether the sales volume increase is attributed to population increase, larger average gross living area of homes, and more frequent turnover of single family residences and apartments.

The trends shown in Table 8 are illustrated in Graph 3, showing that overall emissions continue to decline despite increased production and sales of coatings in the state.

Graph 3



While California’s population and sales volume of coatings grew significantly over the last 29 years, statewide VOC regulations requiring lower-VOC limits have managed to reduce the emissions from architectural coatings to lower than the 1975 emission levels. Regulations began having an effect on architectural coating emissions by 1984. Emissions continued to decline through the real estate recession until 1996, and resumed their increase from that point until 2000. As predicted in the 2006 Annual Report, emissions declined from 2000 to 2004, most likely reflecting the effect of regulatory action. The next CARB survey should begin to show the effects of the recent VOC reductions in Rule 1113.

I. Flat Coatings Data from Draft CARB 2005 Architectural Coatings Survey

Table 9 summarizes information extracted from the 2004 sales data on Flat coatings. The information contained in the most recent CARB survey represents sales data from 2004, four years prior to the lower-VOC limit taking effect. This data demonstrates that manufacturers are developing and marketing coatings compliant with the future VOC limits in Rule 1113.

**Table 9**  
CARB 2004 Sales Results – California (excludes quart containers or smaller)

| Coating Category | Total Products Listed | Total 2004 Sales Volume (gallons) | # of Products Meeting Future VOC Limits | Sales Volume meeting Future VOC Limits | % of Products Meeting Future VOC Limits | % of Sales Meeting Future VOC Limits |
|------------------|-----------------------|-----------------------------------|---|--|---|--------------------------------------|
| Flats            | 2,438                 | 36,699,154                        | 360                                     | 2,390,135                              | 15%                                     | 7%                                   |

The sales volume of products meeting the future VOC limit for Flat coatings decreased slightly from the last survey conducted by CARB for the calendar year 2000. That survey indicated 8% future complying market share with the 2008 limit, while the 2004 sales data indicates 7%. The future complying market shares obtained from the CARB surveys represent coatings sold throughout California. AQMD staff has always assumed that the percent complying market share is higher in the South Coast Air Basin where stricter limits require the use of lower-VOC coatings. As this data cannot be extracted from the CARB surveys, there is a clear need for survey data of coatings sold throughout the AQMD.

#### **B. CARB/AQMD Reactivity Study**

As a part of the 1999 amendments to Rule 1113 – Architectural Coatings, the AQMD Board approved a resolution directing staff to assess the reactivity and availability of solvents typically used in the formulation of architectural coatings. As a part of that effort, staff has also been assessing interactions between architectural coating and mobile emission sources on particulate matter (PM) formation.

The Reactivity Research Working Group (RRWG) is a public-private partnership with a charter to conduct research on reactivity-based controls to determine whether it is feasible as an alternative compliance option. As a member of RRWG, AQMD staff has coordinated their current efforts with CARB, as well as recommendations by the RRWG. As part of the collaborative effort, a study was completed in 2005 using an environmental chamber at the University of California at Riverside (UCR). The study used the chamber to evaluate mechanisms for photochemical O<sub>3</sub> formation under low NO<sub>x</sub> conditions (Carter 2004) and for other projects. A final report has recently been released and the CARB and AQMD will continue to address the possibility of an alternate ozone control strategy. However, to date, industry has not reached consensus on the methodology to potentially implement such an approach. Staff plans to conduct a Technology Roundtable in the fall of 2007 to discuss the strengths, weakness, and potential next steps for a reactivity-based ozone control strategy.

Staff will continue to monitor all reactivity-related research and plans to work closely with CARB staff and industry on additional studies, including the Paints and Coatings Environmental Study currently under development at CE-CERT.

## C. Alternate Means of Compliance

### I. Averaging Compliance Option

#### *History*

The averaging compliance option (ACO) program was developed to provide flexibility to manufacturers by allowing additional time to reformulate certain coatings that would be affected by upcoming VOC limit reductions in Rule 1113. This provision allows a coating manufacturer the option to continue selling higher-VOC coatings in certain categories by offsetting those emissions with low-VOC coatings such that the total emissions are less than the allowable emissions.

The ACO program was started in July 2001. Table 10 provides an overview of the ACO program, including the number of participating manufacturers and the coating categories averaged.

**Table 10**  
ACO Period and Number of Coating Manufacturers

| Year of ACO Period | Number of Manufacturers | Coating Categories Allowed for Averaging  |
|--------------------|-------------------------|---|
| 2002 *             | 3                       | F   |
| 2003               | 8                       | FL, PSU, QDE, QDPSU, RPC, SP, STN, WS, IMC, NF  |
| 2004               | 9                       |   |
| 2005               | 8                       |   |
| 2006               | 10                      |   |
| 2007               | 12                      | Same as above plus**: FRC, FRP, HGNF, MPC, RP, SS, STNi, CWF-V, WCMS, CWF-SSsc, CWF-Vsc |

\*2002 is actually the July 1, 2001 through June 30, 2002 ACO period

\*\*Effective July 1, 2006

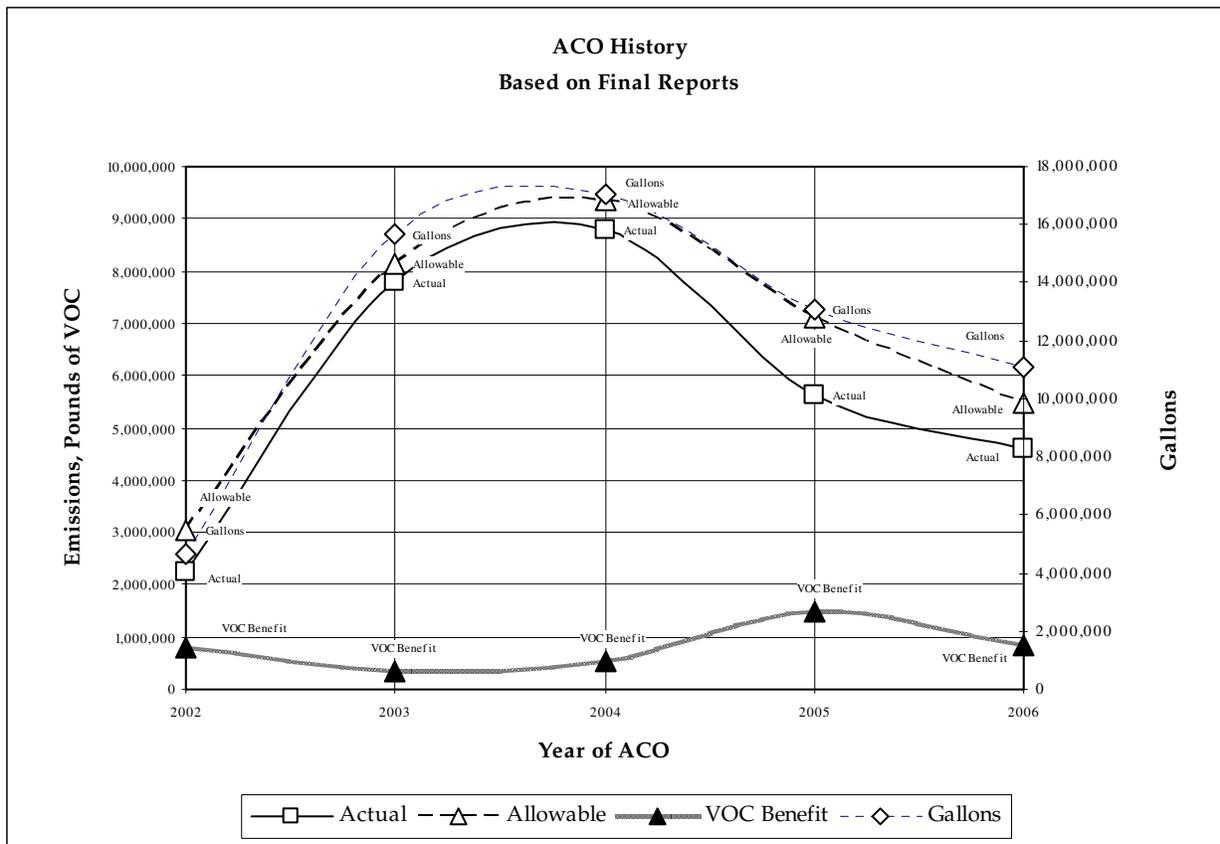
| KEY  |  |
|--|--|
| <b>CWF-SSsc</b> = Clear Wood Finish-Sanding Sealer (small container size), | <b>PSU</b> = Primers, Sealers, Undercoaters,             |
| <b>CWF-V</b> = Clear Wood Finish-Varnish,                                  | <b>QDE</b> = Quick-dry Enamels,                          |
| <b>CWF-Vsc</b> = Clear Wood Finish-Varnish (small container size),         | <b>QDPSU</b> = Quick-dry Primers, Sealers, Undercoaters, |
| <b>F</b> = Flat Coatings,  | <b>RP</b> = Roof Primers, Bituminous,                    |
| <b>FL</b> = Floor Coatings,  | <b>RPC</b> = Rust Preventative Coatings,                 |
| <b>FRC</b> = Fire Retardant-Clear Coating,                                 | <b>SP</b> = Specialty Primers,                           |
| <b>FRP</b> = Fire Retardant-Pigmented Coatings,                            | <b>SS</b> = Sanding Sealers,                             |
| <b>HGNF</b> = High Gloss Non-flat Coatings,                                | <b>STN</b> = Stain,                                      |
| <b>IMC</b> = Industrial Maintenance Coatings,                              | <b>STNi</b> = Stains, Interior,                          |
| <b>MPC</b> = Metallic Pigmented Coatings,                                  | <b>WCMS</b> = Waterproofing Concrete Masonry Sealers,    |
| <b>NF</b> = Non-flat Coatings  | <b>WS</b> = Waterproofing Sealers                        |

AQMD staff has completed audits on four ACO programs and determined all were in compliance. Three of the audits were for the July 1, 2001 to June 30, 2002 period and the fourth audit was for the 2003 calendar year. Staff is currently auditing the remainder of the ACO plans and is working with the coating manufacturers to complete the process.

**Statistics**

The ACO program has been available to manufacturers since 2001, enabling staff to analyze statistics related to the coatings. Graph 4 shows a cumulative overview of the gallons sold, the actual emissions, and the allowable emissions for coating manufacturers that have participated in the averaging compliance option to date. The graph shows a timeframe ranging from 2002 to 2006 (year 2007 data is not yet available); the year 2002 includes the averaging period July 1, 2001 through June 30, 2002.

**Graph 4**



**Graph Discussion**

Graph 4 shows trend lines for actual emissions, allowable emissions, VOC benefit and gallons. There is a marked increase from the year 2002 to 2003. This is because the year 2002 included three coating manufacturers, while the year 2003 included eight coating manufacturers. The increase is also due to additional coatings categories being allowed in the ACO program. The year 2003 was a milestone in Rule 1113, since multiple coating categories had VOC limit reductions starting on January 1, 2003. The trend lines increase slightly from the year 2003 to 2004 because there were nine coating manufacturers averaging for 2004, an increase of 12.5%. The trend lines between the year 2004 and the year 2005 show a large decrease. There were nine coating manufacturers reporting in 2004 and eight coating manufacturers reporting in 2005. The

area between the actual emissions and the allowable emissions show that the year 2005 had a larger gap (greater emission reduction benefit) than the year 2004. This shows that the coating manufacturers have continued to reformulate coatings to meet the upcoming VOC limits. There were three coating categories that had VOC reductions for year 2005 but they were not used in any of the ACO programs. The trend lines between the year 2005 and 2006 show another decrease, but the area between the actual emissions and the allowable emissions is less for 2006 than 2005. The year 2006 affected several coating categories, additional VOC limit reductions began in the middle of the year on July 1, 2006. Many coating manufacturers had to make mid-year adjustments to comply with their ACO programs, some also had to eliminate their supply of the higher-VOC products. The reduction of actual emissions from 2004 to 2006 calculates to 47.5% even though year 2006 had one more coating manufacturer averaging than year 2004.

The VOC benefit trend line in Graph 4 reflects the emission reduction benefit in any prior year. This is the difference between the allowable emissions and the actual emissions. The allowable emissions are the maximum that can be emitted at the regulatory limits, while the actual emissions are those that were emitted based on sales of coatings in the manufacturers ACO reports. The difference demonstrates that through the ACO program, the actual emissions were significantly lower than the allowable emissions. Table 11 shows Graph 4 in tabular format.

**Table 11**  
Annual Summary of ACO Plans

| Year                 | Volume (gal/yr) | Actual (lbs/yr) | Allowable (lbs/yr) | VOC Benefit (lbs) |
|----------------------|-----------------|-----------------|--------------------|-------------------|
| 2002                 | 4,679,617       | 2,241,674       | 3,053,318          | 811,644           |
| 2003                 | 15,698,206      | 7,775,839       | 8,120,810          | 344,971           |
| 2004                 | 17,075,532      | 8,787,633       | 9,337,542          | 539,908           |
| 2005                 | 13,095,173      | 5,614,696       | 7,093,904          | 1,479,208         |
| 2006                 | 11,080,033      | 4,616,066       | 5,467,371          | 851,304           |
| <b>Total Benefit</b> |                 |                 |                    | <b>4,027,035</b>  |

The data shows that the coating manufacturers are reformulating their products and meeting the VOC requirements in Rule 1113. Many of the large manufacturers continue to use the ACO and utilize new low-VOC coating products that are used to offset their sales of higher-VOC products. In addition, as the VOC limits of several coating categories have been reduced through rule amendments, most of these same categories are also included in the ACO projection, allowing the manufacturers to offset the higher-VOC coatings with the new low-VOC coatings. In 2007, there are twelve coating manufacturers participating in the ACO program.

***ACO – Conclusion***

The manufacturers have expressed the benefits of utilizing the ACO, since it provides them with compliance flexibility by allowing them to continue marketing some niche higher-VOC products and offsetting them with low-VOC products. Similarly, recent court decisions have also supported the ACO and recognized this provision as an “escape clause” that provides manufacturers with compliance flexibility, while retaining the more stringent limits.

Staff recognizes that the ACO cannot be used by all manufacturers, but will continue the provision for other manufacturers who have demonstrated its benefits.

**II. Sell Through Option**

As mentioned in previous reports to the board, another compliance option available to architectural coating manufacturers allows the sale or application of a coating manufactured prior to the effective date of the corresponding standard in the Table of Standards for up to three years after the effective date of the standard. This sell-through provision applies to all coatings listed in the Table of Standards and any effective dates applicable to the specific coating. Many manufacturers continue to take advantage of this available option in order to allow them additional time to reformulate their products just prior to the effective date change in the limits. This allows the manufacturers to eliminate any potential losses in revenue due to excess stock of non-compliant coatings.

**III. Small Container Exemption**

Another compliance option is the small container exemption which provides regulatory relief to the manufacturers provided they submit an annual report within three months of the end of each calendar year for their products that are sold in quart size containers or less in select categories. If a manufacturer fails to submit their annual report, the manufacturer cannot claim the exemption for the previous year. The number of reporting manufacturers selling coatings within the jurisdiction of the AQMD under this exemption has increased over the years. Table 12 below shows the trend.

**Table 12**  
AQMD Small Container trends, 2000-2006, Companies Reporting

|                               | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 |
|-------------------------------|------|------|------|------|------|------|------|
| Number of Companies Reporting | 12   | 13   | 15   | 24   | 29   | 30   | 34   |

Staff has been actively tracking the statistics of the small container exemption under Rule 1113. These reporting requirements assist AQMD staff in tracking the excess emissions that result from the small container exemptions and assist in tracking other coating categories of interest. In the last rule amendment, the exemption was removed for Clear Wood Finishes as the reporting requirement revealed a sharp increase in sales, indicating a possible circumvention of the VOC limit for that category.

In 2006, the small container exemption resulted in excess emissions of approximately 1.1 tons per day; a slight decrease from 2005 where there was approximately 1.5 tons per day of excess emissions. Table 13 displays the data from the year 2000 through 2006. The table also summarizes the total volume of coatings sold under the small container exemption in Rule 1113.

**Table 13**

AQMD Small Container Trends, 2000-2006, Product Category Sales Reported in Gallons

| Coating Category       | 2000           | 2001           | 2002           | 2003           | 2004           | 2005           | 2006           |
|------------------------|----------------|----------------|----------------|----------------|----------------|----------------|----------------|
| Faux Finishes          | 128            | 190            | 0              | 9,943          | 6,202          | 4,615          | 5,032          |
| Flat                   | 246            | 4,813          | 24,613         | 10,645         | 6,358          | 5,678          | 728            |
| Floor                  | 0              | 70             | 0              | 1,709          | 840            | 980            | 1,054          |
| Industrial Maintenance | 641            | 0              | 169            | 21,998         | 364            | 2,355          | 1,950          |
| Lacquers               | 237            | 1,333          | 1,964          | 745            | 2,404          | 2,860          | 2,068          |
| Mastic Coating         | 0              | 0              | 0              | 35             | 0              | 0              | 0              |
| Metallic Pigmented     | 0              | 101            | 0              | 1,487          | 154            | 63             | 76             |
| Multi-Color            | 109            | 0              | 0              | 0              | 0              | 0              | 0              |
| Non-Flat               | 13,819         | 19,748         | 9,503          | 98,753         | 36,640         | 14,945         | 28,164         |
| Non-Flat High Gloss    |                |                |                |                |                |                | 5,856          |
| PSU                    | 18,864         | 13,225         | 26,197         | 25,043         | 21,904         | 21,658         | 18,533         |
| QD-E                   | 0              | 0              | 0              | 4,605          | 4,683          | 1,722          | 2,550          |
| QDPSU                  | 1,335          | 1,651          | 327            | 4,465          | 14,826         | 24,265         | 26,755         |
| Roof Coating           | 0              | 0              | 0              | 32,969         | 9              | 0              | 0              |
| Rust Preventative      | 0              | 0              | 0              | 70             | 107            | 68,826         | 50,107         |
| Sanding Sealer         | 583            | 735            | 4,061          | 2,825          | 3,654          | 3,686          | 2,332          |
| Stain                  | 120,299        | 141,650        | 220,058        | 250,243        | 270,601        | 246,868        | 224,711        |
| Traffic Coating        | 0              | 0              | 0              | 7,250          | 0              | 0              | 0              |
| Varnishes              | 125,764        | 130,197        | 186,557        | 217,289        | 235,140        | 253,906        | 125,056        |
| Waterproofing Sealers  | 197            | 48             | 1,798          | 1,478          | 92             | 45             | 29             |
| WCMS                   | 0              | 0              | 0              | 229            | 17             | 1,932          | 11,349         |
| <b>Total:</b>          | <b>282,221</b> | <b>313,760</b> | <b>475,247</b> | <b>691,781</b> | <b>603,995</b> | <b>654,404</b> | <b>506,349</b> |

One can see from Table 13 that the total sales for each year increased except for year 2004 and 2006. Interpreting the data in 2006 was complicated by several changes in Rule 1113. Due to the elimination of the small container exemption for the Clear Wood Finishes, manufacturers were only required to report small container sales for Clear Wood Finishes up to June 30, 2006. This resulted in an expected decrease in reported sales. If it is assumed that the sales volume of Clear Wood Finish for the full calendar year is double what was reported, then the gallons sold under the exemption would increase to approximately 635,000, which is still a decrease from 2005.

Sales of Flat coatings, under the small container exemption have decreased sharply since 2002. During the 2006 calendar year only 727 gallons were reported sold. This indicates that manufacturers do not need this exemption to produce compliant Flat coatings or to produce niche products requiring higher-VOC formulations.

Graph 5 presents the totals shown in Table 13 in graphical format.

**Graph 5**



#### **D. Summary of Past AQMD Sponsored and Other Coating Studies**

To address concerns by industry representatives and coating manufacturers that lowering the allowable VOCs in products to meet the future limits may compromise coating characteristics such as applicability and durability; staff has contracted with industry experts and conducted several studies over the years. Staff also continues to review those completed by other agencies and the industry.

Prior reports and summaries submitted to the Board regarding architectural coatings include coating technology assessments and product availability studies that indicated the availability of compliant coatings in the specific categories studied. A review of those studies supports staff's contention that low-VOC and super-compliant coatings meet or exceed expected characteristic performance standards compared to products that have much higher-VOC content. For a summary of past studies refer to the 2006 Annual Status Report for Rule 1113 which can be found at:

<http://www.aqmd.gov/hb/2006/060126a.html>

#### **E. Future Program Activities and Studies**

AQMD staff will continue to review and maintain a current database of compliant and super-compliant products in all coating categories for additional products with VOCs less than current and future rule limits. As technology improves and VOCs in all categories get closer to zero, staff will continue to evaluate the feasibility of further reductions in the VOC content of all architectural coating categories as currently listed in the Table of Standards in Rule 1113. Voluntary use of available low-VOC or near zero-VOC technology is evidence that the coatings are performing at or above industry expectations.

Staff will be involved in the following activities over the next year:

##### **I. Technology Roundtable on Reactivity Fall 2007**

As a part of the 1999 amendments to Rule 1113 – Architectural Coatings, the AQMD Board approved a resolution directing the staff to assess the reactivity and availability of solvents typically used in the formulation of architectural coatings. To assist in the assessment, a Technology Roundtable will be held in the fall of 2007 to discuss the strengths, weakness, and potential next steps for a reactivity-based ozone control strategy.

##### **II. Architectural Coatings Technical Symposium 2008**

Staff will hold an Architectural Coatings Technical Symposium (ACTS) in 2008 as an outreach to manufacturers, contractors, architects and painters. The goal is to provide an open forum of communication and to exchange information among all parties impacted by Rule 1113.

### III. More Robust Enforcement Program

As VOC limits continue to decrease, AQMD will enhance enforcement efforts by continuing a strong field presence at construction sites, points of distribution, and other architectural coating projects.

### IV. Clean Coatings Certification Program

The 2007 AQMP contains a control measure (#CTS-02) to implement a certification program for coatings with low-, ultra low- or near zero-VOC content. The intent is to positively influence the manufacturing, marketing, and consumer purchase decisions towards products that produce fewer emissions. This suggested control measure could potentially foster the marketing of cleaner technologies by encouraging manufacturers to lower their VOC content to levels below what traditional control rules mandate, in an effort to reduce the overall VOC emissions in the Basin.

### V. Test Methodology for VOC Analysis

EPA Method 24 and SCAMQD Method 304<sup>2</sup> are rigorous test methods that provide accurate and reliable results when measuring the volatile organic compounds (VOC) in many architectural coatings, but there is inherent variability when employing Method 24 to analyze the VOC content of low-VOC waterborne coatings. The AQMD has invested a significant effort in working with industry, CARB, US EPA, and academic institutions in identifying a superior alternative to Method 24.

Specifically, the AQMD has spent considerable effort investigating ASTM Method D6886 as an alternate to Method 24 for the analysis of low-VOC waterborne coatings. Method D6886 appears to be an improvement to Method 24 because it directly measures the VOC content of a coating yielding far greater precision. AQMD staff will continue to investigate this new method and if it proves to be a reliable alternative to current Method 24, staff will seek EPA approval for incorporating Method D6886, or an equivalent method, into AQMD 304 for the analysis of low-VOC waterborne coatings.

### VI. Proposed Coating Registration

AQMD staff will be proposing a rule for architectural coatings to require registration of all architectural coatings manufactured, supplied, sold, or offered for sale for use within the South Coast Air Basin. For over 30 years the AQMD has regulated architectural coatings, mainly relying on California Air Resources Board (CARB) architectural coating surveys for sales and emission data relative to rule and Air Quality Management Plans development. The data provided by CARB relates to all of California, and the South Coast Air Basin portion of the sales and emissions are typically estimated by population demographics, which may or may not estimate the correct emission inventory from the sale and use of architectural coatings. The data is often three to six years old and may not reflect newer technologies recently released into the consumer market, particularly lower-VOC containing products. With the adoption of this proposed rule, staff will have the

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<sup>2</sup> EPA Method 24 and AQMD 304 are not identical but they use the same principles, cite the same ASTM methods, and are included in Rule 1113.

most current and reliable architectural coating information for compliance, Rule Development and Air Quality Management Plans.

In addition to the registration aspect, the proposed rule is also intended to recover program costs associated with the AQMD's architectural coatings program. The current Rule 1113 program is extensive and includes staff assigned to inspections, planning and rule development, laboratory services, legal, administrative, and monitoring and analysis as well as support personnel

#### VII. Other Future Activities

1. Further Evaluation of the Final 2005 CARB Architectural Coatings Survey for Year 2004 Sales
2. Updates of Low- and Super-Compliant- VOC Product Availability Lists
3. Compliance Audits of Averaging Compliance Plans

### CONCLUSIONS

AQMD's performance studies and research of technical information from many coating manufacturers, coating studies, assessments of sales data, marketing brochures, Material Safety Data Sheets and other sources, clearly shows an ever increasing number and volume of products that meet the future proposed limits, or are well below current limits.

The completion of the most recent technology assessment by the University of Missouri-Rolla-Coatings Institute demonstrates that the 2008 limit for Flat coatings is feasible. Field and product availability surveys also demonstrate that there currently are more than adequate replacement products for the higher-VOC Flats, many of which are well below the current lowest effective limit of 50 g/l VOC.

## APPENDIX A

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Internet Search of Future Compliant Flat Coatings

Rule 1113 Future Flat Compliant Coatings  
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| <b>Flats (<math>\leq 50</math> g/l)</b>  |                      |                   |                      |                      |  |                                |
|--|----------------------|-------------------|----------------------|----------------------|--|--------------------------------|
| Coating Company and Product Name   | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics  | Dry time                       |
| Alistagen<br>Caliwel with BNA<br>Antimicrobial Interior Latex<br>Covering                    | Interior             | 0                 |                      | 250                  | Protects surface coating from microorganisms such as odor-causing bacteria, mold, mildew algae and fungi for years after application.  | 15 min touch<br>4 hr recoat    |
| American Formulating &<br>Manufacturing<br>Safecoat Flat Zero VOC 1411                       | Interior             | 0                 | 33                   | 350                  | Premium quality, fast curing paint designed for interior surfaces where a flat finish and superior film formation properties are needed.   | 1 hr touch<br>4 hr recoat      |
| American Pride Paint<br>Interior Flat Latex Paint 100<br>Line                                | Interior             | 0                 | 38                   | 400                  | This product can be used in occupied areas without typical odor complaints because of the very low odor during application and drying.   | 2 hr touch<br>Overnight recoat |
| Benjamin Moore<br>M59 220 Latex Fire Retardant<br>Coating                                    | Interior             | 0                 | 48                   | 150-300              | A premium quality decorative, intumescent, fire retardant paint for interior ceilings, walls and trim.   | 1 hr touch<br>4 hr recoat      |
| Benjamin Moore<br>MoorGard® N103 100%<br>Acrylic Low Lustre Latex<br>House Paint             | Exterior             | 37                | 43                   | 300-400              | Protective exterior coating that will remain looking freshly painted years after the job is finished and can be applied at a wider temperature range.  | 2-4 hr touch<br>4 hr recoat    |
| Benjamin Moore<br>Moorcraft Super Spec® 100%<br>Acrylic Latex Low Lustre<br>House Paint N185 | Exterior             | 48                | 34                   | 350-475              | 100% acrylic exterior latex house paint with a low lustre finish. This product is suitable for use on a wide variety of exterior surfaces and for application at temperatures as low as 40°F.          | 1 hr touch<br>4 hr recoat      |
| Benjamin Moore<br>Pristine Eco® Spec Interior<br>Latex Flat 219                              | Interior             | 0                 | 34                   | 400-450              | A low odor, low VOC, 100% acrylic latex flat that provides high hiding, excellent touch up, and a uniform flat finish.   | 1 hr touch<br>2 hr recoat      |
| Benjamin Moore<br>MoorLife® N105 100%<br>Acrylic Flat Latex House Paint                      | Exterior             | 46                | 42                   | 300-400              | Protective coating that will remain looking freshly painted years after the job is finished and can be applied at a wider temperature range.   | 2-4 hr touch<br>4 hr recoat    |
| California Paints<br>Fres~Coat Low VOC Low<br>Odor Flat with Microban<br>63391               | Interior             | 15                | 32                   | 250-350              | Provides excellent hide, minimizes surface imperfections, has excellent color retention and is washable with Microban® that will inhibit the growth of stain and odor causing bacteria, mold & mildew. | 1 hr touch<br>2 hr recoat      |
| Cloverdale Paint<br>Horizon Interior Flat Latex<br>Wall Paint 90763                          | Interior             | <1                | 40                   | 317-420              | Designed to significantly reduce odor and polluting vapors. A durable finish that hides small surface imperfections due to its smooth appearing flat wall finish.                                      | 30 min touch<br>3 hr recoat    |
| Columbia<br>Professional High-Build<br>Interior Latex Flat 02-558                            | Interior             | 50                | 38-40                | 100                  | Provides excellent high build properties, fills and seals porous surfaces, minimizes surfaces imperfections, and offers very good low temperature low flexibility.                                     | 2 hr touch<br>24 hr recoat     |

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| <b>Flats (<math>\leq 50</math> g/l)</b>  |                      |                   |                      |                      |   |                                      |
|--|----------------------|-------------------|----------------------|----------------------|---|--------------------------------------|
| Coating Company and Product Name   | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics   | Dry time                             |
| Columbia Paint<br>Professional Interior Latex Flat Primer Finish 02-737            | Interior             | 22                | 28-30                | 320                  | Good hiding and touch-up, dries to smooth uniform flat finish with easy application and clean up.   | .5 - 1 hr touch<br>2 - 4 hr recoat   |
| Columbia Paint<br>Professional Pro-Choice Interior Latex Flat Primer Finish 02-790 | Interior             | 47                | 24-26                | 325                  | Dries to a durable flat finish. Offers excellent touch up, is easy to apply by brush, roller and cleans up easily with soap and water. Dries rapidly and has low odor.  | .5 - 1 hr touch<br>2 - 4 hr recoat   |
| Columbia Paints<br>PURECOAT Low Odor Acrylic Flat 05-578                           | Interior             | 0                 | 34-36                | 360                  | Features very good flow and leveling, water clean up, good hiding, excellent spatter resistance, and adhesion to a variety of properly prepared glossy surfaces. Fortified with Microban® Antimicrobial Protection. | 0.5-1 hr touch<br>4-6 hr recoat      |
| Coronado Paint<br>Air Care Odorless Acrylic Flat                                   | Interior             | 0                 | 35.5                 | 450                  | It is spatterless during application, flows easily, has excellent hiding power, dries quickly and cleans up readily with soap and water and can withstand repeated washings.  | 30 min touch<br>4 hr recoat          |
| Devoe Paint<br>Wonder-Pure™ No-VOC/Odor Interior Flat Wall Paint DR 31XX           | Interior             | 0                 | 34                   | 400                  | Virtually no odor, quick drying and recoat, uniform appearance, excellent touch-up, super hide, washable and scrubbable.  | .5 - 1 hr touch<br>2 hr recoat       |
| Diamond Vogel<br>Health Kote Interior Latex Flat DF-1591                           | Interior             | 0                 | 39                   | 626                  | High quality low odor, Zero VOC product that dries to a durable velvety flat finish and has excellent washability and easy cleaning.  | 1 - 2 hr touch<br>4 -6 hr recoat     |
| Dunn-Edwards<br>Ultra-Scrub™ Interior Scrubable Latex Flat Paint W 6400            | Interior             | 50                | 36                   | 300-375              | Providing a tough, durable finish that is extremely washable. Excellent touch up qualities, very good hide, and is self priming on new drywall.   | 30 - 60 min touch<br>2 - 4 hr recoat |
| Dunn-Edwards<br>Flex-Tex® Texture Coating Medium W 322                             | Exterior             | 50                | 48                   | 40-50                | Quality medium textured coating that provides good flexibility and good weather resistance.   | 1 - 2 hr touch<br>4 -6 hr recoat     |
| Dunn-Edwards<br>Athletic Field Striping W 5361                                     | Exterior             | 0                 | 37                   | 12-15 gal per field  | Produces a hard breathable film that is resistant to the blistering effects from the sun.   | 30 - 60 min touch<br>2 - 4 hr recoat |
| Dunn-Edwards<br>Dura-Tilt® Latex Tilt-Up Flat Plat W 6310                          | Exterior             | 35                | 36                   | 200-375              | Extremely flat finish that has excellent touch up, good hide and good alkali resistance.  | 20 - 30 min touch<br>1 - 2 hr recoat |
| Dunn-Edwards<br>Flex-Tex® Coating Fine W 320                                       | Exterior             | 50                | 49                   | 40-50                | Quality fine-textured coating that provides good flexibility and weather resistance.  | 1 - 2 hr touch<br>4 -6 hr recoat     |

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| <b>Flats (≤ 50 g/l)</b>  |                      |                   |                      |                      |  |                                      |
|--|----------------------|-------------------|----------------------|----------------------|--|--------------------------------------|
| Coating Company and Product Name   | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics  | Dry time                             |
| Dunn-Edwards Acri-Flat® Exterior Acrylic Wood Stain & Masonry Flat Paint W 704 V | Exterior             | 45                | 41                   | 300-400              | Provides dependable performance, excellent color retention and good grain-crack resistance for long term exterior durability.  | 1 - 2 hr touch<br>4 - 6 hr recoat    |
| Dunn-Edwards Quik-Wall® Interior Washable Latex Flat Paint W 6401                | Interior             | 50                | 43                   | 250-350              | Heavy bodied washable flat wall paint that offers good hide and very good touch up properties.   | 30 - 60 min touch<br>2 - 4 hr recoat |
| Dunn-Edwards Super-Wall® Interior Latex Flat Paint W 6402                        | Interior             | 50                | 35                   | 250-350              | Professional heavy bodied interior washable latex flat paint that provides excellent touch up and good hide.   | 30 - 60 min touch<br>2 - 4 hr recoat |
| Dunn-Edwards Flex-Tex® Elastomeric Coating Smooth W 321                          | Exterior             | 45                | 48                   | 75-100               | Quality, smooth elastomeric coating that provides very good flexibility alkali resistance.   | 1 - 2 hr touch<br>24 hr recoat       |
| Dunn-Edwards Super-Wall® Ready-To-Use Interior Latex Flat Paint W 6403           | Interior             | 50                | 30                   | 200-300              | Interior washable latex flat paint that provides excellent touch up and good hide.   | 30 - 60 min touch<br>2 - 4 hr recoat |
| Dunn-Edwards Exterior Paint Tan W 5995   | Exterior             | 35                | 36                   | 200-400              | Has good hide and applies easily.  | 20 - 30 min touch<br>1 - 2 hr recoat |
| Dunn-Edwards Ready-To-Use Nevada Ext Flat W 6267                                 | Exterior             | 40                | 33                   | 300-340              | Easy to apply, touches up well and provides good weather resistance.   | 2 hr touch<br>4 hr recoat            |
| Dunn-Edwards Walltone® Interior Latex Flat W 420                                 | Interior             | 35                | 36                   | 250-350              | Quality interior latex flat paint designed for use in apartments, condos, rental, and commercial properties that are repainted frequently.   | 30 - 60 min touch<br>2 - 4 hr recoat |
| Dunn-Edwards Exterior Paint Gray W 5996  | Exterior             | 30                | 38                   | 200-400              | Has good hide and applies easily.  | 20 - 30 min touch<br>1 - 2 hr recoat |
| Dunn-Edwards EnduraWall® Elastomeric Wall Coating Smooth W 370                   | Exterior             | 40                | 50                   | 40-100               | Provides superior protection against wind-driven rain, and moisture by bridging hairline cracks and other small cracks with outstanding resistance to ultra violet and dirt pick up, easy touched. | 1 - 2 hr touch<br>24 hr recoat       |
| Dunn-Edwards VersaFlat® Int/Ext Latex Flat Paint W 6240                          | Int/Ext              | 35                | 36                   | 200-375              | Extremely flat finish that has excellent touch up, good hide and good alkali resistance.   | 20 - 30 min touch<br>1 - 2 hr recoat |

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| <b>Flats (<math>\leq 50</math> g/l)</b>                                     |                      |                   |                      |                      |  |                                    |
|---|----------------------|-------------------|----------------------|----------------------|--|------------------------------------|
| Coating Company and Product Name  | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics  | Dry time                           |
| Dunn-Edwards Acoustikote® Latex Flat Ceiling Paint W 615                    | Interior             | 0                 | 34                   | 150-300              | Has a good hide and little effect upon the sound deadening qualities of acoustical surfaces. Applies easily and dries fast.  | .5 - 1 hr touch<br>1 - 2 hr recoat |
| Dunn-Edwards Ecoshield™ Low-Odor / Zero-VOC Interior Latex Flat Paint W 601 | Interior             | 10                | 40                   | 350-400              | Very low odor and no added solvents, provide a durable, washable film and has excellent hide and good adhesion. Applies easily and low odor.   | .5 - 1 hr touch<br>2 - 4 hr recoat |
| Duron Paints & Wall Coverings Genesis Odor Free Interior Acrylic Latex Flat | Interior             | 35                | 35                   | 400                  | Excellent hiding, easy to apply, resists household dirt, stain absorption & will withstand light to moderate hand washings.  | 30 min touch<br>4 hr recoat        |
| EVR-GARD Coatings 100 Vinyl Acrylic Int/Ext Flat                            | Int/Ext              | 0                 | 72                   | 200-350              | Economical product designed to cover most surfaces in one coat.  | 1 hr touch<br>4 - 6 hr recoat      |
| EVR-GARD Coatings 400 Elast-A-Bond Vinyl Acrylic Coatings                   | Int/Ext              | 0                 | 36                   | 200-400              | To resist blistering and peeling, but also exhibits extremely fine weather resistance. Superior hiding power, durability, ease of application and rapid drying.                                    | 1 hr touch<br>4 - 6 hr recoat      |
| Farrell-Calhoun, Inc. 200 Line 100% Acrylic Exterior Latex Flat House Paint | Exterior             | 52.7              | 41                   | 300-400              | Excellent flexibility & resistant to cracking, blistering, and mildew. Outstanding adhesion, color and gloss retention and blocking resistance.  | 30 min touch<br>2 - 4 hr recoat    |
| Farrell-Calhoun, Inc. 300 Line Interior Premium Flat Latex Wall Paint       | Interior             | 35                | 37                   | 300-400              | Soft pleasing appearance, unsurpassed washability and resistance. Outstanding touch-up.  | 30 min touch<br>4 hr recoat        |
| Farrell-Calhoun, Inc. 400 Line Vinyl Acrylic Interior Flat Latex Wall Paint | Interior             | 37                | 30                   | 300-400              | Superior hiding & ease of application. Outstanding touch-up. Good flow and leveling, low odor, non-splattering.  | 30 min touch<br>4 hr recoat        |
| Frazee Paint 018 Envirokote Interior Low Odor-Low VOC Flat Finish           | Interior             | <10               | 41                   | 200-400              | Top of the line interior flat paint ideal for use where low odor and reduced chemical exposure are desired.  | 30 min touch<br>3 - 4 hr recoat    |
| Fuhr ZVOC® Interior Acrylic Latex Paint 6100                                | Interior             | 0                 | 41                   | 100                  | Excellent wet adhesion, blister resistance, superior touch up qualities, along with a low, non-obtrusive odor & enamel holdout on wood, as well as great color retention and full scrub potential. | 20 min touch<br>30 min recoat      |
| Fuller O'Brien Crown Coat™ Interior-Exterior Flat Latex Finish FOB 802-10   | Int/Ext              | 18                | 24                   | 400                  | Self-sealing, has good touch-up and mild odor, and cleans up with water.   | 30 min touch<br>2 hr recoat        |

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| <b>Flats (≤ 50 g/l)</b>  |                      |                   |                      |                      |  |                                      |
|--|----------------------|-------------------|----------------------|----------------------|--|--------------------------------------|
| Coating Company and Product Name   | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics  | Dry time                             |
| Fuller O'Brien<br>Crown Coat™ Interior Flat<br>Latex Wall Paint FOB 600-XX | Interior             | 18                | 25                   | 350-400              | Excellent hiding properties & low odor. It is fast drying and has good washability and stain resistance.                                       | 30 min touch<br>2 - 4 hr recoat      |
| Hallman Lindsay<br>CLASSIC BUILDER<br>SKIM-KOTE Level 5 Surface<br>371     | Interior             | 21                | 59                   | 150                  | It provides an excellent primed surface or can be left unpainted on ceilings as a finish coat.   | 1 to 24 hr touch<br>2 - 24 hr recoat |
| Hallman Lindsay<br>CLASSIC BUILDER Smooth<br>Flat Hi-Build 353-2           | Interior             | 15                | 33                   | 160                  | Economical choice for either a one-coat prime and finish that provides a high-build finish with good touch-up and sealing properties.          | 1 hr touch<br>overnight recoat       |
| Hallman Lindsay<br>COMFORT KOTE Low-Odor<br>Latex Flat 261                 | Interior             | 3                 | 37                   | 350                  | Provides excellent hiding and touch-up in addition to good stain removal and washability where old odor is important.                          | 2 hr touch<br>4 hr recoat            |
| Hallman Lindsay<br>FARM & RANCH Acrylic Flat<br>Exterior 202               | Exterior             | 26                | 38                   | 400                  | High hiding, quality exterior finish featuring outstanding color retention, durability and shaking resistance.                                 | 1 hr touch<br>2-4 hr recoat          |
| Hallman Lindsay<br>MASONRY KOTE 100%<br>Acrylic Flat Masonry Paint 165     | Exterior             | 28                | 35                   | 400                  | Provides outstanding color and gloss retention, early moisture resistance and good mildew resistance.  | 1 hr touch<br>overnight recoat       |
| Hallman Lindsay<br>MASTER BUILDER Latex<br>Flat Wall Paint 364             | Interior             | 23                | 31                   | 350                  | Provides good coverage, appearance and application properties with high-hide and excellent touch up.   | 1 hr touch<br>4 hr recoat            |
| Hallman Lindsay<br>PRO HIDE Latex Flat Wall<br>Paint 269N                  | Interior             | 25                | 28                   | 400                  | High production flat coating with excellent touch-up designed for superior appearance and hiding.  | 1 hr touch<br>4 hr recoat            |
| Hallman Lindsay<br>PRO KOTE Latex Flat Wall<br>Paint 264                   | Interior             | 22                | 32                   | 400                  | Provides high-hiding finish with excellent touch-up when applied by brush, roll and/or spray.  | 1hr touch<br>4 hr recoat             |
| Hallman Lindsay<br>STRIPE KOTE Athletic Field<br>Marking 305               | Exterior             | 14                | 44                   | 250-300              | Mon-toxic, non-poisonous, non-irritating and harmless to grass or sod.   | 2 hr dry time                        |
| Hallman Lindsay<br>WOODTONE Acrylic Solid<br>Hide Stain 186                | Exterior             | 49                | 36                   | 400                  | Designed for both new and repaint work exhibiting outstanding color retention, blocks tannin discoloration, and resists mildew and blistering. | 2 hr touch<br>overnight recoat       |

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| <b>Flats (≤ 50 g/l)</b>  |                      |                   |                      |                      |   |                                 |
|--|----------------------|-------------------|----------------------|----------------------|---|---------------------------------|
| Coating Company and Product Name   | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics   | Dry time                        |
| ICI Glidden<br>MP 6400 Flat Latex Wall & Ceiling Paint                           | Interior             | 25                | 22                   | 400                  | Fast drying matte finish minimizes surface imperfections & offers one-coat possibilities.   | 30 min touch<br>2 hr recoat     |
| ICI Glidden<br>Professional Finishes Ultra-Build Interior Latex Flat GL8020      | Interior             | 36                | 15                   | 400                  | Easy to apply, dries in as little as 30 minutes to a smooth, uniform appearance.  | 30 min touch<br>2 hr recoat     |
| ICI Paints<br>Ultra-Wall® Latex Flat Interior Wall Paint 1230-xxxx               | Interior             | 50                | 28                   | 400                  | Designed as a high hiding product with very good touch-up when applied by brush roller or spray that forms a spatter free uniform finish.                             | 30 min touch<br>2 - 4 hr recoat |
| ICI Paints<br>Dulux® LIFEMASTER™ Flat Interior Latex Enamel 9100-xxxx            | Interior             | 0                 | 35                   | 400                  | Premium quality acrylic that brings increased washability and durable yet extremely uniform surfaces.   | 30 min touch<br>4 hr recoat     |
| ICI Paints<br>Speed-Wall® Latex Flat Interior Wall Paint 1250-xxxx               | Interior             | 18                | 25                   | 400                  | Delivers high production with excellent hide, easy application, quick drying and recoat when applied by brush, roller or spray.                                       | 30 min touch<br>2 hr recoat     |
| ICI Paints<br>Speed-Wall® Latex Matte Flat Interior Wall Paint 1251-xxxx         | Interior             | 33                | 25                   | 400                  | Delivers high production with good hide and excellent tough-up ability with easy application, quick drying and recoat.  | 30 min touch<br>2 hr recoat     |
| ICI Paints<br>Ultra-Hide® High-Build Latex Flat Interior Primer/Finish 1260-xxxx | Interior             | 46                | 32                   | 205-257              | Quickly and easily applied by airless spray and dries to a uniform flat finish which minimizes surface imperfections with excellent touch-up and superior uniformity. | 30 min touch<br>4 hr recoat     |
| ICI Paints<br>Ultra-Hide® Speed-Wall® Latex Flat Interior Wall Paint 6400-xxxx   | Interior             | 24                | 23                   | 400                  | Delivers high production with excellent hide, easy application, quick drying and recoat when applied by brush, roller or spray.                                       | 30 min touch<br>2 hr recoat     |
| ICI Paints<br>Speed-Cote™ Exterior Latex Flat Masonry Finish 2240-xxxx           | Exterior             | 22                | 24                   | 400-500              | Uniform flat finish, easy application, quick drying and recoat, low odor.   | 1-2 hr touch<br>4 hr recoat     |
| Kelly-Moore Paints™<br>119 KEL-PRO Interior Latex Flat Wall                      | Interior             | 39                | 27                   | 200-300              | Designed to provide an economical and decorative flat finish for wall and ceiling surfaces.   | 1 hr touch<br>4 hr recoat       |
| Kelly-Moore Paints™<br>1500 ENVIRO-COTE Interior Acrylic Flat Wall Paint         | Interior             | <15               | 42                   | 350-450              | A premium quality interior acrylic flat wall paint featuring low odor and low VOC.  | 1 hr touch<br>4 hr recoat       |

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| <b>Flats (<math>\leq 50</math> g/l)</b>  |                      |                   |                      |                      |   |                               |
|--|----------------------|-------------------|----------------------|----------------------|---|-------------------------------|
| Coating Company and Product Name   | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics   | Dry time                      |
| Kelly-Moore Paints™<br>485 EZY-COAT Interior Acrylic Flat Wall Paint                           | Interior             | 33                | 32                   | 250-350              | Designed to provide a decorative flat finish for interior wall and ceiling surfaces, excellent touch up and uniformity.                                   | 1 hr touch<br>4 hr recoat     |
| MAB Paints<br>Enviro-Pure Latex Flat   | Interior             | 10                | 40                   | 640                  | Designed for very low odor during application and drying and features water clean-up, two coat application in one day and self priming on drywall.        | 1 hr touch<br>5-6 hr recoat   |
| McCormick Paints<br>Natural Odor Free Interior Latex Flat Wall Paint 39 Series                 | Interior             | 0                 | 40                   | 400                  | This unique product technology is designed for painting in areas where minimal disruption of work or household routine is desired.                        | 30 min touch<br>4 hr recoat   |
| Miller Paint Co.<br>Super Premium Flat 4780  | Interior             | 46                | 34                   | 400-500              | High quality acrylic wall paint that offers an elegant finish formulated to give rich color and maximum coverage and hid.                                 | 30 min touch<br>4 hr recoat   |
| Miller Paint Co.<br>Acro Flat 6450   | Interior             | 0                 | 30                   | 300-350              | Formulated for exceptional wall coverage and durability. Acro is enhanced to fight the growth of mold, bacteria and mildew.                               | 30 min touch<br>4 hr recoat   |
| Miller Paint Co.<br>Acro Flat 6350   | Interior             | 0                 | 39                   | 300-350              | Formulated for exceptional wall coverage and durability. Acro is enhanced to fight the growth of mold, bacteria and mildew.                               | 30 min touch<br>4 hr recoat   |
| Miller Paint Co.<br>Premium Flat 3780  | Interior             | 48                | 33                   | 400-500              | This product offers an elegant finish with exceptional coverage, rich lasting color and very low odor.  | 30 min touch<br>4 hr recoat   |
| PPG Pittsburgh™ Paints<br>Builder's Spec™ High Build Interior Flat Latex 57-610 Series         | Interior             | 32                | 28                   | 400-500              | Formulated to meet the application and touch-up requirements of the new home construction market. Excellent dry hide.                                     | 30 min touch<br>4 hr recoat   |
| PPG Pittsburgh™ Paints<br>Interior Hi Build Touch Up Flat Pastel UC65307                       | Interior             | 17                | 28                   | 400-500              | High build finish, good touch up, soap and water clean-up.  | 4 hr recoat<br>30 days recoat |
| PPG Pittsburgh™ Paints<br>Pure Performance® Interior Flat Latex 9-100 Series                   | Interior             | 0                 | 40                   | 350-400              | It is formulated to provide excellent hiding, touch up and application properties in addition to minimal odor, zero VOC's, and anti-microbial properties. | 1 hr touch<br>4 hr recoat     |
| PPG Pittsburgh™ Paints<br>Speed Finish Plus™ Interior Flat Wall and Ceiling Paint 8-112 Series | Interior             | 47                | 30                   | 350-450              | Designed as a good-hiding latex paint with excellent touch-up properties.   | 30 min touch<br>4 hr recoat   |

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| <b>Flats (<math>\leq 50</math> g/l)</b>   |                      |                   |                      |                      |  |                             |
|---|----------------------|-------------------|----------------------|----------------------|--|-----------------------------|
| Coating Company and Product Name  | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics  | Dry time                    |
| PPG Pittsburgh™ Paints Speedcraft® Interior Wall & Ceiling Flat Latex 5-70 Series   | Interior             | 32                | 29                   | 400-500              | It has good adhesion, application and touch-up properties on walls, ceilings and trim surfaces.  | 30 min touch<br>4 hr recoat |
| PPG Pittsburgh™ Paints SpeedPro® Interior Wall & Ceiling Flat Latex 14-110 Series   | Interior             | 38                | 28                   | 400-500              | Formulated to be used in commercial markets where application speed and good quality are needed.   | 30 min touch<br>4 hr recoat |
| PPG Pittsburgh™ Paints Speedhide® Ultra Interior Wall Flat Latex 100% Acrylic 6-700 | Interior             | 51                | 34                   | 350-400              | Designed as a high hiding product with excellent touch-up properties. The uniform, flat finish has excellent scrubability and stain resistance.          | 30 min touch<br>4 hr recoat |
| PPG Pittsburgh™ Paints Interior Ceiling Paint Flat Latex 50-35                      | Interior             | 42                | 29                   | 400-500              | A high hiding latex designed specifically for finishing interior ceilings.   | 30 min touch<br>4 hr recoat |
| PPG Pittsburgh™ Paints Speedhide® Interior Fire Retardant Flat Latex 42-7           | Interior             | 32                | 50                   | 150-335              | It is formulated to meet the performance requirements of professional application. The paint film intumesces when exposed to flame or high temperatures. | 30 min touch<br>4 hr recoat |
| PPG Pittsburgh™ Paints Speedhide® Interior Low Odor Wall Flat Latex UC80021         | Interior             | 17                | 31                   | 400-500              | Ideal for use anywhere that odor is a concern during application and drying; it has excellent hiding and excellent touch-up properties.                  | 30 min touch<br>4 hr recoat |
| PPG Pittsburgh™ Paints Speedhide® Interior Wall Flat Latex 6-70 Series              | Interior             | 24                | 32                   | 400-500              | An excellent hiding latex with excellent touch-up properties that dries to a flat finish to help hide tape joints and surface imperfections              | 30 min touch<br>4 hr recoat |
| PPG Pittsburgh™ Paints GLB2005 Interior Flat Wall and Ceiling Paint                 | Interior             | 48                | 34                   | 300-440              | An excellent hiding latex with superior touch-up properties that dries to a dead flat finish to help hide tape joints and surface imperfections.         | 30 min touch<br>4 hr recoat |
| Rodda Paint Interior Flat Wall Paint - White Base 33663                             | Interior             | 46                | 35                   | 300                  | A flat finish, latex resin emulsion formulated to protect and beautify interior surfaces.  | 1.5 hr touch<br>2 hr recoat |
| Rodda Paint Horizon Flat Interior Wall Paint 513501                                 | Interior             | <5                | 40                   | 320                  | Provides a durable, low odor / low VOC enamel finish; has very low odor during application and drying  | 30 min touch<br>2 hr recoat |
| Sherwin Williams® Duration® Interior Latex Matte A96-100 Series                     | Interior             | 37                | 40                   | 350-400              | Low odor, low VOC coating stands up to the wear and tear of daily lining and high traffic areas.   |                             |

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| <b>Flats (<math>\leq 50</math> g/l)</b>                                |                      |                   |                      |                      |  |                             |
|--|----------------------|-------------------|----------------------|----------------------|--|-----------------------------|
| Coating Company and Product Name                                       | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics  | Dry time                    |
| Sherwin Williams® Harmony® Interior Latex Flat B5 Series               | Interior             | 0                 | 42                   | 350-400              | Provides a durable, low-odor, antimicrobial, interior paint formulated without silica.   | 1 hr touch<br>4 hr recoat   |
| Sherwin Williams® #6057 ISOWALL Interior Latex Washable Flat Paint     | Interior             | 48                | 32                   | 200                  | Provides a heavy bodied, self-primed, waterborne flat designed to hide wall imperfections and give good durability.              | 30 min touch<br>2 hr recoat |
| Sherwin Williams® AcryShell 100% Acrylic Exterior Latex Flat B42WT6007 | Exterior             | 42                | 29                   | 400                  | AcryShell is ideal for professional use.   | 1 hr touch<br>4 hr recoat   |
| Sherwin Williams® CAL-SCRUB Interior Scrubbable Flat B30WJ551          | Interior             | 50                | 38                   | 400                  | An upgraded interior flat wit exceptional scrub resistance.  | 1 hr touch<br>4 hr recoat   |
| Sherwin Williams® ColorAccents™ Interior Latex Flat Y10 Series         | Interior             | 50                | 34                   | 350-400              | Provides bright and deep colors for walls, trim, or ceilings with superior resistance to burnishing and marring.                 | 1 hr touch<br>4 hr recoat   |
| Sherwin Williams® ProMar™ 700 Interior Latex Flat B30W7700             | Interior             | 41                | 26                   | 350-400              | Economical, interior latex flat wall paint .   | 1 hr touch<br>4 hr recoat   |
| Sherwin Williams® ProTouch™ Interior Latex Flat B30W351                | Interior             | 49                | 31                   | 350-400              | This product provides good washability and durability as well as excellent touch-up.   | 1 hr touch<br>4 hr recoat   |
| Surface Protection Industries High Hide Set White 5006-0001            | Interior             | <50               |                      | 250-400              | Formulated to provide excellent hiding and tinting, with good adhesion, hold out and toughness.                                  | 30 min recoat               |
| Surface Protection Industries Studio White 5050-1                      | Int/Ext              | 14                |                      | 250-400              | Provides excellent whiteness and very good hide with toughness, adhesion, hold-out, controlled penetration and color acceptance. | 30 min recoat               |
| Surface Protection Industries Vara-Bond Series 85                      | Int/Ext              | 8                 |                      | 250-400              | Versatile paint formulated to be tough, durable and economical; weather resistant, moisture and permeable.                       | 30 min recoat               |
| Surface Protection Industries Vara-Bond Water Base Flat Latex 8507-00  | Int/Ext              | 11                |                      | 250-400              | Versatile paint formulated to be tough, durable and economical; weather resistant, moisture permeable and elastic.               | 30 min recoat               |

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| <b>Flats (<math>\leq 50</math> g/l)</b>                       |                      |                   |                      |                      |   |                               |
|---|----------------------|-------------------|----------------------|----------------------|---|-------------------------------|
| Coating Company and Product Name                              | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics   | Dry time                      |
| Surface Protection Industries<br>VYN-WALL 69-01               | Interior             | 14                |                      | 250-350              | Combines quality and moderate coat with good film toughness, excellent coverage and adhesion to many surfaces.  | 30 min recoat                 |
| Teifs Professional Coatings<br>PC1100 Interior Flat Wall #335 | Interior             | 19                |                      | 350-400              | Interior flat latex designed for the professional contractor. Provides performance.   | 1 hr touch<br>4 hr recoat     |
| Tibbetts - Newport Corp.<br>900 Acra Kote Flat                | Int/Ext              | 35                |                      | 300-350              | Provides excellent hide, washability, spot resistance and easy application.   | 1 hr touch<br>2 hr recoat     |
| Tibbetts - Newport Corp.<br>1500 WALL KOTE                    | Interior             | 15                |                      | 300-400              | Offers an economical and durable finish with fast dry with good washable properties   | 1 - 2 hr touch<br>4 hr recoat |
| Tibbetts - Newport Corp.<br>1900 ACRA-VEL                     | Interior             | <50               |                      | 300-400              | Velvet flat finish with fast drying and good washable properties offering a long lasting low maintenance finish.  | 1 - 2 hr touch<br>4 hr recoat |
| Tibbetts - Newport Corp.<br>3600 DECOBOND                     | Int/Ext              | <50               |                      | 300-400              | Offers an economical and durable finish with good hide and easy application   | 1 hr recoat                   |
| Tibbetts - Newport Corp.<br>Permanox Stain Flat               | Exterior             | 7                 |                      | 300-350              | Delivers maximum protection with a breathable finish that applies easily, dries fast and cleans-up easily with water  | 2 - 4 hr touch<br>4 hr recoat |
| Vista Paint<br>1000 Duraglide                                 | Int/Ext              | 50                | 41.8                 | 300-400              | A fortified vinyl acrylic exterior and interior flat. Excellent touch-up, outstanding hid and good washability.   | 1 hr touch<br>4 hr recoat     |
| Vista Paint<br>2000 Duratone                                  | Exterior             | 17                | 43.6                 | 350-420              | 100% acrylic exterior flat that produces a tough flexible film with outstanding resistance to fading and chalking.  | 1 hr touch<br>4-6 hr recoat   |
| Vista Paint<br>6100 Carefree Earth Coat Flat                  | Interior             | 2                 | 40                   | 350-400              | Environmentally preferable odor free, low VOC interior acrylic flat with exceptional hide, touch-up with superior adhesion, resistant to scuffing, staining and abrasion. | 45 min touch<br>6 hr recoat   |
| Vista Paint<br>2800 Coverall Exterior Flat                    | Exterior             | 46                | 42                   | 300-400              | Provides a tough, flexible matte flat finish with outstanding resistance to chalking and fading.  | 1 hr touch<br>4 hr recoat     |

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| <b>Flats (<math>\leq 50</math> g/l)</b>       |                      |                   |                      |                      |  |                             |
|---|----------------------|-------------------|----------------------|----------------------|--|-----------------------------|
| Coating Company and Product Name              | Interior<br>Exterior | VOC content (g/l) | Solids (% by volume) | Coverage (sq ft/gal) | Coating Characteristics  | Dry time                    |
| Vista Paint<br>3600 Coverall Maintenance Flat | Interior             | 49                | 38                   | 350-500              | Provides an outstanding hide, coupled with excellent touch-up characteristics. | 1 hr touch<br>2 hr recoat   |
| Vista Paint<br>013Acoustic Kote               | Interior             | 31                | 29                   | 50-400               | A high-hiding, non-bridging vinyl flat for acoustical ceilings.                | 30 min touch<br>4 hr recoat |
| Vista Paint<br>RC10 Latex Roll Coat           | Interior             | 26                | 37                   | 600                  | Water-based latex, very low VOC formulated for roll coating applications.      | 45 -60 min dry time         |

## APPENDIX B

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UMR Coatings Institute - Flat Coating Laboratory Performance Study

**FINAL REPORT**  
**Flat Coatings Technology Assessment**

**RFP # P2007-22**

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# Executive Summary

## Introduction

This study was a critical component of the ongoing technology assessment for Rule 1113 – Architectural Coatings. The assurance that performance of paints is not hindered by lower VOC requirements is an important aspect of the rule. Of particular interest were the physical properties of twenty flat coatings in interior and exterior paint categories. Nine interior, nine exterior, and two interior/exterior coatings were tested. A series of general tests for all the paints and some specific tests for the two categories were performed.

## Task 1 - Testing Protocol

### Tests for General Properties of All Paints

| Property               | Standard             | Number of Replicates | Substrate   | Film Thickness/ Bar Type |
|------------------------|----------------------|----------------------|-------------|--------------------------|
| Appearance             | Observation          | 1 gallon as received | -----       | -----                    |
| Gloss                  | ASTM D523-89         | 2                    | Leneta Card | 3mil/Bird bar            |
| Stability              | ASTM D1849-95        | 1                    | N/A         | 3mil/Bird bar            |
| Stability - Syneresis  | Rohm&Haas Method 807 | 3                    | N/A         | N/A                      |
| Open Time/Wet Edge     | Rohm&Haas Method 301 | 3                    | Plastic     | 7 mil/Dow bar            |
| Freeze-Thaw Resistance | ASTM D2243-95        | 3                    | Leneta Card | 3 mil/Bird bar           |
| Flow & Leveling        | ASTM D 4062-99       | 3                    | Leneta Card | NPCA bar                 |
| Sag Resistance         | ASTM D4400-99        | 3                    | Leneta Card | Anti-sag meter           |
| Dry Time - Mechanical  | ASTM D5895-03        | 3                    | Glass       | 3mil Cube Applicator     |
| Hide                   | Spectrophotometer    | 3                    | Leneta Card | 3mil/Bird bar            |

### Tests for Interior Flat Paints

| Property         | Standard        | Number of Replicates | Substrate   | Film Thickness/ Bar type |
|------------------|-----------------|----------------------|-------------|--------------------------|
| Adhesion         | ASTM D 3359     | 3                    | Leneta Card | 3mil/Bird bar            |
| Scrub Resistance | ASTM D2486-00   | 3                    | Plastic     | 7 mil/Dow bar            |
| Stain Resistance | ASTM D4828 mod. | 3                    | Plastic     | 7 mil/Dow bar            |
| Touch-Up         | ASTM D 3928     | 3                    | Drywall     | Brush/Roller             |

### Tests for Exterior Flat Paints

| Property              | Standard                    | Number of Replicates | Substrate | Film Thickness/ Bar type |
|-----------------------|-----------------------------|----------------------|-----------|--------------------------|
| Adhesion              | ASTM D 3359                 | 3                    | Glass     | 3mil/Bird bar            |
| Tannin Stain Blocking | Prior SCAQMD Study Protocol | 3                    | Cedar     | Brush                    |
| Alkalinity Resistance | Dunn Edwards Method         | 3                    | Concrete  | Brush                    |

## Tests for General Properties Summary

Appearance – The coatings were evaluated upon receipt for general appearance including odor of spoilage, skinning, pressure, can corrosion, etc.

### Appearance Summary

|   | <b>Observations – 1 gallon can as received:<br/>Notes on Odor, Skinning, Pressure, Can Corrosion</b> |
|---|--|
| A | None   |
| B | Very Trace Can Corrosion   |
| C | None   |
| D | None   |
| E | None   |
| F | None   |
| G | Trace Can Corrosion  |
| H | Very Slight Separation   |
| I | None   |
| J | None   |
| K | None   |
| L | None   |
| M | 1 ¾ inch medium yellow separation layer with darker spots  |
| N | None   |
| O | None   |
| P | None   |
| Q | None   |
| R | Very Slight Separation   |
| S | Trace Can Corrosion  |
| T | None   |

Gloss – ASTM D 523 was used with a BYK-Gardner micro-TRI-gloss meter calibrated just prior to use. Measurements were taken for 60° and 85°.

Gloss Summary\*

|     | <b>60°Mean</b> | <b>60°SD</b> | <b>85°Mean</b> | <b>85°SD</b> |
|-----|----------------|--------------|----------------|--------------|
| A   | 1.9            | 0.1          | 0.8            | 0.1          |
| B   | 2.7            | 0.1          | 2.2            | 0.1          |
| C   | 2.3            | 0.1          | 2.5            | 0.1          |
| D   | 2.1            | 0.1          | 1.6            | 0.1          |
| E** | 8.7            | 0.1          | 28.0           | 0.2          |
| F   | 2.5            | 0.1          | 2.7            | 0.1          |
| G   | 1.7            | 0.1          | 0.6            | 0.1          |
| H   | 1.9            | 0.1          | 1.1            | 0.1          |
| I   | 2.0            | 0.1          | 1.0            | 0.1          |
| J   | 2.5            | 0.1          | 4.4            | 0.1          |
| K   | 2.0            | 0.1          | 2.0            | 0.1          |
| L   | 2.1            | 0.1          | 3.2            | 0.1          |
| M   | 1.9            | 0.1          | 1.1            | 0.1          |
| N   | 2.3            | 0.1          | 4.9            | 0.1          |
| O   | 2.0            | 0.1          | 2.4            | 0.1          |
| P   | 2.3            | 0.1          | 2.3            | 0.1          |
| Q   | 2.1            | 0.1          | 2.8            | 0.1          |
| R   | 3.0            | 0.1          | 1.3            | 0.1          |
| S   | 2.3            | 0.1          | 1.9            | 0.1          |
| T   | 1.9            | 0.1          | 1.3            | 0.1          |

\*Average values

\*\*The gloss readings for coating E exceed the Rule 1113 definition of a flat coating therefore, according to the Rule 1113, this coating is considered a non-flat coating and the data concerning this coating is not applicable to the flat coatings study.

Stability – ASTM D 1849 was used with one pint sample of each being kept at 125 °F for 30 days, followed by evaluation as indicated in the ASTM method. Gloss measurements were also taken of the samples during evaluation. The change in viscosity of the samples was rated from 0-10 with rating of 0, 2, 4, 6, 8, and 10 for changes in viscosity (KU) of 10 or higher, 8, 6, 4, 2, and 0 respectively. The overall character (separation, skinning, pressure, can corrosion, and odor of spoilage) of the coating was also put into a 0-10 scale with ratings of 0, 2, 4, 6, 8, and 10 for complete failure, considerable, moderate, slight, very slight, and none, respectively.

Stability Summary

|   | <b>Stormer<br/>(original)</b> | <b>Stormer<br/>(post-test)</b> | <b>Viscosity<br/>Rating</b> | <b>Overall Character<br/>Rating</b> | <b>Character</b>               |
|---|-------------------------------|--------------------------------|-----------------------------|-------------------------------------|--------------------------------|
| A | 97                            | 101                            | 6                           | 8                                   | Separation - spots             |
| B | 94                            | 96                             | 8                           | 6                                   | Separation – thin layer < 1/8” |
| C | 102                           | 114                            | 0                           | 8                                   | Separation – spots             |
| D | 101                           | 103                            | 8                           | 8                                   | Separation - spots             |
| E | 103                           | 108                            | 5                           | 4                                   | Separation – ¼” layer          |
| F | 108                           | 114                            | 4                           | 8                                   | Separation – spots             |
| G | 115                           | 115                            | 10                          | 6                                   | Separation – thin layer < 1/8” |
| H | 104                           | 103                            | 9                           | 6                                   | Separation – thin layer < 1/8” |
| I | 100                           | 102                            | 8                           | 6                                   | Separation – thin layer < 1/8” |
| J | 95                            | 104                            | 1                           | 10                                  | No failure                     |
| K | 110                           | 120                            | 0                           | 8                                   | Separation – spots             |
| L | 107                           | 124                            | 0                           | 6                                   | Separation – thin layer < 1/8” |
| M | 100                           | 101                            | 9                           | 4                                   | Separation – ¼” layer          |
| N | 102                           | 101                            | 9                           | 6                                   | Separation – thin layer < 1/8” |
| O | 97                            | 94                             | 7                           | 6                                   | Separation – thin layer < 1/8” |
| P | 102                           | 104                            | 8                           | 4                                   | Separation – ¼” layer          |
| Q | 109                           | 112                            | 7                           | 6                                   | Separation – thin layer < 1/8” |
| R | 117                           | 126                            | 1                           | 6                                   | Separation – thin layer < 1/8” |
| S | 99                            | 94                             | 5                           | 6                                   | Separation – thin layer < 1/8” |
| T | 99                            | 100                            | 9                           | 4                                   | Separation – ¼” layer          |

Stability Summary - Gloss Measurements (Before/After)

|   | <b>60°Mean</b> | <b>60 SD</b> | <b>85°Mean</b> | <b>85 SD</b> |
|---|----------------|--------------|----------------|--------------|
| A | 1.9 / 1.9      | 0.1 / 0.1    | 0.8 / 0.8      | 0.1 / 0.1    |
| B | 2.7 / 2.6      | 0.1 / 0.1    | 2.2 / 2.3      | 0.1 / 0.1    |
| C | 2.3 / 2.3      | 0.1 / 0.1    | 2.5 / 2.7      | 0.1 / 0.1    |
| D | 2.1 / 2.1      | 0.1 / 0.1    | 1.6 / 1.7      | 0.1 / 0.1    |
| E | 8.7 / 9.7      | 0.1 / 0.2    | 28.0 / 29.3    | 0.2 / 0.2    |
| F | 2.5 / 2.5      | 0.1 / 0.1    | 2.7 / 2.8      | 0.1 / 0.1    |
| G | 1.7 / 1.7      | 0.1 / 0.1    | 0.6 / 0.6      | 0.1 / 0.1    |
| H | 1.9 / 1.9      | 0.1 / 0.1    | 1.1 / 1.0      | 0.1 / 0.1    |
| I | 2.0 / 2.0      | 0.1 / 0.1    | 1.0 / 0.9      | 0.1 / 0.1    |
| J | 2.5 / 2.4      | 0.1 / 0.1    | 4.4 / 4.7      | 0.1 / 0.2    |
| K | 2.0 / 2.1      | 0.1 / 0.1    | 2.0 / 2.0      | 0.1 / 0.1    |
| L | 2.1 / 2.1      | 0.1 / 0.1    | 3.2 / 3.2      | 0.1 / 0.1    |
| M | 1.9 / 2.0      | 0.1 / 0.1    | 1.1 / 1.3      | 0.1 / 0.1    |
| N | 2.3 / 2.2      | 0.1 / 0.1    | 4.9 / 5.0      | 0.1 / 0.1    |
| O | 2.0 / 2.0      | 0.1 / 0.1    | 2.4 / 2.4      | 0.1 / 0.1    |
| P | 2.3 / 2.3      | 0.1 / 0.1    | 2.3 / 2.4      | 0.1 / 0.1    |
| Q | 2.1 / 2.1      | 0.1 / 0.1    | 2.8 / 2.8      | 0.1 / 0.1    |
| R | 3.0 / 2.9      | 0.1 / 0.1    | 1.3 / 1.3      | 0.1 / 0.1    |
| S | 2.3 / 2.3      | 0.1 / 0.1    | 1.9 / 2.0      | 0.1 / 0.1    |
| T | 1.9 / 1.9      | 0.1 / 0.1    | 1.3 / 1.3      | 0.1 / 0.1    |

Stability – Syneresis – Rohm&Haas Method 807 was used. 40mm pieces of graph paper were attached to the back of 1 oz. vials and the vials were filled with paint to the top of the graph paper. The vials were put in an oven at 60 °C (140 °F) for 10 days and the separation and settling were evaluated. The separation was evaluated by measuring the clear liquid on top of the coating in mm and putting these values into a 0-10 scale in which the ratings are 0, 2, 4, 6, 8, and 10 for 10mm, 8mm, 6mm, 4mm, 2mm, and 0mm, respectively.

Stability – Colorant/pigment float – Syneresis\*

|   | Separation, mm | Rating | Settling         |
|---|----------------|--------|------------------|
| A | 0.75           | 9      | None             |
| B | 1.0            | 9      | Soft Pack        |
| C | 0.5            | 9      | Hard Pack        |
| D | 1.0            | 9      | Soft Pack        |
| E | 2.0            | 8      | <i>Soft Pack</i> |
| F | 0.5            | 9      | Soft Pack        |
| G | 1.0            | 9      | Soft Pack        |
| H | 1.0            | 9      | Soft Pack        |
| I | 0.5            | 9      | Soft Pack        |
| J | 1.0            | 9      | Hard Pack        |
| K | 2.0            | 8      | Soft Pack        |
| L | 2.0            | 8      | Hard Pack        |
| M | 1.0            | 9      | None             |
| N | 1.0            | 9      | Soft Pack        |
| O | 2.0            | 8      | Soft Pack        |
| P | 1.0            | 9      | Soft Pack        |
| Q | 1.0            | 9      | Soft Pack        |
| R | 0.5            | 9      | Soft Pack        |
| S | 1.0            | 9      | None             |
| T | 1.0            | 9      | None             |

\*Average Values

Open Time/Wet Edge – Rohm&Haas Method 301A was used. The coatings were drawdown on plastic scrub panels and horizontal squiggles were made at 2 minute intervals. The squiggle was painted over with a set number of strokes (5 full) immediately after being made and the panels were allowed to dry 24 hours before evaluation to determine which squiggle was first visible. The time before the squiggle was first visible was recorded. A 0-10 rating system was then applied to the results with ratings of 0, 2, 4, 6, 8, and 10 for 0 minutes, 2, 4, 6, 8, and 10 minutes, respectively.

Open Time/ Wet Edge Summary\*

|   | Last Non-Visible Squiggle Time, min | Rating |
|---|-------------------------------------|--------|
| A | 14                                  | 10+    |
| B | 10                                  | 10     |
| C | 12                                  | 10+    |
| D | 15                                  | 10+    |
| E | 15                                  | 10+    |
| F | 14                                  | 10+    |
| G | 13                                  | 10+    |
| H | 16                                  | 10+    |
| I | 13                                  | 10+    |
| J | 11                                  | 10+    |
| K | 12                                  | 10+    |
| L | 12                                  | 10+    |
| M | 12                                  | 10+    |
| N | 13                                  | 10+    |
| O | 9                                   | 9      |
| P | 8                                   | 8      |
| Q | 8                                   | 8      |
| R | 8                                   | 8      |
| S | 10                                  | 10     |
| T | 14                                  | 10+    |

\*Average Values

Freeze-thaw Resistance – ASTM D 2243 was used for the water-borne paints for three samples of each with the paints applied to black and white Leneta charts after each of the five cycles. A cycle was defined according to the ASTM method. Viscosity and gloss measurements were taken of the sample after each cycle, as long as it had not failed. The overall results were fitted into a 0-10 scale with ratings of 0, 2, 4, 6, 8, and 10 for 0 cycles passed, 1, 2, 3, 4, and 5 cycles passed, respectively.

Freeze-Thaw Resistance: Pass/Fail Summary

|   | After 1<br>Cycle | After 2<br>Cycles | After 3<br>Cycles | After 4<br>Cycles | After 5<br>Cycles | Rating |
|---|------------------|-------------------|-------------------|-------------------|-------------------|--------|
| A | Pass             | Pass              | Pass              | Pass              | Pass              | 10     |
| B | Pass             | Pass              | Pass              | Pass              | Pass              | 10     |
| C | Fail             | -----             | -----             | -----             | -----             | 0      |
| D | Pass             | Pass              | Pass              | Pass              | Pass              | 10     |
| E | <i>Fail</i>      | -----             | -----             | -----             | -----             | 0      |
| F | Fail             | -----             | -----             | -----             | -----             | 0      |
| G | Pass             | Fail              | -----             | -----             | -----             | 2      |
| H | Pass             | Pass              | Pass              | Pass              | Fail              | 8      |
| I | Pass             | Pass              | Pass              | Pass              | Pass              | 10     |
| J | Fail             | -----             | -----             | -----             | -----             | 0      |
| K | Pass             | Fail              | -----             | -----             | -----             | 2      |
| L | Fail             | -----             | -----             | -----             | -----             | 0      |
| M | Fail             | -----             | -----             | -----             | -----             | 0      |
| N | Fail             | -----             | -----             | -----             | -----             | 0      |
| O | Fail             | -----             | -----             | -----             | -----             | 0      |
| P | Fail             | -----             | -----             | -----             | -----             | 0      |
| Q | Fail             | -----             | -----             | -----             | -----             | 0      |
| R | Fail             | -----             | -----             | -----             | -----             | 0      |
| S | Fail             | -----             | -----             | -----             | -----             | 0      |
| T | Fail             | -----             | -----             | -----             | -----             | 0      |

\*Average values

Flow & Leveling – ASTM D 4062 was used. This is an old ASTM method that is analogous to the New York Society for Paint Technology “Official Digest” No. 44 Vol. 32, No. 430, p. 1435. The NYPC Level Blade was used.

Sag Resistance – ASTM D4400 was used. An anti-sag bar was used to apply paint to a black and white Leneta chart. This bar deposits strips of paint from 3 to 12 mils thick approximately ½” wide. The chart was immediately lifted to a vertical position with the 12 mil thick strip at the bottom. Evaluation was based upon how much the strips flow into the strips below.

Flow & Leveling and Sag are often used in conjunction to help gauge the application performance of a coating, often for vertical wall applications, although Flow & Leveling is also important for coatings for horizontal applications such as floors. Flow & Leveling represents short term and Sag represents a longer time effect. Flow & Leveling ratings represent a coatings ability to reduce the appearance of brush strokes and similar marks by flowing from the thicker areas to the adjacent thinner areas. Sag Resistance gauges how thick a coating can be applied before the coating shifts and causes visual defects. Typically, flat coatings are applied to about 3mil dry film, but sometimes thicker, so the coating needs to be able to withstand 6-8 wet mils before sagging to ensure that there will be no sagging of the coating in the desired application thickness range. Sag Resistance values are the highest mil thickness that can be applied without the coating sagging.

Flow/Level and Sag Resistance Summary\*

|   | <b>Flow/Level</b> | <b>Sag</b> |
|---|-------------------|------------|
| A | 0                 | 12+        |
| B | 0                 | 12+        |
| C | 0                 | 12+        |
| D | 0                 | 12+        |
| E | 0                 | 12+        |
| F | 0                 | 12+        |
| G | 0                 | 12+        |
| H | 0                 | 12+        |
| I | 0                 | 12+        |
| J | 5                 | 10         |
| K | 1                 | 12+        |
| L | 0                 | 12+        |
| M | 0                 | 12+        |
| N | 0                 | 12+        |
| O | 3                 | 12+        |
| P | 0                 | 12+        |
| Q | 0                 | 12+        |
| R | 0                 | 12+        |
| S | 0                 | 12+        |
| T | 0                 | 12+        |

\*Average values

Mechanical Dry Time – ASTM D 5895 was used to determine dry time with a mechanical straight line drying time recorder.

Mechanical Dry Time Summary (in minutes)\*

|   | Set-Touch | Tack-Free | Dry-Hard | Dry-Through |
|---|-----------|-----------|----------|-------------|
| A | 6         | 10        | 24       | > 6 Hours   |
| B | 3         | 12        | 22       | > 6 Hours   |
| C | 5         | 12        | 43       | > 6 Hours   |
| D | 8         | 14        | 36       | > 6 Hours   |
| E | 4         | 10        | 23       | > 6 Hours   |
| F | 2         | 4         | 23       | > 6 Hours   |
| G | 10        | 18        | 26       | > 6 Hours   |
| H | 6         | 15        | 19       | > 6 Hours   |
| I | 1         | 9         | 12       | > 6 Hours   |
| J | 2         | 7         | 19       | > 6 Hours   |
| K | 6         | 11        | 58       | > 6 Hours   |
| L | 1         | 4         | 6        | > 6 Hours   |
| M | 2         | 6         | 113      | > 6 Hours   |
| N | 6         | 12        | 14       | > 6 Hours   |
| O | 5         | 8         | 40       | > 6 Hours   |
| P | 4         | 7         | 14       | > 6 Hours   |
| Q | 3         | 5         | 8        | > 6 Hours   |
| R | 1         | 8         | 20       | > 6 Hours   |
| S | 3         | 8         | 12       | > 6 Hours   |
| T | 2         | 5         | 66       | > 6 Hours   |

\*Average values; times in minutes; stylus diameter = 1mm; speed = 6 hours

Hide – For dry hide and gloss, a three-mil Bird bar was used to apply paint to three black and white Leneta charts. The color was measured using a Minolta CM-2002 spectrophotometer and the CIE XYZ value for Y was recorded. The Y values over the white section and the black section were used to calculate dry hide. Due to Beer’s and Lambert’s Law, hide increases as film thickness increases. Hide also increases as concentration of hiding pigments increases. A 0-10 rating scale was applied to the contrast ratios with ratings of 0, 2, 4, 6, 8, and 10 being contrast ratios of 0.95, 0.96, 0.97, 0.98, 0.99, and 1.00, respectively.

Hide Summary – Contrast Ratio\*

|   | 3 mil #1 | 3 mil #2 | 3 mil #3 | Average | Rating |
|---|----------|----------|----------|---------|--------|
| A | 0.976    | 0.976    | 0.975    | 0.976   | 6      |
| B | 0.974    | 0.976    | 0.977    | 0.976   | 6      |
| C | 0.980    | 0.979    | 0.980    | 0.980   | 6      |
| D | 0.979    | 0.976    | 0.979    | 0.978   | 6      |
| E | 0.996    | 0.999    | 0.998    | 0.998   | 10     |
| F | 0.992    | 0.994    | 0.994    | 0.993   | 8      |
| G | 0.966    | 0.967    | 0.964    | 0.966   | 4      |
| H | 0.982    | 0.983    | 0.981    | 0.982   | 6      |
| I | 0.976    | 0.977    | 0.977    | 0.976   | 6      |
| J | 0.985    | 0.986    | 0.987    | 0.986   | 8      |
| K | 0.979    | 0.980    | 0.979    | 0.980   | 6      |
| L | 0.981    | 0.980    | 0.979    | 0.980   | 6      |
| M | 0.981    | 0.982    | 0.983    | 0.982   | 6      |
| N | 0.984    | 0.986    | 0.987    | 0.986   | 8      |
| O | 0.982    | 0.982    | 0.983    | 0.982   | 6      |
| P | 0.983    | 0.982    | 0.983    | 0.983   | 6      |
| Q | 0.984    | 0.983    | 0.984    | 0.983   | 6      |
| R | 0.988    | 0.988    | 0.988    | 0.988   | 8      |
| S | 0.978    | 0.978    | 0.977    | 0.978   | 6      |
| T | 0.970    | 0.969    | 0.969    | 0.970   | 4      |

\*Average values

### Tests for Interior Flat Paints Summary

Adhesion – ASTM D 3359-Method B was used to determine adhesion of a 3mil drawdown on a Leneta chart. This method used a cutting tool and 3mm cutting guide to make a series of perpendicular cuts in the surface. Pressure sensitive tape in accordance with the ASTM procedure was then applied and removed after 90 seconds and the adhesion was qualitatively analyzed based on how much coating was removed by the tape. The ASTM classification of 0B-5B was put into a rating system of 0-5, respectively, with 5 being 0% removed and a 0 being greater than 65% removed.

Adhesion (on Leneta chart)\*

|   | <b>ASTM Rating</b> | <b>% Failure</b> | <b>Failure Mechanism</b> | <b>AQMD Rating</b> |
|---|--------------------|------------------|--------------------------|--------------------|
| J | 4B                 | 3.5              | Substrate                | 4                  |
| K | 4B                 | 13.3             | Substrate                | 4                  |
| L | 3B                 | 6.7              | Substrate                | 3                  |
| M | 5B                 | 0.2              | Substrate                | 5                  |
| N | 4B                 | 8.5              | Substrate                | 4                  |
| O | 3B                 | 6.0              | Adhesion                 | 3                  |
| P | 3B                 | 6.7              | Adhesion                 | 3                  |
| Q | 2B                 | 23.3             | Adhesion                 | 2                  |
| R | 4B                 | 2.7              | Substrate                | 4                  |
| S | 4B                 | 4.0              | Substrate                | 4                  |
| T | 5B                 | 1.0              | Substrate                | 5                  |

\*Average Values

Note: When substrate failure occurs, the adhesion of the tape to the coating and the adhesion of the coating to the substrate are stronger than the substrate's cohesive strength which results in a lower rating even though the coating did not fail

Scrub Resistance – Test method B of ASTM D2486 was used with a new brush to insure correct data. Sherwin Williams Harmony was used as the standard.

Scrub Resistance Summary\*

|      | <b>Standard Average**</b> | <b>Sample Average</b> | <b>Sample/Standard</b> |
|------|---------------------------|-----------------------|------------------------|
| J    | 196                       | 1089                  | 5.56                   |
| K    | 199                       | 864                   | 4.34                   |
| L    | 210                       | 685                   | 3.26                   |
| M    | 213                       | 2106                  | 9.89                   |
| N    | 282                       | 890                   | 3.16                   |
| O*** | 223                       | 645                   | 2.89                   |
| P    | 232                       | 908                   | 3.91                   |
| Q    | 209                       | 915                   | 4.38                   |
| R    | 217                       | 673                   | 3.10                   |
| S    | 206                       | 308                   | 1.50                   |
| T    | 216                       | 1231                  | 5.70                   |

\*Average Values

\*\*The standard is Sherwin Williams' Harmony

\*\*\*Average of 4 Panels

**Stain Resistance** – ASTM D 4828 was modified for this test. This method was actually a washability test and provides information about the changes which occur as a result of sponge cleaning a stained area rather than the paint’s likelihood of resisting a stain. To better determine the paint’s resistance to staining, the paint was applied to four plastic panels and allowed to dry for 7 days as described in the ASTM method. Color was measured on each stripe on each panel using a Minolta CM-2002 spectrophotometer and the CIE XYZ values were recorded. Four staining materials, ketchup, mustard, wine and red crayon, were applied with each panel having three approximately one-inch stripes that were approximately half an inch apart of one stain resulting in three stripes per stain, and one stain per panel. The materials were left on the panels for 24 hours and then rinsed with de-ionized water and washed for 100 cycles with non-abrasive cleaner and a sponge according to the ASTM method. The panel was patted dry with paper towels to remove standing water, and was then allowed to air dry for one day. Then, averaged color measurements were taken of the stripes with CIE XYZ values and  $\Delta E$  values recorded. A crude visual gloss, stain, and erosion evaluation was performed and rated. The crude visual gloss rating system included 5 levels: None (N), Increase (I), Large Increase (LI), Decrease (D), and Large Decrease (LD). The crude visual stain rating system rated the samples from 0-10 with 0 being highly stained, and 10 being highly stain resistant. The crude visual erosion rating included 3 levels: None (N), Slight (S), and Moderate (M). Numerical gloss measurements were taken with the gloss meter of each stripe after washing.

**Stain Resistance – Stain Visual Rating Summary\***

|   | <b>Ketchup</b> | <b>Mustard</b> | <b>Wine</b> | <b>Red Crayon</b> |
|---|----------------|----------------|-------------|-------------------|
| J | 10             | 10             | 3           | 3                 |
| K | 10             | 7              | 3           | 3                 |
| L | 10             | 5              | 3           | 3                 |
| M | 10             | 7              | 3           | 3                 |
| N | 10             | 7              | 3           | 3                 |
| O | 10             | 5              | 5           | 3                 |
| P | 7              | 5              | 3           | 3                 |
| Q | 7              | 5              | 3           | 3                 |
| R | 10             | 3              | 5           | 0                 |
| S | 7              | 3              | 3           | 0                 |
| T | 10             | 3              | 3           | 0                 |

\*Average Values

Stain Resistance – Gloss Change Visual Rating Summary\*

|   | <b>Ketchup</b> | <b>Mustard</b> | <b>Wine</b> | <b>Red Crayon</b> |
|---|----------------|----------------|-------------|-------------------|
| J | None           | None           | None        | None              |
| K | None           | None           | None        | None              |
| L | None           | None           | None        | None              |
| M | None           | None           | None        | None              |
| N | None           | None           | None        | None              |
| O | None           | None           | None        | None              |
| P | None           | None           | None        | None              |
| Q | None           | None           | None        | None              |
| R | None           | None           | None        | None              |
| S | None           | None           | None        | None              |
| T | None           | None           | None        | None              |

\*Average Values

Stain Resistance – Erosion Visual Rating Summary\*

|   | <b>Ketchup</b> | <b>Mustard</b> | <b>Wine</b> | <b>Red Crayon</b> |
|---|----------------|----------------|-------------|-------------------|
| J | None           | None           | None        | None              |
| K | None           | None           | None        | None              |
| L | None           | None           | None        | None              |
| M | None           | None           | None        | None              |
| N | None           | None           | None        | None              |
| O | None           | None           | None        | None              |
| P | None           | None           | None        | None              |
| Q | None           | None           | None        | None              |
| R | None           | None           | None        | None              |
| S | None           | None           | None        | None              |
| T | None           | None           | None        | None              |

\*Average Values

Stain Resistance –  $\Delta E$  Summary\*

|   | <b>Ketchup</b> | <b>Mustard</b> | <b>Wine</b> | <b>Red Crayon**</b> |
|---|----------------|----------------|-------------|---------------------|
| J | 0.40           | 0.43           | 2.25        | 12.19               |
| K | 0.39           | 0.45           | 1.99        | 15.19               |
| L | 0.23           | 1.38           | 3.28        | 13.21               |
| M | 0.05           | 0.22           | 1.61        | 12.53               |
| N | 0.08           | 0.68           | 2.50        | 23.27               |
| O | 0.09           | 0.85           | 1.15        | 29.28               |
| P | 0.40           | 0.75           | 2.44        | 12.79               |
| Q | 0.31           | 1.51           | 3.18        | 16.11               |
| R | 0.24           | 5.49           | 0.91        | 8.98                |
| S | 0.66           | 3.98           | 2.04        | 8.74                |
| T | 0.31           | 4.56           | 1.67        | 10.25               |

\*Average Values \*\*The red crayon was not removed by the non-abrasive cleaner and water, therefore the color represents the color of the crayon

Stain Resistance – Gloss Summary\*

| <b>Washed Area – Ketchup (Pre/Post)</b> |                 |               |                 |               |
|---|-----------------|---------------|-----------------|---------------|
|   | <b>60° Mean</b> | <b>60° SD</b> | <b>85° Mean</b> | <b>85° SD</b> |
| J                                       | 2.4 / 2.6       | 0.1 / 0.1     | 4.0 / 4.6       | 0.2 / 0.2     |
| K                                       | 2.0 / 2.1       | 0.1 / 0.1     | 1.8 / 2.6       | 0.1 / 0.2     |
| L                                       | 2.0 / 2.1       | 0.1 / 0.1     | 3.0 / 4.2       | 0.1 / 0.2     |
| M                                       | 1.9 / 1.9       | 0.1 / 0.1     | 1.1 / 1.5       | 0.1 / 0.1     |
| N                                       | 2.3 / 2.3       | 0.1 / 0.1     | 4.5 / 6.1       | 0.1 / 0.2     |
| O                                       | 2.0 / 2.0       | 0.1 / 0.1     | 2.3 / 3.0       | 0.1 / 0.1     |
| P                                       | 2.2 / 2.4       | 0.1 / 0.1     | 2.1 / 2.5       | 0.1 / 0.1     |
| Q                                       | 2.0 / 2.2       | 0.1 / 0.1     | 2.5 / 3.0       | 0.1 / 0.2     |
| R                                       | 2.8 / 2.9       | 0.1 / 0.1     | 1.2 / 1.5       | 0.1 / 0.1     |
| S                                       | 2.2 / 2.3       | 0.1 / 0.1     | 1.7 / 2.5       | 0.1 / 0.2     |
| T                                       | 1.9 / 2.0       | 0.1 / 0.1     | 1.2 / 1.9       | 0.1 / 0.1     |

| <b>Washed Area – Mustard (Pre/Post)</b> |                 |               |                 |               |
|---|-----------------|---------------|-----------------|---------------|
|   | <b>60° Mean</b> | <b>60° SD</b> | <b>85° Mean</b> | <b>85° SD</b> |
| J                                       | 2.4 / 2.5       | 0.1 / 0.1     | 3.9 / 4.5       | 0.2 / 0.1     |
| K                                       | 1.9 / 2.1       | 0.1 / 0.1     | 1.8 / 2.5       | 0.1 / 0.1     |
| L                                       | 2.0 / 2.4       | 0.1 / 0.1     | 3.0 / 4.5       | 0.1 / 0.2     |
| M                                       | 1.9 / 1.9       | 0.1 / 0.1     | 0.8 / 1.5       | 0.2 / 0.1     |
| N                                       | 2.3 / 2.6       | 0.1 / 0.1     | 4.6 / 6.5       | 0.1 / 0.1     |
| O                                       | 2.0 / 2.3       | 0.1 / 0.1     | 2.3 / 3.3       | 0.1 / 0.1     |
| P                                       | 2.2 / 2.5       | 0.1 / 0.1     | 2.1 / 2.5       | 0.1 / 0.1     |
| Q                                       | 2.0 / 2.5       | 0.1 / 0.1     | 2.5 / 3.5       | 0.1 / 0.1     |
| R                                       | 2.8 / 3.3       | 0.1 / 0.1     | 1.2 / 1.7       | 0.1 / 0.1     |
| S                                       | 2.2 / 2.3       | 0.1 / 0.2     | 1.8 / 2.8       | 0.1 / 0.2     |
| T                                       | 1.9 / 2.1       | 0.1 / 0.1     | 1.2 / 1.8       | 0.1 / 0.1     |

| <b>Washed Area – Wine (Pre/Post)</b> |                 |               |                 |               |
|--------------------------------------|-----------------|---------------|-----------------|---------------|
|                                      | <b>60° Mean</b> | <b>60° SD</b> | <b>85° Mean</b> | <b>85° SD</b> |
| J                                    | 2.4 / 2.5       | 0.1 / 0.1     | 3.9 / 4.6       | 0.2 / 0.2     |
| K                                    | 2.0 / 2.0       | 0.1 / 0.1     | 1.8 / 2.7       | 0.1 / 0.1     |
| L                                    | 2.0 / 2.0       | 0.1 / 0.1     | 3.0 / 4.2       | 0.1 / 0.2     |
| M                                    | 1.9 / 1.8       | 0.1 / 0.1     | 1.1 / 1.5       | 0.1 / 0.1     |
| N                                    | 2.2 / 2.3       | 0.1 / 0.1     | 4.3 / 7.2       | 0.1 / 0.1     |
| O                                    | 2.0 / 2.0       | 0.1 / 0.1     | 2.3 / 3.4       | 0.1 / 0.2     |
| P                                    | 2.2 / 2.2       | 0.1 / 0.1     | 2.1 / 2.6       | 0.1 / 0.1     |
| Q                                    | 2.0 / 2.1       | 0.1 / 0.1     | 2.5 / 3.4       | 0.1 / 0.2     |
| R                                    | 2.8 / 2.9       | 0.1 / 0.1     | 1.2 / 1.5       | 0.1 / 0.1     |
| S                                    | 2.2 / 2.3       | 0.1 / 0.1     | 1.8 / 2.9       | 0.1 / 0.1     |
| T                                    | 1.9 / 1.9       | 0.1 / 0.1     | 1.2 / 2.0       | 0.1 / 0.1     |

| <b>Washed Area – Red Crayon (Pre/Post)**</b> |                 |               |                 |               |
|--|-----------------|---------------|-----------------|---------------|
|  | <b>60° Mean</b> | <b>60° SD</b> | <b>85° Mean</b> | <b>85° SD</b> |
| J  | 2.4 / 3.2       | 0.1 / 0.2     | 3.9 / 8.9       | 0.1 / 0.5     |
| K  | 1.9 / 2.4       | 0.1 / 0.1     | 1.8 / 5.4       | 0.1 / 0.2     |
| L  | 2.0 / 2.8       | 0.1 / 0.2     | 3.0 / 8.8       | 0.1 / 0.9     |
| M  | 1.9 / 2.1       | 0.1 / 0.1     | 1.1 / 3.6       | 0.1 / 0.3     |
| N  | 2.3 / 3.7       | 0.1 / 0.2     | 4.6 / 15.8      | 0.1 / 1.0     |
| O  | 2.0 / 3.0       | 0.1 / 0.2     | 2.3 / 10.5      | 0.1 / 0.5     |
| P  | 2.2 / 2.7       | 0.1 / 0.1     | 2.0 / 5.4       | 0.1 / 0.4     |
| Q  | 2.0 / 2.6       | 0.1 / 0.2     | 2.5 / 7.1       | 0.1 / 0.3     |
| R  | 2.8 / 2.8       | 0.1 / 0.1     | 1.2 / 2.3       | 0.1 / 0.2     |
| S  | 2.2 / 2.4       | 0.1 / 0.1     | 1.8 / 4.2       | 0.1 / 0.2     |
| T  | 1.9 / 2.1       | 0.1 / 0.1     | 1.2 / 3.3       | 0.1 / 0.2     |

\*Average Values

\*\*The red crayon was not removed by the non-abrasive cleaner and water; therefore the gloss measurements for the red crayon stripes reflect the gloss of the crayon, not the gloss of the coating.

**Touch-Up** – This procedure was performed as indicated in ASTM D 3928 on primed (Behr P.V.A. Drywall Primer & Sealer No. 73) drywall panels, involving two sections (A and B) painted with the test paint 1 minute apart with a two inch overlap between them (C), an ‘X’ (D) painted on the second section 30 seconds after being painted, and a rectangle (E) painted on the first section 24 hours later. Gloss measurements were used to evaluate the results by taking two measurements on the bulk sections (A and B) and the overlapped and touched up sections (C, D, and E) at perpendicular angles (one reading horizontal, one reading vertical). The panels was also checked for visible gloss variations at the touched up sections. The results were fitted to a 0-10 scale.

The A and B sections represent non-touched up and non-overlapped sections after normal application, and the C section represents overlap during application. The D and E sections represent touched up sections where D was an immediate touch up and E was a touch up a day later. The gloss difference between A/B and C represents the gloss difference of overlapped sections that were not painted over repeatedly. The difference in gloss between A/B and D represents the gloss change that results from immediate touching up, and the difference between A/B and E represents the gloss difference that results from touching up a wall a day later.

Touch-Up - Gloss Summary\*

|   | <b>A1</b> | <b>A2</b> | <b>B1</b> | <b>B2</b> | <b>C1</b> | <b>C2</b> | <b>D1</b> | <b>D2</b> | <b>E1</b> | <b>E2</b> | <b>Visual Rating**</b> |
|---|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|------------------------|
| J | 3.4       | 3.9       | 3.7       | 3.4       | 4.1       | 3.8       | 3.6       | 3.6       | 3.8       | 3.9       | 10                     |
| K | 1.6       | 1.8       | 1.7       | 1.7       | 2.0       | 1.9       | 1.8       | 1.8       | 2.2       | 2.0       | 10                     |
| L | 2.4       | 2.6       | 2.5       | 2.5       | 2.6       | 2.6       | 2.5       | 2.6       | 2.5       | 2.4       | 10                     |
| M | 0.9       | 1.1       | 1.3       | 0.9       | 1.3       | 0.9       | 1.2       | 1.2       | 1.2       | 1.1       | 10                     |
| N | 2.8       | 3.2       | 3.4       | 3.1       | 4.0       | 3.3       | 3.5       | 3.4       | 3.5       | 3.9       | 10                     |
| O | 1.7       | 2.1       | 2.0       | 1.8       | 2.1       | 1.8       | 2.0       | 2.0       | 2.0       | 1.9       | 10                     |
| P | 1.6       | 2.0       | 2.1       | 1.8       | 2.2       | 1.7       | 2.1       | 2.1       | 1.9       | 1.9       | 10                     |
| Q | 1.9       | 2.2       | 2.1       | 1.9       | 2.3       | 1.9       | 2.1       | 2.1       | 2.2       | 1.9       | 10                     |
| R | 1.1       | 1.3       | 1.2       | 1.1       | 1.4       | 1.2       | 1.1       | 1.1       | 0.9       | 0.9       | 10                     |
| S | 1.2       | 1.6       | 1.6       | 1.2       | 1.4       | 1.1       | 1.6       | 1.6       | 1.5       | 1.5       | 10                     |
| T | 0.9       | 1.3       | 1.2       | 1.0       | 1.3       | 1.0       | 1.1       | 1.2       | 1.1       | 1.2       | 10                     |

\*Average Values

\*\*Because these paints are flat, there was no discernable visual gloss difference at 85°

\*\*\*Note: A1, B1, C1, and E1 are all horizontal gloss measurements along the length of the panel and A2, B2, C2, and E2 were all vertical measurements along the width of the panel. D1 was a measurement along the diagonal stroke that goes from the upper left to the lower right, and D2 was a measurement along the diagonal stroke that goes from the upper right to the lower left

## Tests for Exterior Flat Paints Summary

Adhesion – ASTM D 3359-Method B was used to determine adhesion of a 3mil drawdown on a Leneta chart. This method used a cutting tool and 3mm cutting guide to make a series of perpendicular cuts in the surface. Pressure sensitive tape in accordance with the ASTM procedure was then applied and removed after 90 seconds and the adhesion was qualitatively analyzed based on how much coating was removed by the tape. The ASTM classification of 0B-5B was put into a rating system of 0-5, respectively, with 5 being 0% removed and a 0 being greater than 65% removed.

Adhesion Summary – Glass\*

|   | ASTM Rating | Failure % | Failure Mechanism | AQMD Rating |
|---|-------------|-----------|-------------------|-------------|
| A | 3B          | 10        | Adhesion          | 3           |
| B | 4B          | 2         | Adhesion          | 4           |
| C | 2B          | 20        | Adhesion          | 2           |
| D | 4B          | 4         | Adhesion          | 4           |
| E | 5B          | 0         | -----             | 5           |
| F | 2B          | 18        | Adhesion          | 2           |
| G | 2B          | 17        | Adhesion          | 2           |
| H | 4B          | 3         | Adhesion          | 4           |
| I | 4B          | 1         | Adhesion          | 4           |
| S | 2B          | 20        | Adhesion          | 2           |
| T | 3B          | 7         | Adhesion          | 3           |

\*Average Values

Tannin Stain Blocking – Protocol from prior SCAQMD study was used. This test evaluates a coating’s ability to resist tannin bleed-through from wood substrates. Cedar was used as the substrate. The panels were coated by weight, allowed to dry 24 hours in ambient conditions, and then were dried for two weeks at 50°C. The panels were then evaluated for color change by spectrophotometer before and after drying in the oven, as well as being ranked relative to positive (Morewear 1150 Acrylic Stain Blocking Primer) and negative (Valspar Ultra Premium 72926) tannin controls on the boards. Each of the three sets of coatings were visually ranked from 1-13 with 13 being the most white coating, and 1 being the least white coating.

Color difference ( $\Delta E$ ) measurements were taken for two different comparisons. The first one was the tannin bleed which was measured as the difference in color between the coating after initial drying on the cedar panels and the final after the panels were removed from the oven. The second color difference measured incorporates the flash tannin bleed which was the tannin bleed that occurs during the application and drying of the coating by measuring the panels after the test versus the color on a Leneta chart drawdown. A high color difference between the Leneta and the final and a low color difference between the tannin board before and after oven drying indicates that a coating had a large amount of flash tannin bleed, but had less tannin bleed once the coating was initially dry.

Tannin Stain Blocking Summary\*

|                   | $\Delta E$ (Initial Cedar) | Visual Ranking** | $\Delta E$ (Leneta) |
|-------------------|----------------------------|------------------|---------------------|
| Positive Standard | 1.27                       | 5                | 4.48                |
| Negative Standard | 0.67                       | 1                | 2.77                |
| A                 | 1.17                       | 9                | 4.38                |
| B                 | 0.79                       | 3                | 4.93                |
| C                 | 0.88                       | 4                | 4.28                |
| D                 | 0.81                       | 2                | 4.78                |
| E                 | 0.91                       | 12               | 1.54                |
| F                 | 1.00                       | 13               | 1.70                |
| G                 | 0.98                       | 8                | 3.69                |
| H                 | 0.86                       | 10               | 3.15                |
| I                 | 1.35                       | 11               | 4.23                |
| S                 | 1.08                       | 7                | 4.15                |
| T                 | 1.23                       | 7                | 4.95                |

\*Average Values

\*\*These values are the average of the three visual rankings

Alkalinity Resistance – The Dunn Edwards Alkali Resistance Test Method was used with Dunn Edwards concrete test panels. A sample of the coating was tinted with a mixture of D-E QTC1 and QTC 7 tints and applied to the test panel. The back of the test panel was immersed in a tub of water and the tub was placed outdoors for full exposure. The panels were examined every day for 7 days and the spectrophotometer was used to determine color changes. The panels were also visually examined for color change. The results were fitted into a 0-10 scale with 10 being no color change and 0 being severe color change.

The spectrophotometer  $\Delta E$  readings provide a numerical representation of the color changes. For example, a reading of 0.50 is often considered a visual match between a standard and a sample. For this test, a  $\Delta E$  reading less than 1.00 would indicate an excellent resistance, a reading of 2.00 would indicate very good, 3.00 good, 4.00 poor, and 5.00 complete failure.

The coatings in this test were only allowed to dry one day before severe exposure, which includes the concrete being placed in water. Because these coatings are only allowed to dry one day, they are tested before they are fully coalesced. The amount of time required for a given coating to fully coalesce depends on the particle size and molecular weight of that particular coating's resin. A coating that has not fully coalesced tends to be more permeable to both water and base, resulting in accelerated failure for most of the coatings under these conditions.

Alkalinity Resistance -  $\Delta E$  Summary\*

|   | 1 Day | 2 Days | 3 Days | 4 Days | 5Days | 6 Days | 7 Days | Final | Visual |
|---|-------|--------|--------|--------|-------|--------|--------|-------|--------|
| A | 1.31  | 2.23   | 4.19   | 6.14   | 7.47  | 8.99   | 9.95   | 8.75  | 0      |
| B | 0.95  | 1.25   | 1.77   | 2.38   | 2.99  | 2.97   | 3.13   | 3.20  | 1      |
| C | 0.97  | 3.20   | 5.14   | 7.17   | 7.73  | 8.42   | 8.53   | 8.79  | 0      |
| D | 0.66  | 1.04   | 1.37   | 1.94   | 2.34  | 2.45   | 2.79   | 2.42  | 1      |
| E | 1.03  | 3.37   | 6.36   | 9.65   | 11.57 | 11.34  | 12.81  | 12.92 | 0      |
| F | 2.11  | 4.14   | 8.52   | 12.54  | 13.65 | 15.75  | 15.51  | 15.32 | 0      |
| G | 2.31  | 4.18   | 6.86   | 9.57   | 11.77 | 12.89  | 13.60  | 14.12 | 1      |
| H | 1.14  | 1.90   | 3.59   | 6.31   | 9.04  | 9.66   | 11.32  | 11.87 | 0      |
| I | 1.35  | 3.13   | 5.82   | 9.68   | 13.83 | 14.92  | 15.68  | 14.95 | 0      |
| S | 0.84  | 2.77   | 8.78   | 13.71  | 19.30 | 19.76  | 20.72  | 20.96 | 0      |
| T | 1.65  | 5.88   | 16.30  | 22.03  | 25.38 | 26.48  | 27.58  | 26.50 | 0      |

\*Average Values

## Test Results

### Tests for General Properties of All Paints

#### Appearance

|   | <b>Observations – 1 gallon can as received:<br/>Notes on Odor, Skinning, Pressure, Can Corrosion</b> |
|---|--|
| A | None   |
| B | Very Trace Can Corrosion   |
| C | None   |
| D | None   |
| E | <i>None</i>  |
| F | None   |
| G | Trace Can Corrosion  |
| H | Very Slight Separation   |
| I | None   |
| J | None   |
| K | None   |
| L | None   |
| M | 1 ¾ inch medium yellow separation layer with darker spots  |
| N | None   |
| O | None   |
| P | None   |
| Q | None   |
| R | Very Slight Separation   |
| S | Trace Can Corrosion  |
| T | None   |

#### Gloss (60° & 85°)

|             | <b>Gloss (5 readings per replicate)</b> |                      |                 |                      |
|-------------|---|----------------------|-----------------|----------------------|
|             | <b>60° Mean</b>                         | <b>60° Std. Dev.</b> | <b>85° Mean</b> | <b>85° Std. Dev.</b> |
| A           | 1.9                                     | 0.1                  | 0.8             | 0.1                  |
| Replicate 2 | 1.9                                     | 0.1                  | 0.8             | 0.1                  |
| Average     | <b>1.9</b>                              | <b>0.1</b>           | <b>0.8</b>      | <b>0.1</b>           |
| B           | 2.7                                     | 0.1                  | 2.2             | 0.1                  |
| Replicate 2 | 2.7                                     | 0.1                  | 2.2             | 0.1                  |
| Average     | <b>2.7</b>                              | <b>0.1</b>           | <b>2.2</b>      | <b>0.1</b>           |
| C           | 2.3                                     | 0.1                  | 2.5             | 0.1                  |
| Replicate 2 | 2.3                                     | 0.1                  | 2.5             | 0.1                  |
| Average     | <b>2.3</b>                              | <b>0.1</b>           | <b>2.5</b>      | <b>0.1</b>           |
| D           | 2.1                                     | 0.1                  | 1.6             | 0.1                  |
| Replicate 2 | 2.1                                     | 0.1                  | 1.6             | 0.1                  |
| Average     | <b>2.1</b>                              | <b>0.1</b>           | <b>1.6</b>      | <b>0.1</b>           |
| E           | 8.7                                     | 0.1                  | 28.0            | 0.1                  |
| Replicate 2 | 8.7                                     | 0.1                  | 28.0            | 0.2                  |
| Average     | <b>8.7</b>                              | <b>0.1</b>           | <b>28.0</b>     | <b>0.2</b>           |
| F           | 2.5                                     | 0.1                  | 2.7             | 0.1                  |
| Replicate 2 | 2.5                                     | 0.1                  | 2.7             | 0.1                  |

|             |            |            |            |            |
|-------------|------------|------------|------------|------------|
| Average     | <b>2.5</b> | <b>0.1</b> | <b>2.7</b> | <b>0.1</b> |
| G           | 1.7        | 0.1        | 0.6        | 0.1        |
| Replicate 2 | 1.6        | 0.1        | 0.6        | 0.1        |
| Average     | <b>1.7</b> | <b>0.1</b> | <b>0.6</b> | <b>0.1</b> |
| H           | 1.9        | 0.1        | 1.1        | 0.1        |
| Replicate 2 | 1.9        | 0.1        | 1.1        | 0.1        |
| Average     | <b>1.9</b> | <b>0.1</b> | <b>1.1</b> | <b>0.1</b> |
| I           | 2.0        | 0.1        | 1.0        | 0.1        |
| Replicate 2 | 2.0        | 0.1        | 1.0        | 0.1        |
| Average     | <b>2.0</b> | <b>0.1</b> | <b>1.0</b> | <b>0.1</b> |
| J           | 2.4        | 0.1        | 4.3        | 0.1        |
| Replicate 2 | 2.5        | 0.1        | 4.4        | 0.1        |
| Average     | <b>2.5</b> | <b>0.1</b> | <b>4.4</b> | <b>0.1</b> |
| K           | 2.0        | 0.1        | 2.0        | 0.1        |
| Replicate 2 | 2.0        | 0.1        | 1.9        | 0.1        |
| Average     | <b>2.0</b> | <b>0.1</b> | <b>2.0</b> | <b>0.1</b> |
| L           | 2.1        | 0.1        | 3.2        | 0.1        |
| Replicate 2 | 2.1        | 0.1        | 3.2        | 0.1        |
| Average     | <b>2.1</b> | <b>0.1</b> | <b>3.2</b> | <b>0.1</b> |
| M           | 1.9        | 0.1        | 1.1        | 0.1        |
| Replicate 2 | 1.9        | 0.1        | 1.1        | 0.1        |
| Average     | <b>1.9</b> | <b>0.1</b> | <b>1.1</b> | <b>0.1</b> |
| N           | 2.3        | 0.1        | 4.9        | 0.1        |
| Replicate 2 | 2.3        | 0.1        | 4.9        | 0.1        |
| Average     | <b>2.3</b> | <b>0.1</b> | <b>4.9</b> | <b>0.1</b> |
| O           | 2.0        | 0.1        | 2.4        | 0.1        |
| Replicate 2 | 2.0        | 0.1        | 2.4        | 0.1        |
| Average     | <b>2.0</b> | <b>0.1</b> | <b>2.4</b> | <b>0.1</b> |
| P           | 2.3        | 0.1        | 2.3        | 0.1        |
| Replicate 2 | 2.3        | 0.1        | 2.3        | 0.1        |
| Average     | <b>2.3</b> | <b>0.1</b> | <b>2.3</b> | <b>0.1</b> |
| Q           | 2.1        | 0.1        | 2.8        | 0.1        |
| Replicate 2 | 2.1        | 0.1        | 2.8        | 0.1        |
| Average     | <b>2.1</b> | <b>0.1</b> | <b>2.8</b> | <b>0.1</b> |
| R           | 2.9        | 0.1        | 1.3        | 0.1        |
| Replicate 2 | 3.0        | 0.1        | 1.3        | 0.1        |
| Average     | <b>3.0</b> | <b>0.1</b> | <b>1.3</b> | <b>0.1</b> |
| S           | 2.3        | 0.1        | 1.9        | 0.1        |
| Replicate 2 | 2.3        | 0.1        | 1.9        | 0.1        |
| Average     | <b>2.3</b> | <b>0.1</b> | <b>1.9</b> | <b>0.1</b> |
| T           | 1.9        | 0.1        | 1.3        | 0.1        |
| Replicate 2 | 1.9        | 0.1        | 1.3        | 0.1        |
| Average     | <b>1.9</b> | <b>0.1</b> | <b>1.3</b> | <b>0.1</b> |

Stability

|   | Initial | Storage | Stormer Visc. |      | Viscosity | Character | Gloss (5 readings per replicate) |       |         |       |
|---|---------|---------|---------------|------|-----------|-----------|----------------------------------|-------|---------|-------|
|   | Stormer | Time    | Viscosity     | Temp | Rating    | Rating    | 60°Mean                          | 60°SD | 85°Mean | 85°SD |
| A | 97      | 30 Days | 101           | 25   | 6         | 8         | 1.9                              | 0.1   | 0.8     | 0.1   |
| B | 94      | 30 Days | 96            | 25   | 8         | 6         | 2.6                              | 0.1   | 2.3     | 0.1   |
| C | 102     | 30 Days | 114           | 25   | 0         | 8         | 2.3                              | 0.1   | 2.7     | 0.1   |
| D | 101     | 30 Days | 103           | 25   | 8         | 8         | 2.1                              | 0.1   | 1.7     | 0.1   |
| E | 103     | 30 Days | 108           | 25   | 5         | 4         | 9.7                              | 0.2   | 29.3    | 0.2   |
| F | 108     | 30 Days | 114           | 25   | 4         | 8         | 2.5                              | 0.1   | 2.8     | 0.1   |
| G | 115     | 30 Days | 115           | 25   | 10        | 6         | 1.7                              | 0.1   | 0.6     | 0.1   |
| H | 104     | 30 Days | 103           | 25   | 9         | 6         | 1.9                              | 0.1   | 1.0     | 0.1   |
| I | 100     | 30 Days | 102           | 25   | 8         | 6         | 2.0                              | 0.1   | 0.9     | 0.1   |
| J | 95      | 30 Days | 104           | 25   | 1         | 10        | 2.4                              | 0.1   | 4.7     | 0.2   |
| K | 110     | 30 Days | 120           | 25   | 0         | 8         | 2.0                              | 0.1   | 2.0     | 0.1   |
| L | 107     | 30 Days | 124           | 25   | 0         | 6         | 2.1                              | 0.1   | 3.2     | 0.1   |
| M | 100     | 30 Days | 101           | 25   | 9         | 4         | 2.0                              | 0.1   | 1.3     | 0.1   |
| N | 102     | 30 Days | 101           | 25   | 9         | 6         | 2.2                              | 0.1   | 5.0     | 0.1   |
| O | 97      | 30 Days | 94            | 25   | 7         | 6         | 2.0                              | 0.1   | 2.4     | 0.1   |
| P | 102     | 30 Days | 104           | 25   | 8         | 4         | 2.3                              | 0.1   | 2.4     | 0.1   |
| Q | 109     | 30 Days | 112           | 25   | 7         | 6         | 2.1                              | 0.1   | 2.8     | 0.1   |
| R | 117     | 30 Days | 126           | 25   | 1         | 6         | 2.9                              | 0.1   | 1.3     | 0.1   |
| S | 99      | 30 Days | 94            | 25   | 5         | 6         | 2.3                              | 0.1   | 2.0     | 0.1   |
| T | 99      | 30 Days | 100           | 25   | 9         | 4         | 1.9                              | 0.1   | 1.3     | 0.1   |

Stability – Syneresis

|                |         | Clear Layer | AQMD     |                  |                |         | Clear Layer | AQMD     |                  |
|----------------|---------|-------------|----------|------------------|----------------|---------|-------------|----------|------------------|
|                | Time    | (mm)        | Rating   | Settling Notes   |                | Time    | (mm)        | Rating   | Settling Notes   |
| A              | 10 Days | 0.75        | 9        | None             | K              | 10 Days | 2           | 8        | Soft Pack        |
| Replicate 2    |         | 0.75        | 9        | None             | Replicate 2    |         | 2           | 8        | Soft Pack        |
| Replicate 3    |         | 0.75        | 9        | None             | Replicate 3    |         | 2           | 8        | Soft Pack        |
| <b>Average</b> |         | <b>0.75</b> | <b>9</b> | <b>None</b>      | <b>Average</b> |         | <b>2</b>    | <b>8</b> | <b>Soft Pack</b> |
| B              | 10 Days | 1           | 9        | Soft Pack        | L              | 10 Days | 2           | 8        | Hard Pack        |
| Replicate 2    |         | 1           | 9        | Soft Pack        | Replicate 2    |         | 2           | 8        | Hard Pack        |
| Replicate 3    |         | 1           | 9        | Soft Pack        | Replicate 3    |         | 2           | 8        | Hard Pack        |
| <b>Average</b> |         | <b>1</b>    | <b>9</b> | <b>Soft Pack</b> | <b>Average</b> |         | <b>2</b>    | <b>8</b> | <b>Hard Pack</b> |
| C              | 10 Days | 0.5         | 9        | Hard Pack        | M              | 10 Days | 1           | 9        | None             |
| Replicate 2    |         | 0.5         | 9        | Hard Pack        | Replicate 2    |         | 1           | 9        | None             |
| Replicate 3    |         | 0.5         | 9        | Hard Pack        | Replicate 3    |         | 1           | 9        | None             |
| <b>Average</b> |         | <b>0.5</b>  | <b>9</b> | <b>Hard Pack</b> | <b>Average</b> |         | <b>1</b>    | <b>9</b> | <b>None</b>      |
| D              | 10 Days | 1           | 9        | Soft Pack        | N              | 10 Days | 1           | 9        | Soft Pack        |

|                |         |            |          |                  |                |         |            |          |                  |
|----------------|---------|------------|----------|------------------|----------------|---------|------------|----------|------------------|
| Replicate 2    |         | 1          | 9        | Soft Pack        | Replicate 2    |         | 1          | 9        | Soft Pack        |
| Replicate 3    |         | 1          | 9        | Soft Pack        | Replicate 3    |         | 1          | 9        | Soft Pack        |
| <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>Soft Pack</b> | <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>Soft Pack</b> |
| E              | 10 Days | 2          | 8        | Soft Pack        | O              | 10 Days | 2          | 8        | Soft Pack        |
| Replicate 2    |         | 2          | 8        | Soft Pack        | Replicate 2    |         | 2          | 8        | Soft Pack        |
| Replicate 3    |         | 2          | 8        | Soft Pack        | Replicate 3    |         | 2          | 8        | Soft Pack        |
| <b>Average</b> |         | <b>2</b>   | <b>8</b> | <b>Soft Pack</b> | <b>Average</b> |         | <b>2</b>   | <b>8</b> | <b>Soft Pack</b> |
| F              | 10 Days | 0.5        | 9        | Soft Pack        | P              | 10 Days | 1          | 9        | Soft Pack        |
| Replicate 2    |         | 0.5        | 9        | Soft Pack        | Replicate 2    |         | 1          | 9        | Soft Pack        |
| Replicate 3    |         | 0.5        | 9        | Soft Pack        | Replicate 3    |         | 1          | 9        | Soft Pack        |
| <b>Average</b> |         | <b>0.5</b> | <b>9</b> | <b>Soft Pack</b> | <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>Soft Pack</b> |
| G              | 10 Days | 1          | 9        | Soft Pack        | Q              | 10 Days | 1          | 9        | Soft Pack        |
| Replicate 2    |         | 1          | 9        | Soft Pack        | Replicate 2    |         | 1          | 9        | Soft Pack        |
| Replicate 3    |         | 1          | 9        | Soft Pack        | Replicate 3    |         | 1          | 9        | Soft Pack        |
| <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>Soft Pack</b> | <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>Soft Pack</b> |
| H              | 10 Days | 1          | 9        | Soft Pack        | R              | 10 Days | 0.5        | 9        | Soft Pack        |
| Replicate 2    |         | 1          | 9        | Soft Pack        | Replicate 2    |         | 0.5        | 9        | Soft Pack        |
| Replicate 3    |         | 1          | 9        | Soft Pack        | Replicate 3    |         | 0.5        | 9        | Soft Pack        |
| <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>Soft Pack</b> | <b>Average</b> |         | <b>0.5</b> | <b>9</b> | <b>Soft Pack</b> |
| I              | 10 Days | 0.5        | 9        | Soft Pack        | S              | 10 Days | 1          | 9        | None             |
| Replicate 2    |         | 0.5        | 9        | Soft Pack        | Replicate 2    |         | 1          | 9        | None             |
| Replicate 3    |         | 0.5        | 9        | Soft Pack        | Replicate 3    |         | 1          | 9        | None             |
| <b>Average</b> |         | <b>0.5</b> | <b>9</b> | <b>Soft Pack</b> | <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>None</b>      |
| J              | 10 Days | 1          | 9        | Hard Pack        | T              | 10 Days | 1          | 9        | None             |
| Replicate 2    |         | 1          | 9        | Hard Pack        | Replicate 2    |         | 1          | 9        | None             |
| Replicate 3    |         | 1          | 9        | Hard Pack        | Replicate 3    |         | 1          | 9        | None             |
| <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>Hard Pack</b> | <b>Average</b> |         | <b>1</b>   | <b>9</b> | <b>None</b>      |

Open Time/ Wet Edge

|                | <b>Last Non-Visible Squiggle</b> | <b>AQMD</b>   |  |                | <b>Last Non-Visible Squiggle</b> | <b>AQMD</b>   |
|----------------|----------------------------------|---------------|--|----------------|----------------------------------|---------------|
|                | <b>Time (min)</b>                | <b>Rating</b> |  |                | <b>Time (min)</b>                | <b>Rating</b> |
| A              | 16                               | 10+           |  | K              | 14                               | 10+           |
| Replicate 2    | 14                               | 10+           |  | Replicate 2    | 10                               | 10            |
| Replicate 3    | 12                               | 10+           |  | Replicate 3    | 12                               | 10+           |
| <b>Average</b> | <b>14</b>                        | <b>10+</b>    |  | <b>Average</b> | <b>12</b>                        | <b>10+</b>    |
| B              | 10                               | 10            |  | L              | 12                               | 10+           |
| Replicate 2    | 10                               | 10            |  | Replicate 2    | 12                               | 10+           |
| Replicate 3    | 10                               | 10            |  | Replicate 3    | 12                               | 10+           |
| <b>Average</b> | <b>10</b>                        | <b>10</b>     |  | <b>Average</b> | <b>12</b>                        | <b>10+</b>    |

|                    |           |            |  |                |           |            |
|--------------------|-----------|------------|--|----------------|-----------|------------|
| C                  | 12        | 10+        |  | M              | 12        | 10+        |
| Replicate 2        | 12        | 10+        |  | Replicate 2    | 12        | 10+        |
| Replicate 3        | 12        | 10+        |  | Replicate 3    | 12        | 10+        |
| <b>Average</b>     | <b>12</b> | <b>10+</b> |  | <b>Average</b> | <b>12</b> | <b>10+</b> |
| D                  | 16        | 10+        |  | N              | 12        | 10+        |
| Replicate 2        | 14        | 10+        |  | Replicate 2    | 12        | 10+        |
| Replicate 3        | 14        | 10+        |  | Replicate 3    | 14        | 10+        |
| <b>Average</b>     | <b>15</b> | <b>10+</b> |  | <b>Average</b> | <b>13</b> | <b>10+</b> |
| <i>E</i>           | <i>16</i> | <i>10+</i> |  | O              | 10        | 10         |
| <i>Replicate 2</i> | <i>14</i> | <i>10+</i> |  | Replicate 2    | 8         | 8          |
| <i>Replicate 3</i> | <i>14</i> | <i>10+</i> |  | Replicate 3    | 8         | 8          |
| <b>Average</b>     | <b>15</b> | <b>10+</b> |  | <b>Average</b> | <b>9</b>  | <b>9</b>   |
| F                  | 14        | 10+        |  | P              | 8         | 8          |
| Replicate 2        | 14        | 10+        |  | Replicate 2    | 8         | 8          |
| Replicate 3        | 14        | 10+        |  | Replicate 3    | 8         | 8          |
| <b>Average</b>     | <b>14</b> | <b>10+</b> |  | <b>Average</b> | <b>8</b>  | <b>8</b>   |
| G                  | 12        | 10+        |  | Q              | 8         | 8          |
| Replicate 2        | 14        | 10+        |  | Replicate 2    | 8         | 8          |
| Replicate 3        | 14        | 10+        |  | Replicate 3    | 8         | 8          |
| <b>Average</b>     | <b>13</b> | <b>10+</b> |  | <b>Average</b> | <b>8</b>  | <b>8</b>   |
| H                  | 16        | 10+        |  | R              | 8         | 8          |
| Replicate 2        | 16        | 10+        |  | Replicate 2    | 8         | 8          |
| Replicate 3        | 16        | 10+        |  | Replicate 3    | 8         | 8          |
| <b>Average</b>     | <b>16</b> | <b>10+</b> |  | <b>Average</b> | <b>8</b>  | <b>8</b>   |
| I                  | 14        | 10+        |  | S              | 10        | 10         |
| Replicate 2        | 14        | 10+        |  | Replicate 2    | 10        | 10         |
| Replicate 3        | 12        | 10+        |  | Replicate 3    | 10        | 10         |
| <b>Average</b>     | <b>13</b> | <b>10+</b> |  | <b>Average</b> | <b>10</b> | <b>10</b>  |
| J                  | 10        | 10         |  | T              | 14        | 10+        |
| Replicate 2        | 12        | 10+        |  | Replicate 2    | 14        | 10+        |
| Replicate 3        | 12        | 10+        |  | Replicate 3    | 14        | 10+        |
| <b>Average</b>     | <b>11</b> | <b>10+</b> |  | <b>Average</b> | <b>14</b> | <b>10+</b> |

Freeze-Thaw Resistance

|       | Original | After 1 Cycle |         |      | After 2 Cycles |         |      | After 3 Cycles |         |      | After 4 Cycles |         |      | After 5 Cycles |         |      | AQMD   |
|-------|----------|---------------|---------|------|----------------|---------|------|----------------|---------|------|----------------|---------|------|----------------|---------|------|--------|
|       | Stormer  | S/G/C         | Stormer | Temp | S/G/C          | Stormer | Temp | S/G/C          | Stormer | Temp | S/G/C          | Stormer | Temp | S/G/C          | Stormer | Temp | Rating |
| A     | 97       | 10            | 99      | 25   | 8              | 97      | 25   | 8              | 94      | 25   | 6              | 94      | 25   | 4              | 102     | 25   | 10     |
| Can 2 | 97       | 10            | 96      | 25   | 8              | 95      | 25   | 8              | 94      | 25   | 6              | 94      | 25   | 4              | 101     | 25   | 10     |
| Can 3 | 97       | 10            | 98      | 25   | 8              | 98      | 25   | 8              | 98      | 25   | 6              | 94      | 25   | 4              | 104     | 25   | 10     |
| B     | 94       | 10            | 94      | 25   | 6              | 95      | 25   | 6              | 96      | 25   | 4              | 96      | 25   | 4              | 99      | 25   | 10     |
| Can 2 | 94       | 10            | 94      | 25   | 6              | 93      | 25   | 6              | 93      | 25   | 4              | 93      | 25   | 4              | 100     | 25   | 10     |
| Can 3 | 94       | 10            | 93      | 25   | 6              | 92      | 25   | 6              | 92      | 25   | 4              | 93      | 25   | 4              | 98      | 25   | 10     |
| C     | 101      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 2 | 102      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 3 | 102      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| D     | 100      | 8             | 100     | 25   | 6              | 103     | 25   | 6              | 102     | 25   | 4              | 107     | 25   | 2              | 109     | 25   | 10     |
| Can 2 | 102      | 8             | 104     | 25   | 6              | 104     | 25   | 6              | 104     | 25   | 4              | 109     | 25   | 2              | 109     | 25   | 10     |
| Can 3 | 101      | 8             | 102     | 25   | 6              | 104     | 25   | 6              | 105     | 25   | 4              | 109     | 25   | 2              | 109     | 25   | 10     |
| E     | 103      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 2 | 103      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 3 | 103      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| F     | 108      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 2 | 109      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 3 | 108      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| G     | 115      | 4             | 138     | 25   | Failure        |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 2      |
| Can 2 | 115      | 4             | 141     | 25   | Failure        |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 2      |
| Can 3 | 116      | 4             | 141     | 25   | Failure        |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 2      |
| H     | 104      | 6             | 118     | 25   | 4              | 125     | 25   | 2              | 131     | 25   | 2              | 131     | 25   | Failure        |         |      | 8      |
| Can 2 | 104      | 6             | 117     | 25   | 4              | 123     | 25   | 2              | 131     | 25   | 2              | 133     | 25   | Failure        |         |      | 8      |
| Can 3 | 104      | 6             | 117     | 25   | 4              | 123     | 25   | 2              | 130     | 25   | 2              | 132     | 25   | Failure        |         |      | 8      |
| I     | 101      | 8             | 103     | 25   | 6              | 105     | 25   | 6              | 104     | 25   | 4              | 106     | 25   | 2              | 113     | 25   | 10     |
| Can 2 | 98       | 8             | 99      | 25   | 6              | 101     | 25   | 6              | 102     | 25   | 4              | 103     | 25   | 2              | 113     | 25   | 10     |
| Can 3 | 101      | 8             | 102     | 25   | 6              | 103     | 25   | 6              | 103     | 25   | 4              | 105     | 25   | 2              | 112     | 25   | 10     |
| J     | 94       | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 2 | 95       | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 3 | 95       | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| K     | 110      | 4             | 122     | 25   | Failure        |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 2      |
| Can 2 | 109      | 4             | 132     | 25   | Failure        |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 2      |
| Can 3 | 110      | 4             | 133     | 25   | Failure        |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 2      |
| L     | 108      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 2 | 107      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |
| Can 3 | 107      | Failure       |         |      | -----          |         |      | -----          |         |      | -----          |         |      | -----          |         |      | 0      |

|       |                 |                      |                |             |                       |                |             |                       |                |             |                       |                |             |                       |                |             |   |
|-------|-----------------|----------------------|----------------|-------------|-----------------------|----------------|-------------|-----------------------|----------------|-------------|-----------------------|----------------|-------------|-----------------------|----------------|-------------|---|
| M     | 99              | Failure              | -----          | -----       | -----                 | -----          | 0           |                       |                |             |                       |                |             |                       |                |             |   |
| Can 2 | 100             | Failure              | -----          | -----       | -----                 | -----          | 0           |                       |                |             |                       |                |             |                       |                |             |   |
| Can 3 | 100             | Failure              | -----          | -----       | -----                 | -----          | 0           |                       |                |             |                       |                |             |                       |                |             |   |
| N     | 102             | Failure              | -----          | -----       | -----                 | -----          | 0           |                       |                |             |                       |                |             |                       |                |             |   |
| Can 2 | 101             | Failure              | -----          | -----       | -----                 | -----          | 0           |                       |                |             |                       |                |             |                       |                |             |   |
| Can 3 | 102             | Failure              | -----          | -----       | -----                 | -----          | 0           |                       |                |             |                       |                |             |                       |                |             |   |
|       | <b>Original</b> | <b>After 1 Cycle</b> |                |             | <b>After 3 Cycles</b> |                |             | <b>After 5 Cycles</b> |                |             | <b>After 8 Cycles</b> |                |             | <b>After 8 Cycles</b> |                |             |   |
|       | <b>Stormer</b>  | <b>S/G/C</b>         | <b>Stormer</b> | <b>Temp</b> | <b>S/G/C</b>          | <b>Stormer</b> | <b>Temp</b> | <b>S/G/C</b>          | <b>Stormer</b> | <b>Temp</b> | <b>S/G/C</b>          | <b>Stormer</b> | <b>Temp</b> | <b>S/G/C</b>          | <b>Stormer</b> | <b>Temp</b> |   |
| O     | 97              | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 2 | 97              | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 3 | 96              | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| P     | 102             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 2 | 103             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 3 | 101             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Q     | 109             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 2 | 109             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 3 | 109             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| R     | 114             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 2 | 118             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 3 | 119             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| S     | 100             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 2 | 99              | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 3 | 99              | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| T     | 99              | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 2 | 100             | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |
| Can 3 | 99              | Failure              | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | -----                 | -----          | -----       | 0 |

Freeze-Thaw Resistance: Gloss

|       | After 1 Cycle |       |       |       | After 2 Cycles |       |       |       | After 3 Cycles |       |       |       |
|-------|---------------|-------|-------|-------|----------------|-------|-------|-------|----------------|-------|-------|-------|
|       | 60° M         | 60°SD | 85° M | 85°SD | 60° M          | 60°SD | 85° M | 85°SD | 60° M          | 60°SD | 85° M | 85°SD |
| A     | 1.9           | 0.1   | 0.8   | 0.1   | 1.8            | 0.1   | 0.8   | 0.1   | 1.9            | 0.1   | 0.8   | 0.1   |
| Can 2 | 1.9           | 0.1   | 0.8   | 0.1   | 1.9            | 0.1   | 0.8   | 0.1   | 1.9            | 0.1   | 0.8   | 0.1   |
| Can 3 | 1.9           | 0.1   | 0.8   | 0.1   | 1.8            | 0.1   | 0.8   | 0.1   | 1.9            | 0.1   | 0.8   | 0.1   |
| B     | 2.6           | 0.1   | 2.2   | 0.1   | 2.4            | 0.1   | 2.1   | 0.1   | 2.5            | 0.1   | 2.2   | 0.1   |
| Can 2 | 2.6           | 0.1   | 2.2   | 0.1   | 2.4            | 0.1   | 2.1   | 0.2   | 2.5            | 0.1   | 2.2   | 0.1   |
| Can 3 | 2.6           | 0.1   | 2.2   | 0.1   | 2.4            | 0.1   | 2.1   | 0.2   | 2.5            | 0.1   | 2.1   | 0.1   |
| C     | 2             | 0.1   | 2     | 0.1   | Failure        |       |       |       | -----          |       |       |       |
| Can 2 | 2             | 0.1   | 2     | 0.1   | Failure        |       |       |       | -----          |       |       |       |
| Can 3 | 2             | 0.1   | 2.1   | 0.1   | Failure        |       |       |       | -----          |       |       |       |

|       |         |     |     |     |         |     |     |     |       |     |     |     |
|-------|---------|-----|-----|-----|---------|-----|-----|-----|-------|-----|-----|-----|
| D     | 2.1     | 0.1 | 1.6 | 0.1 | 2       | 0.1 | 1.6 | 0.1 | 2.1   | 0.1 | 1.6 | 0.1 |
| Can 2 | 2.1     | 0.1 | 1.6 | 0.1 | 2       | 0.1 | 1.5 | 0.1 | 2.2   | 0.1 | 1.5 | 0.1 |
| Can 3 | 2.1     | 0.1 | 1.6 | 0.1 | 2       | 0.1 | 1.5 | 0.1 | 2.2   | 0.1 | 1.6 | 0.1 |
| E     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| F     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| G     | 1.7     | 0.1 | 0.6 | 0.1 | Failure |     |     |     | ----- |     |     |     |
| Can 2 | 1.7     | 0.1 | 0.6 | 0.1 | Failure |     |     |     | ----- |     |     |     |
| Can 3 | 1.7     | 0.1 | 0.7 | 0.2 | Failure |     |     |     | ----- |     |     |     |
| H     | 1.8     | 0.1 | 1   | 0.2 | 1.9     | 0.1 | 1.1 | 0.1 | 1.9   | 0.1 | 1.1 | 0.1 |
| Can 2 | 1.8     | 0.2 | 1.1 | 0.1 | 1.9     | 0.1 | 1.1 | 0.1 | 1.9   | 0.1 | 1.2 | 0.1 |
| Can 3 | 1.8     | 0.1 | 1.1 | 0.1 | 1.9     | 0.1 | 1.1 | 0.1 | 1.9   | 0.1 | 1.1 | 0.1 |
| I     | 1.9     | 0.1 | 0.9 | 0.1 | 1.9     | 0.1 | 0.9 | 0.1 | 2     | 0.1 | 0.9 | 0.1 |
| Can 2 | 1.9     | 0.1 | 0.9 | 0.1 | 1.9     | 0.1 | 0.9 | 0.1 | 1.9   | 0.1 | 0.9 | 0.1 |
| Can 3 | 1.9     | 0.1 | 0.9 | 0.1 | 1.9     | 0.1 | 0.9 | 0.1 | 1.9   | 0.1 | 0.9 | 0.1 |
| J     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| K     | 2       | 0.1 | 1.8 | 0.1 | Failure |     |     |     | ----- |     |     |     |
| Can 2 | 2       | 0.1 | 1.8 | 0.1 | Failure |     |     |     | ----- |     |     |     |
| Can 3 | 2       | 0.1 | 1.8 | 0.1 | Failure |     |     |     | ----- |     |     |     |
| L     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| M     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| N     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| O     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| P     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 2 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Can 3 | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |
| Q     | Failure |     |     |     | -----   |     |     |     | ----- |     |     |     |

|       |         |       |       |
|-------|---------|-------|-------|
| Can 2 | Failure | ----- | ----- |
| Can 3 | Failure | ----- | ----- |
| R     | Failure | ----- | ----- |
| Can 2 | Failure | ----- | ----- |
| Can 3 | Failure | ----- | ----- |
| S     | Failure | ----- | ----- |
| Can 2 | Failure | ----- | ----- |
| Can 3 | Failure | ----- | ----- |
| T     | Failure | ----- | ----- |
| Can 2 | Failure | ----- | ----- |
| Can 3 | Failure | ----- | ----- |

| Continued... | After 4 Cycles |       |       |       | After 5 Cycles |       |       |       |
|--------------|----------------|-------|-------|-------|----------------|-------|-------|-------|
|              | 60° M          | 60°SD | 85° M | 85°SD | 60° M          | 60°SD | 85° M | 85°SD |
| A            | 1.9            | 0.1   | 0.8   | 0.1   | 1.8            | 0.2   | 1.8   | 0.1   |
| Can 2        | 1.9            | 0.1   | 0.8   | 0.1   | 1.9            | 0.1   | 0.8   | 0.1   |
| Can 3        | 1.9            | 0.1   | 0.8   | 0.1   | 1.9            | 0.1   | 0.8   | 0.1   |
| B            | 2.6            | 0.1   | 2.2   | 0.1   | 2.5            | 0.1   | 2.2   | 0.1   |
| Can 2        | 2.6            | 0.1   | 2.2   | 0.1   | 2.5            | 0.1   | 2.2   | 0.1   |
| Can 3        | 2.6            | 0.1   | 2.2   | 0.1   | 2.5            | 0.1   | 2.2   | 0.1   |
| C            | -----          |       |       |       | -----          |       |       |       |
| Can 2        | -----          |       |       |       | -----          |       |       |       |
| Can 3        | -----          |       |       |       | -----          |       |       |       |
| D            | 2.1            | 0.1   | 1.6   | 0.1   | 2.1            | 0.1   | 1.6   | 0.1   |
| Can 2        | 2.1            | 0.1   | 1.6   | 0.1   | 2.1            | 0.1   | 1.6   | 0.1   |
| Can 3        | 2.1            | 0.1   | 1.6   | 0.1   | 2.1            | 0.1   | 1.6   | 0.1   |
| E            | -----          |       |       |       | -----          |       |       |       |
| Can 2        | -----          |       |       |       | -----          |       |       |       |
| Can 3        | -----          |       |       |       | -----          |       |       |       |
| F            | -----          |       |       |       | -----          |       |       |       |
| Can 2        | -----          |       |       |       | -----          |       |       |       |
| Can 3        | -----          |       |       |       | -----          |       |       |       |
| G            | -----          |       |       |       | -----          |       |       |       |
| Can 2        | -----          |       |       |       | -----          |       |       |       |
| Can 3        | -----          |       |       |       | -----          |       |       |       |
| H            | 1.9            | 0.1   | 1.2   | 0.1   | Failure        |       |       |       |
| Can 2        | 1.9            | 0.1   | 1.2   | 0.1   | Failure        |       |       |       |
| Can 3        | 1.9            | 0.1   | 1.2   | 0.1   | Failure        |       |       |       |
| I            | 1.9            | 0.1   | 1     | 0.1   | 1.9            | 0.1   | 1     | 0.1   |
| Can 2        | 2              | 0.1   | 0.9   | 0.1   | 1.9            | 0.1   | 1     | 0.1   |



## Flow & Leveling

| Flat | Flow and Leveling |   |   |         |
|------|-------------------|---|---|---------|
|      | 1                 | 2 | 3 | Average |
| A    | 0                 | 0 | 0 | 0       |
| B    | 0                 | 0 | 0 | 0       |
| C    | 0                 | 0 | 0 | 0       |
| D    | 0                 | 0 | 0 | 0       |
| E    | 0                 | 0 | 0 | 0       |
| F    | 0                 | 0 | 0 | 0       |
| G    | 0                 | 0 | 0 | 0       |
| H    | 0                 | 0 | 0 | 0       |
| I    | 0                 | 0 | 0 | 0       |
| J    | 5                 | 5 | 5 | 5       |
| K    | 1                 | 1 | 0 | 1       |
| L    | 0                 | 0 | 0 | 0       |
| M    | 0                 | 0 | 0 | 0       |
| N    | 0                 | 0 | 0 | 0       |
| O    | 3                 | 3 | 3 | 3       |
| P    | 0                 | 0 | 1 | 0       |
| Q    | 0                 | 0 | 0 | 0       |
| R    | 0                 | 0 | 0 | 0       |
| S    | 0                 | 0 | 0 | 0       |
| T    | 0                 | 0 | 0 | 0       |

## Sag Resistance

| Flat | Sag |     |     |         |
|------|-----|-----|-----|---------|
|      | 1   | 2   | 3   | Average |
| A    | 12+ | 12+ | 12+ | 12+     |
| B    | 12+ | 12+ | 12+ | 12+     |
| C    | 12+ | 12+ | 12+ | 12+     |
| D    | 12+ | 12+ | 12+ | 12+     |
| E    | 12+ | 12+ | 12+ | 12+     |
| F    | 12+ | 12+ | 12+ | 12+     |
| G    | 12+ | 12+ | 12+ | 12+     |
| H    | 12+ | 12+ | 12+ | 12+     |
| I    | 12+ | 12+ | 12+ | 12+     |
| J    | 11  | 10  | 10  | 10      |
| K    | 12+ | 12+ | 12+ | 12+     |
| L    | 12+ | 12+ | 12+ | 12+     |
| M    | 12+ | 12+ | 12+ | 12+     |
| N    | 12+ | 12+ | 12+ | 12+     |
| O    | 12+ | 12+ | 12+ | 12+     |
| P    | 12+ | 12+ | 12+ | 12+     |
| Q    | 12+ | 12+ | 12+ | 12+     |
| R    | 12+ | 12+ | 12+ | 12+     |
| S    | 12+ | 12+ | 12+ | 12+     |
| T    | 12+ | 12+ | 12+ | 12+     |





Hide

|           | 3mi I- 1  |           |              | 3mil - 2  |           |              | 3mil - 3  |           |              | Avg          | AQMD Rating |
|-----------|-----------|-----------|--------------|-----------|-----------|--------------|-----------|-----------|--------------|--------------|-------------|
|           | Y (Black) | Y (White) | Cont. Rat.   | Y (Black) | Y (White) | Cont. Rat.   | Y (Black) | Y (White) | Cont. Rat.   |              |             |
| A         | 87.29     | 89.57     | 0.975        | 87.13     | 89.49     | 0.974        | 87.19     | 89.50     | 0.974        |              |             |
| Reading 2 | 87.33     | 89.44     | 0.976        | 87.38     | 89.51     | 0.976        | 87.20     | 89.46     | 0.975        |              |             |
| Reading 3 | 87.36     | 89.46     | 0.977        | 87.44     | 89.48     | 0.977        | 87.37     | 89.45     | 0.977        |              |             |
| Average   |           |           | <b>0.976</b> |           |           | <b>0.976</b> |           |           | <b>0.975</b> | <b>0.976</b> | 6           |
| B         | 87.92     | 90.55     | 0.971        | 88.27     | 90.59     | 0.974        | 88.48     | 90.71     | 0.975        |              |             |
| Reading 2 | 88.35     | 90.63     | 0.975        | 88.38     | 90.41     | 0.978        | 88.53     | 90.61     | 0.977        |              |             |
| Reading 3 | 88.41     | 90.46     | 0.977        | 88.40     | 90.46     | 0.977        | 88.61     | 90.56     | 0.978        |              |             |
| Average   |           |           | <b>0.974</b> |           |           | <b>0.976</b> |           |           | <b>0.977</b> | <b>0.976</b> | 6           |
| C         | 87.97     | 89.87     | 0.979        | 87.93     | 89.87     | 0.978        | 88.14     | 89.97     | 0.980        |              |             |
| Reading 2 | 88.02     | 89.81     | 0.980        | 87.97     | 89.85     | 0.979        | 88.00     | 89.91     | 0.979        |              |             |
| Reading 3 | 88.23     | 89.85     | 0.982        | 87.94     | 89.77     | 0.980        | 88.22     | 89.83     | 0.982        |              |             |
| Average   |           |           | <b>0.980</b> |           |           | <b>0.979</b> |           |           | <b>0.980</b> | <b>0.980</b> | 6           |
| D         | 87.69     | 89.70     | 0.978        | 87.53     | 89.86     | 0.974        | 87.82     | 89.75     | 0.978        |              |             |
| Reading 2 | 87.87     | 89.76     | 0.979        | 87.85     | 89.84     | 0.978        | 87.87     | 89.78     | 0.979        |              |             |
| Reading 3 | 87.86     | 89.61     | 0.980        | 87.58     | 89.64     | 0.977        | 87.79     | 89.68     | 0.979        |              |             |
| Average   |           |           | <b>0.979</b> |           |           | <b>0.976</b> |           |           | <b>0.979</b> | <b>0.978</b> | 6           |
| E         | 83.23     | 83.56     | 0.996        | 83.42     | 83.45     | 1.000        | 83.34     | 83.55     | 0.997        |              |             |
| Reading 2 | 83.26     | 83.58     | 0.996        | 83.24     | 83.48     | 0.997        | 83.27     | 83.49     | 0.997        |              |             |
| Reading 3 | 83.25     | 83.50     | 0.997        | 83.39     | 83.47     | 0.999        | 83.30     | 83.42     | 0.999        |              |             |
| Average   |           |           | <b>0.996</b> |           |           | <b>0.999</b> |           |           | <b>0.998</b> | <b>0.998</b> | 10          |
| F         | 82.82     | 83.50     | 0.992        | 83.09     | 83.50     | 0.995        | 82.99     | 83.55     | 0.993        |              |             |
| Reading 2 | 82.96     | 83.52     | 0.993        | 83.06     | 83.57     | 0.994        | 83.05     | 83.60     | 0.993        |              |             |
| Reading 3 | 82.71     | 83.50     | 0.991        | 83.00     | 83.51     | 0.994        | 82.98     | 83.47     | 0.994        |              |             |
| Average   |           |           | <b>0.992</b> |           |           | <b>0.994</b> |           |           | <b>0.994</b> | <b>0.993</b> | 8           |
| G         | 85.27     | 88.37     | 0.965        | 85.39     | 88.35     | 0.966        | 84.96     | 88.05     | 0.965        |              |             |
| Reading 2 | 85.24     | 88.27     | 0.966        | 85.35     | 88.24     | 0.967        | 85.18     | 88.25     | 0.965        |              |             |
| Reading 3 | 85.33     | 88.20     | 0.967        | 85.46     | 88.32     | 0.968        | 84.91     | 88.15     | 0.963        |              |             |
| Average   |           |           | <b>0.966</b> |           |           | <b>0.967</b> |           |           | <b>0.964</b> | <b>0.966</b> | 4           |
| H         | 88.71     | 90.34     | 0.982        | 88.63     | 90.26     | 0.982        | 88.33     | 90.35     | 0.978        |              |             |
| Reading 2 | 88.74     | 90.37     | 0.982        | 88.84     | 90.27     | 0.984        | 88.75     | 90.39     | 0.982        |              |             |
| Reading 3 | 88.60     | 90.28     | 0.981        | 88.75     | 90.18     | 0.984        | 88.90     | 90.28     | 0.985        |              |             |
| Average   |           |           | <b>0.982</b> |           |           | <b>0.983</b> |           |           | <b>0.981</b> | <b>0.982</b> | 6           |
| I         | 86.83     | 89.07     | 0.975        | 87.10     | 89.27     | 0.976        | 86.91     | 89.07     | 0.976        |              |             |
| Reading 2 | 87.05     | 89.09     | 0.977        | 87.36     | 89.20     | 0.979        | 87.08     | 89.13     | 0.977        |              |             |
| Reading 3 | 86.86     | 89.10     | 0.975        | 86.98     | 89.21     | 0.975        | 87.14     | 89.13     | 0.978        |              |             |
| Average   |           |           | <b>0.976</b> |           |           | <b>0.977</b> |           |           | <b>0.977</b> | <b>0.976</b> | 6           |
| J         | 81.69     | 82.94     | 0.985        | 81.76     | 82.89     | 0.986        | 81.59     | 82.78     | 0.986        |              |             |
| Reading 2 | 81.64     | 82.77     | 0.986        | 81.62     | 82.96     | 0.984        | 81.68     | 82.76     | 0.987        |              |             |
| Reading 3 | 81.62     | 82.92     | 0.984        | 81.72     | 82.83     | 0.987        | 81.75     | 82.70     | 0.989        |              |             |
| Average   |           |           | <b>0.985</b> |           |           | <b>0.986</b> |           |           | <b>0.987</b> | <b>0.986</b> | 8           |
| K         | 88.97     | 91.17     | 0.976        | 88.81     | 90.79     | 0.978        | 88.79     | 90.75     | 0.978        |              |             |
| Reading 2 | 88.97     | 90.62     | 0.982        | 89.12     | 90.88     | 0.981        | 89.08     | 90.93     | 0.980        |              |             |
| Reading 3 | 88.91     | 90.65     | 0.981        | 88.95     | 90.54     | 0.982        | 88.90     | 90.74     | 0.980        |              |             |
| Average   |           |           | <b>0.979</b> |           |           | <b>0.980</b> |           |           | <b>0.979</b> | <b>0.980</b> | 6           |
| L         | 89.72     | 91.53     | 0.980        | 89.73     | 91.53     | 0.980        | 89.64     | 91.56     | 0.979        |              |             |
| Reading 2 | 89.73     | 91.51     | 0.981        | 89.69     | 91.46     | 0.981        | 89.45     | 91.37     | 0.979        |              |             |
| Reading 3 | 89.72     | 91.37     | 0.982        | 89.53     | 91.40     | 0.980        | 89.58     | 91.55     | 0.978        |              |             |

| Average   |                  |                  | <b>0.981</b>      |                  |                  | <b>0.980</b>      |                  |                  | <b>0.979</b>      | <b>0.980</b> | 6 |
|-----------|------------------|------------------|-------------------|------------------|------------------|-------------------|------------------|------------------|-------------------|--------------|---|
|           | <b>3mi I - 1</b> |                  |                   | <b>3mil - 2</b>  |                  |                   | <b>3mil - 3</b>  |                  |                   |              |   |
| Continued | <b>Y (Black)</b> | <b>Y (White)</b> | <b>Cont. Rat.</b> | <b>Y (Black)</b> | <b>Y (White)</b> | <b>Cont. Rat.</b> | <b>Y (Black)</b> | <b>Y (White)</b> | <b>Cont. Rat.</b> |              |   |
| M         | 83.51            | 85.14            | 0.981             | 83.46            | 85.22            | 0.979             | 83.40            | 84.98            | 0.981             |              |   |
| Reading 2 | 83.46            | 85.14            | 0.980             | 83.55            | 85.01            | 0.983             | 83.53            | 84.87            | 0.984             |              |   |
| Reading 3 | 83.46            | 85.06            | 0.981             | 83.54            | 84.91            | 0.984             | 83.54            | 84.89            | 0.984             |              |   |
| Average   |                  |                  | <b>0.981</b>      |                  |                  | <b>0.982</b>      |                  |                  | <b>0.983</b>      | <b>0.982</b> | 6 |
| N         | 85.73            | 87.16            | 0.984             | 85.87            | 87.24            | 0.984             | 86.09            | 87.18            | 0.987             |              |   |
| Reading 2 | 85.84            | 87.17            | 0.985             | 85.94            | 87.16            | 0.986             | 85.85            | 87.18            | 0.985             |              |   |
| Reading 3 | 85.83            | 87.13            | 0.985             | 86.08            | 87.20            | 0.987             | 86.11            | 87.13            | 0.988             |              |   |
| Average   |                  |                  | <b>0.984</b>      |                  |                  | <b>0.986</b>      |                  |                  | <b>0.987</b>      | <b>0.986</b> | 8 |
| O         | 89.69            | 91.32            | 0.982             | 89.70            | 91.31            | 0.982             | 89.67            | 91.31            | 0.982             |              |   |
| Reading 2 | 89.58            | 91.29            | 0.981             | 89.65            | 91.20            | 0.983             | 89.81            | 91.29            | 0.984             |              |   |
| Reading 3 | 89.66            | 91.23            | 0.983             | 89.58            | 91.27            | 0.981             | 89.70            | 91.27            | 0.983             |              |   |
| Average   |                  |                  | <b>0.982</b>      |                  |                  | <b>0.982</b>      |                  |                  | <b>0.983</b>      | <b>0.982</b> | 6 |
| P         | 88.73            | 90.37            | 0.982             | 88.69            | 90.33            | 0.982             | 88.64            | 90.34            | 0.981             |              |   |
| Reading 2 | 88.67            | 90.33            | 0.982             | 88.80            | 90.34            | 0.983             | 88.92            | 90.32            | 0.984             |              |   |
| Reading 3 | 88.91            | 90.33            | 0.984             | 88.62            | 90.24            | 0.982             | 88.70            | 90.30            | 0.982             |              |   |
| Average   |                  |                  | <b>0.983</b>      |                  |                  | <b>0.982</b>      |                  |                  | <b>0.983</b>      | <b>0.983</b> | 6 |
| Q         | 89.65            | 91.12            | 0.984             | 89.47            | 91.16            | 0.981             | 89.48            | 91.08            | 0.982             |              |   |
| Reading 2 | 89.66            | 91.11            | 0.984             | 89.62            | 91.14            | 0.983             | 89.64            | 91.07            | 0.984             |              |   |
| Reading 3 | 89.51            | 91.05            | 0.983             | 89.55            | 91.09            | 0.983             | 89.66            | 91.07            | 0.985             |              |   |
| Average   |                  |                  | <b>0.984</b>      |                  |                  | <b>0.983</b>      |                  |                  | <b>0.984</b>      | <b>0.983</b> | 6 |
| R         | 84.33            | 85.34            | 0.988             | 84.28            | 85.37            | 0.987             | 84.19            | 85.32            | 0.987             |              |   |
| Reading 2 | 84.28            | 85.32            | 0.988             | 84.31            | 85.33            | 0.988             | 84.31            | 85.33            | 0.988             |              |   |
| Reading 3 | 84.27            | 85.33            | 0.988             | 84.25            | 85.30            | 0.988             | 84.37            | 85.33            | 0.989             |              |   |
| Average   |                  |                  | <b>0.988</b>      |                  |                  | <b>0.988</b>      |                  |                  | <b>0.988</b>      | <b>0.988</b> | 8 |
| S         | 88.30            | 90.38            | 0.977             | 88.27            | 90.39            | 0.977             | 88.18            | 90.36            | 0.976             |              |   |
| Reading 2 | 88.33            | 90.37            | 0.977             | 88.32            | 90.33            | 0.978             | 88.36            | 90.37            | 0.978             |              |   |
| Reading 3 | 88.43            | 90.29            | 0.979             | 88.44            | 90.33            | 0.979             | 88.33            | 90.33            | 0.978             |              |   |
| Average   |                  |                  | <b>0.978</b>      |                  |                  | <b>0.978</b>      |                  |                  | <b>0.977</b>      | <b>0.978</b> | 6 |
| T         | 87.85            | 90.67            | 0.969             | 87.84            | 90.76            | 0.968             | 87.64            | 90.72            | 0.966             |              |   |
| Reading 2 | 87.89            | 90.60            | 0.970             | 88.08            | 90.73            | 0.971             | 87.96            | 90.65            | 0.970             |              |   |
| Reading 3 | 88.03            | 90.61            | 0.972             | 87.75            | 90.64            | 0.968             | 88.16            | 90.69            | 0.972             |              |   |
| Average   |                  |                  | <b>0.970</b>      |                  |                  | <b>0.969</b>      |                  |                  | <b>0.969</b>      | <b>0.970</b> | 4 |

## Tests for Interior Flat Paints

### Adhesion

|                | <b>Cross-Hatch Adhesion - Leneta Chart</b> |                  |                          | AQMD     |
|----------------|--|------------------|--------------------------|----------|
|                | <b>Rating</b>                              | <b>Failure %</b> | <b>Failure Mechanism</b> | Rating   |
| J              | 5B   | 0.5              | Substrate                | 5        |
| Replicate 2    | 3B   | 10.0             | Substrate                | 3        |
| Replicate 3    | 5B   | 0.0              | -----                    | 5        |
| <b>Average</b> | <b>4B</b>                                  | <b>3.5</b>       | <b>Substrate</b>         | <b>4</b> |
| K              | 5B   | 0.0              | -----                    | 5        |
| Replicate 2    | 1B   | 40.0             | Substrate                | 1        |

|                |           |             |                         |          |
|----------------|-----------|-------------|-------------------------|----------|
| Replicate 3    | 5B        | 0.0         | -----                   | 5        |
| <b>Average</b> | <b>4B</b> | <b>13.3</b> | <b>Substrate</b>        | <b>4</b> |
| L              | 3B        | 10.0        | Substrate               | 3        |
| Replicate 2    | 3B        | 5.0         | Substrate               | 3        |
| Replicate 3    | 3B        | 5.0         | Substrate               | 3        |
| <b>Average</b> | <b>3B</b> | <b>6.7</b>  | <b>Substrate</b>        | <b>3</b> |
| M              | 5B        | 0.5         | Substrate               | 5        |
| Replicate 2    | 5B        | 0.0         | -----                   | 5        |
| Replicate 3    | 5B        | 0.0         | -----                   | 5        |
| <b>Average</b> | <b>5B</b> | <b>0.2</b>  | <b>Substrate</b>        | <b>5</b> |
| N              | 2B        | 25.0        | 20 Substrate 5 Adhesion | 2        |
| Replicate 2    | 5B        | 0.0         | -----                   | 5        |
| Replicate 3    | 5B        | 0.5         | Substrate               | 5        |
| <b>Average</b> | <b>4B</b> | <b>8.5</b>  | <b>Substrate</b>        | <b>4</b> |
| O              | 3B        | 6.0         | 1 Substrate 5 Adhesion  | 3        |
| Replicate 2    | 4B        | 4.0         | 3 Substrate 1 Adhesion  | 4        |
| Replicate 3    | 3B        | 8.0         | 1 Substrate 7 Adhesion  | 3        |
| <b>Average</b> | <b>3B</b> | <b>6.0</b>  | <b>Adhesion</b>         | <b>3</b> |
| P              | 3B        | 5.0         | Adhesion                | 3        |
| Replicate 2    | 3B        | 5.0         | Adhesion                | 3        |
| Replicate 3    | 3B        | 10.0        | Adhesion                | 3        |
| <b>Average</b> | <b>3B</b> | <b>6.7</b>  | <b>Adhesion</b>         | <b>3</b> |
| Q              | 2B        | 20.0        | Adhesion                | 2        |
| Replicate 2    | 2B        | 25.0        | Adhesion                | 2        |
| Replicate 3    | 2B        | 25.0        | Adhesion                | 2        |
| <b>Average</b> | <b>2B</b> | <b>23.3</b> | <b>Adhesion</b>         | <b>2</b> |
| R              | 4B        | 2.0         | Substrate               | 4        |
| Replicate 2    | 4B        | 1.0         | Substrate               | 4        |
| Replicate 3    | 3B        | 5.0         | Substrate               | 3        |
| <b>Average</b> | <b>4B</b> | <b>2.7</b>  | <b>Substrate</b>        | <b>4</b> |
| S              | 3B        | 5.0         | 4 Substrate 1 Adhesion  | 3        |
| Replicate 2    | 4B        | 4.0         | 1 Substrate 3 Adhesion  | 4        |
| Replicate 3    | 4B        | 3.0         | Substrate               | 4        |
| <b>Average</b> | <b>4B</b> | <b>4.0</b>  | <b>Substrate</b>        | <b>4</b> |
| T              | 4B        | 3.0         | 2 Substrate 1 Adhesion  | 4        |
| Replicate 2    | 5B        | 0.0         | -----                   | 5        |
| Replicate 3    | 5B        | 0.0         | -----                   | 5        |
| <b>Average</b> | <b>5B</b> | <b>1.0</b>  | <b>Substrate</b>        | <b>5</b> |

Scrub

|   | Panel 1  |        | Panel 2  |        | Panel 3  |        | Standard | Sample | Panel 4  |        |
|---|----------|--------|----------|--------|----------|--------|----------|--------|----------|--------|
|   | Standard | Sample | Standard | Sample | Standard | Sample | Avg      | Avg    | Standard | Sample |
| J | 200      | 1081   | 206      | 1161   | 182      | 1025   | 196      | 1089   | -----    | -----  |
| K | 192      | 779    | 203      | 739    | 202      | 1074   | 199      | 864    | -----    | -----  |
| L | 197      | 620    | 206      | 714    | 228      | 720    | 210      | 685    | -----    | -----  |
| M | 240      | 2156   | 195      | 1765   | 203      | 2397   | 213      | 2106   | -----    | -----  |
| N | 304      | 962    | 265      | 787    | 277      | 921    | 282      | 890    | -----    | -----  |
| O | 257      | 691    | 219      | 297    | 221      | 625    | 223      | 645    | 195      | 965    |
| P | 254      | 1008   | 237      | 798    | 206      | 917    | 232      | 908    | -----    | -----  |
| Q | 223      | 1004   | 203      | 1015   | 200      | 726    | 209      | 915    | -----    | -----  |

|   |     |      |     |     |     |      |     |      |       |       |
|---|-----|------|-----|-----|-----|------|-----|------|-------|-------|
| R | 230 | 754  | 226 | 666 | 195 | 600  | 217 | 673  | ----- | ----- |
| S | 218 | 334  | 203 | 303 | 198 | 287  | 206 | 308  | ----- | ----- |
| T | 239 | 1408 | 194 | 992 | 216 | 1292 | 216 | 1231 |       |       |



|                |           |          |          |          |             |             |             |             |             |             |             |             |             |
|----------------|-----------|----------|----------|----------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Replicate 2    | 7         | 3        | 3        | 0        | None        |
| Replicate 3    | 7         | 3        | 3        | 0        | None        |
| <b>Average</b> | <b>7</b>  | <b>3</b> | <b>3</b> | <b>0</b> | <b>None</b> |
| T              | 10        | 3        | 3        | 0        | None        |
| Replicate 2    | 10        | 3        | 3        | 0        | None        |
| Replicate 3    | 10        | 3        | 3        | 0        | None        |
| <b>Average</b> | <b>10</b> | <b>3</b> | <b>3</b> | <b>0</b> | <b>None</b> |

Stain Resistance - Color

|             | Ketchup |       |         |       |         |       |             | Mustard |       |         |       |         |       |             |
|-------------|---------|-------|---------|-------|---------|-------|-------------|---------|-------|---------|-------|---------|-------|-------------|
|             | X (Pre) | X     | Y (Pre) | Y     | Z (Pre) | Z     | ΔE          | X (Pre) | X     | Y (Pre) | Y     | Z (Pre) | Z     | ΔE          |
| J           | 76.36   | 77.27 | 80.97   | 81.97 | 85.79   | 86.69 | 0.46        | 76.68   | 77.34 | 81.30   | 82.03 | 86.13   | 86.60 | 0.40        |
| Replicate 2 | 76.46   | 77.24 | 81.07   | 81.93 | 85.89   | 86.68 | 0.40        | 76.40   | 77.34 | 81.00   | 82.04 | 85.83   | 86.67 | 0.50        |
| Replicate 3 | 76.43   | 77.11 | 81.05   | 81.81 | 85.97   | 86.71 | 0.35        | 76.40   | 77.08 | 81.02   | 81.78 | 85.94   | 86.54 | 0.38        |
| Average     | 76.42   | 77.21 | 81.03   | 81.90 | 85.88   | 86.69 | <b>0.40</b> | 76.49   | 77.25 | 81.11   | 81.95 | 85.97   | 86.60 | <b>0.43</b> |
| K           | 82.49   | 83.22 | 87.59   | 88.43 | 92.45   | 93.23 | 0.38        | 82.90   | 83.28 | 88.02   | 88.51 | 92.95   | 92.91 | 0.45        |
| Replicate 2 | 82.06   | 83.09 | 87.14   | 88.29 | 92.03   | 93.21 | 0.50        | 82.50   | 83.19 | 87.60   | 88.42 | 92.46   | 92.83 | 0.50        |
| Replicate 3 | 82.13   | 82.63 | 87.21   | 87.82 | 92.23   | 92.87 | 0.29        | 82.36   | 82.88 | 87.46   | 88.10 | 92.46   | 92.73 | 0.41        |
| Average     | 82.23   | 82.98 | 87.31   | 88.18 | 92.24   | 93.10 | <b>0.39</b> | 82.59   | 83.12 | 87.69   | 88.34 | 92.62   | 92.82 | <b>0.45</b> |
| L           | 84.68   | 84.60 | 89.84   | 89.78 | 94.84   | 94.42 | 0.25        | 84.79   | 83.90 | 89.95   | 89.13 | 94.92   | 92.15 | 1.36        |
| Replicate 2 | 84.46   | 84.30 | 89.61   | 89.47 | 94.68   | 94.22 | 0.22        | 84.60   | 83.47 | 89.76   | 88.70 | 94.81   | 91.65 | 1.48        |
| Replicate 3 | 84.32   | 84.08 | 89.46   | 89.23 | 94.55   | 94.00 | 0.23        | 84.32   | 83.32 | 89.46   | 88.53 | 94.55   | 91.77 | 1.31        |
| Average     | 84.49   | 84.33 | 89.64   | 89.49 | 94.69   | 94.21 | <b>0.23</b> | 84.57   | 83.56 | 89.72   | 88.79 | 94.76   | 91.86 | <b>1.38</b> |
| M           | 78.59   | 78.67 | 83.41   | 83.52 | 87.06   | 87.12 | 0.07        | 78.75   | 78.51 | 83.59   | 83.36 | 87.28   | 86.59 | 0.34        |
| Replicate 2 | 78.51   | 78.55 | 83.33   | 83.39 | 87.06   | 87.11 | 0.03        | 78.48   | 78.17 | 83.30   | 83.00 | 87.07   | 86.53 | 0.21        |
| Replicate 3 | 78.29   | 78.28 | 83.11   | 83.11 | 86.92   | 86.98 | 0.04        | 78.33   | 78.16 | 83.15   | 82.99 | 87.00   | 86.69 | 0.12        |
| Average     | 78.46   | 78.50 | 83.28   | 83.34 | 87.01   | 87.07 | <b>0.05</b> | 78.52   | 78.28 | 83.35   | 83.12 | 87.12   | 86.60 | <b>0.22</b> |
| N           | 80.34   | 80.37 | 85.22   | 85.28 | 89.58   | 89.62 | 0.06        | 80.52   | 80.29 | 85.40   | 85.21 | 89.75   | 88.89 | 0.48        |
| Replicate 2 | 80.22   | 80.21 | 85.11   | 85.13 | 89.57   | 89.48 | 0.11        | 80.39   | 79.92 | 85.28   | 84.86 | 89.70   | 88.37 | 0.67        |
| Replicate 3 | 80.02   | 80.05 | 84.90   | 84.96 | 89.44   | 89.46 | 0.08        | 80.22   | 79.79 | 85.11   | 84.75 | 89.61   | 88.02 | 0.89        |
| Average     | 80.19   | 80.21 | 85.08   | 85.12 | 89.53   | 89.52 | <b>0.08</b> | 80.38   | 80.00 | 85.26   | 84.94 | 89.69   | 88.43 | <b>0.68</b> |
| O           | 83.87   | 83.74 | 88.90   | 88.88 | 93.21   | 93.15 | 0.07        | 83.76   | 82.97 | 88.88   | 88.15 | 93.14   | 90.71 | 1.20        |
| Replicate 2 | 83.53   | 83.51 | 88.64   | 88.64 | 92.97   | 93.12 | 0.11        | 83.39   | 82.98 | 88.49   | 88.14 | 92.78   | 91.61 | 0.59        |
| Replicate 3 | 83.40   | 83.39 | 88.50   | 88.51 | 92.88   | 93.01 | 0.09        | 83.41   | 82.81 | 88.52   | 87.97 | 92.92   | 91.30 | 0.75        |
| Average     | 83.60   | 83.55 | 88.68   | 88.68 | 93.02   | 93.09 | <b>0.09</b> | 83.52   | 82.92 | 88.63   | 88.09 | 92.95   | 91.21 | <b>0.85</b> |
| P           | 83.03   | 82.57 | 88.12   | 87.75 | 92.97   | 91.99 | 0.49        | 83.09   | 82.24 | 88.19   | 87.41 | 93.06   | 91.24 | 0.79        |
| Replicate 2 | 82.65   | 82.30 | 87.72   | 87.45 | 92.62   | 92.09 | 0.28        | 82.79   | 81.83 | 87.88   | 87.00 | 92.84   | 90.76 | 0.91        |
| Replicate 3 | 82.73   | 82.17 | 87.81   | 87.33 | 92.79   | 91.81 | 0.44        | 82.81   | 82.01 | 87.90   | 87.15 | 92.90   | 91.52 | 0.54        |
| Average     | 82.80   | 82.35 | 87.88   | 87.51 | 92.79   | 91.96 | <b>0.40</b> | 82.90   | 82.03 | 87.99   | 87.19 | 92.93   | 91.17 | <b>0.75</b> |

|             |                |          |                |          |                |          |             |                   |          |                |          |                |          |              |
|-------------|----------------|----------|----------------|----------|----------------|----------|-------------|-------------------|----------|----------------|----------|----------------|----------|--------------|
| Q           | 84.06          | 83.53    | 89.23          | 88.73    | 92.92          | 92.05    | 0.34        | 83.99             | 82.71    | 89.15          | 87.96    | 92.91          | 89.71    | 1.47         |
| Replicate 2 | 83.74          | 83.18    | 88.89          | 88.36    | 92.67          | 91.81    | 0.33        | 83.77             | 82.17    | 88.92          | 87.42    | 92.75          | 88.59    | 1.95         |
| Replicate 3 | 83.56          | 83.06    | 88.71          | 88.24    | 92.57          | 91.88    | 0.26        | 83.62             | 82.57    | 88.77          | 87.78    | 92.65          | 90.17    | 1.10         |
| Average     | 83.79          | 83.26    | 88.94          | 88.44    | 92.72          | 91.91    | <b>0.31</b> | 83.79             | 82.48    | 88.95          | 87.72    | 92.77          | 89.49    | <b>1.51</b>  |
| R           | 78.54          | 78.52    | 83.52          | 83.53    | 87.51          | 87.23    | 0.21        | 78.68             | 76.86    | 83.68          | 82.42    | 87.76          | 79.26    | 5.48         |
| Replicate 2 | 78.38          | 78.23    | 83.37          | 83.23    | 87.53          | 87.00    | 0.28        | 78.49             | 76.73    | 83.49          | 82.28    | 87.67          | 79.38    | 5.35         |
| Replicate 3 | 78.34          | 78.22    | 83.33          | 83.23    | 87.48          | 87.06    | 0.23        | 78.37             | 76.63    | 83.36          | 82.22    | 87.52          | 78.95    | 5.63         |
| Average     | 78.42          | 78.32    | 83.41          | 83.33    | 87.51          | 87.10    | <b>0.24</b> | 78.51             | 76.74    | 83.51          | 82.31    | 87.65          | 79.20    | <b>5.49</b>  |
| S           | 81.33          | 81.02    | 86.44          | 86.23    | 91.01          | 89.80    | 0.74        | 81.83             | 79.26    | 86.96          | 84.95    | 91.37          | 82.32    | 5.24         |
| Replicate 2 | 81.06          | 80.71    | 86.46          | 85.91    | 90.87          | 89.77    | 0.62        | 81.47             | 79.75    | 86.59          | 85.17    | 91.15          | 85.39    | 3.18         |
| Replicate 3 | 81.01          | 80.79    | 86.12          | 85.99    | 90.83          | 89.82    | 0.63        | 81.46             | 79.59    | 86.58          | 85.07    | 91.18          | 84.90    | 3.51         |
| Average     | 81.13          | 80.84    | 86.34          | 86.04    | 90.90          | 89.80    | <b>0.66</b> | 81.59             | 79.53    | 86.71          | 85.06    | 91.23          | 84.20    | <b>3.98</b>  |
| T           | 81.25          | 81.08    | 86.29          | 86.18    | 91.61          | 91.13    | 0.28        | 81.15             | 78.97    | 86.19          | 84.46    | 91.53          | 84.05    | 4.24         |
| Replicate 2 | 80.81          | 80.67    | 85.83          | 85.78    | 91.21          | 90.73    | 0.30        | 80.87             | 78.32    | 85.90          | 83.87    | 91.29          | 82.73    | 4.87         |
| Replicate 3 | 80.68          | 80.61    | 85.70          | 85.70    | 91.17          | 90.71    | 0.35        | 80.62             | 78.21    | 85.64          | 83.73    | 91.11          | 83.07    | 4.57         |
| Average     | 80.91          | 80.79    | 85.94          | 85.89    | 91.33          | 90.86    | <b>0.31</b> | 80.88             | 78.50    | 85.91          | 84.02    | 91.31          | 83.28    | <b>4.56</b>  |
|             | <b>Wine</b>    |          |                |          |                |          |             | <b>Red Crayon</b> |          |                |          |                |          |              |
|             | <b>X (Pre)</b> | <b>X</b> | <b>Y (Pre)</b> | <b>Y</b> | <b>Z (Pre)</b> | <b>Z</b> | <b>ΔE</b>   | <b>X (Pre)</b>    | <b>X</b> | <b>Y (Pre)</b> | <b>Y</b> | <b>Z (Pre)</b> | <b>Z</b> | <b>ΔE</b>    |
| J           | 76.84          | 74.09    | 81.47          | 78.65    | 86.30          | 80.61    | 2.37        | 76.58             | 66.17    | 81.20          | 66.47    | 85.97          | 60.43    | 13.62        |
| Replicate 2 | 76.46          | 74.32    | 81.07          | 78.89    | 85.91          | 81.12    | 2.08        | 76.57             | 67.26    | 81.19          | 68.01    | 86.02          | 62.96    | 12.11        |
| Replicate 3 | 76.52          | 73.85    | 81.15          | 78.42    | 86.08          | 80.56    | 2.31        | 76.33             | 68.29    | 80.94          | 69.50    | 85.82          | 65.06    | 10.83        |
| Average     | 76.61          | 74.09    | 81.23          | 78.65    | 86.10          | 80.76    | <b>2.25</b> | 76.49             | 67.24    | 81.11          | 67.99    | 85.94          | 62.82    | <b>12.19</b> |
| K           | 83.00          | 80.81    | 88.13          | 85.79    | 93.05          | 88.16    | 1.96        | 82.68             | 69.73    | 87.80          | 69.19    | 92.67          | 64.21    | 15.12        |
| Replicate 2 | 82.50          | 80.50    | 87.60          | 85.47    | 92.44          | 87.70    | 1.97        | 82.44             | 69.42    | 87.54          | 68.84    | 92.36          | 62.58    | 15.78        |
| Replicate 3 | 82.25          | 80.04    | 87.35          | 84.99    | 92.35          | 87.33    | 2.04        | 82.27             | 69.92    | 87.37          | 69.54    | 92.34          | 64.71    | 14.68        |
| Average     | 82.58          | 80.45    | 87.69          | 85.42    | 92.61          | 87.73    | <b>1.99</b> | 82.46             | 69.69    | 87.57          | 69.19    | 92.46          | 63.83    | <b>15.19</b> |
| L           | 84.91          | 80.40    | 90.08          | 85.37    | 94.97          | 85.97    | 3.47        | 84.83             | 72.10    | 90.00          | 72.19    | 94.95          | 64.34    | 15.29        |
| Replicate 2 | 84.67          | 80.06    | 89.83          | 85.04    | 94.78          | 85.79    | 3.45        | 84.52             | 72.91    | 89.67          | 73.43    | 94.70          | 67.01    | 13.66        |
| Replicate 3 | 84.43          | 80.99    | 89.58          | 86.00    | 94.61          | 87.27    | 2.91        | 84.43             | 74.84    | 89.58          | 76.27    | 94.65          | 72.24    | 10.69        |
| Average     | 84.67          | 80.48    | 89.83          | 85.47    | 94.79          | 86.34    | <b>3.28</b> | 84.59             | 73.28    | 89.75          | 73.96    | 94.77          | 67.86    | <b>13.21</b> |
| M           | 78.71          | 77.15    | 83.53          | 81.86    | 87.16          | 83.77    | 1.40        | 78.85             | 69.36    | 83.68          | 70.09    | 87.29          | 64.79    | 11.85        |
| Replicate 2 | 78.50          | 76.37    | 83.32          | 81.02    | 87.02          | 82.68    | 1.73        | 78.61             | 68.46    | 83.43          | 68.79    | 87.12          | 62.89    | 13.00        |
| Replicate 3 | 78.39          | 76.22    | 83.21          | 80.87    | 87.04          | 82.71    | 1.71        | 78.45             | 68.36    | 83.27          | 68.72    | 87.02          | 63.25    | 12.75        |
| Average     | 78.53          | 76.58    | 83.35          | 81.25    | 87.07          | 83.05    | <b>1.61</b> | 78.64             | 68.73    | 83.46          | 69.20    | 87.14          | 63.64    | <b>12.53</b> |
| N           | 80.52          | 77.09    | 85.42          | 81.75    | 89.79          | 83.40    | 2.43        | 80.46             | 62.38    | 85.35          | 59.80    | 89.76          | 54.20    | 20.64        |
| Replicate 2 | 80.34          | 76.11    | 85.23          | 80.71    | 89.69          | 82.11    | 2.85        | 80.36             | 60.71    | 85.24          | 57.57    | 89.67          | 51.71    | 22.47        |
| Replicate 3 | 80.18          | 77.16    | 85.06          | 81.86    | 89.56          | 83.79    | 2.22        | 80.34             | 57.52    | 85.22          | 53.18    | 89.69          | 46.35    | 26.70        |
| Average     | 80.35          | 76.79    | 85.24          | 81.44    | 89.68          | 83.10    | <b>2.50</b> | 80.39             | 60.20    | 85.27          | 56.85    | 89.71          | 50.75    | <b>23.27</b> |
| O           | 83.79          | 81.89    | 88.91          | 86.87    | 93.14          | 89.32    | 1.45        | 83.91             | 58.92    | 89.03          | 53.80    | 92.37          | 46.31    | 28.96        |
| Replicate 2 | 83.56          | 82.31    | 88.67          | 87.35    | 92.99          | 90.36    | 1.02        | 83.66             | 56.70    | 88.78          | 50.80    | 93.06          | 42.64    | 31.98        |

|             |       |       |       |       |       |       |             |       |       |       |       |       |       |              |
|-------------|-------|-------|-------|-------|-------|-------|-------------|-------|-------|-------|-------|-------|-------|--------------|
| Replicate 3 | 83.38 | 82.08 | 88.49 | 87.12 | 92.89 | 90.33 | 0.97        | 83.52 | 59.97 | 88.63 | 55.44 | 92.99 | 48.62 | 26.89        |
| Average     | 83.58 | 82.09 | 88.69 | 87.11 | 93.01 | 90.00 | <b>1.15</b> | 83.70 | 58.53 | 88.81 | 53.35 | 92.81 | 45.86 | <b>29.28</b> |
| P           | 83.08 | 78.37 | 88.17 | 83.24 | 93.04 | 85.77 | 2.57        | 83.02 | 71.41 | 88.10 | 71.51 | 92.98 | 64.97 | 14.38        |
| Replicate 2 | 82.86 | 78.55 | 87.95 | 83.45 | 92.92 | 86.33 | 2.32        | 82.76 | 72.76 | 87.84 | 73.49 | 92.81 | 68.52 | 12.31        |
| Replicate 3 | 82.77 | 78.24 | 87.85 | 83.14 | 92.86 | 85.98 | 2.43        | 82.65 | 72.57 | 87.73 | 73.31 | 92.74 | 69.74 | 11.69        |
| Average     | 82.90 | 78.39 | 87.99 | 83.28 | 92.94 | 86.03 | <b>2.44</b> | 82.81 | 72.25 | 87.89 | 72.77 | 92.84 | 67.74 | <b>12.79</b> |
| Q           | 83.99 | 79.33 | 89.14 | 84.24 | 93.00 | 84.18 | 2.36        | 84.04 | 68.27 | 89.19 | 66.95 | 93.01 | 61.92 | 16.90        |
| Replicate 2 | 83.73 | 78.07 | 88.87 | 82.92 | 92.80 | 82.40 | 3.94        | 83.84 | 70.90 | 88.98 | 70.78 | 92.85 | 67.05 | 13.52        |
| Replicate 3 | 83.60 | 79.22 | 88.74 | 84.16 | 92.73 | 84.32 | 3.23        | 83.71 | 67.66 | 88.86 | 66.30 | 92.81 | 59.30 | 17.92        |
| Average     | 83.77 | 78.87 | 88.92 | 83.77 | 92.84 | 83.63 | <b>3.18</b> | 83.86 | 68.94 | 89.01 | 68.01 | 92.89 | 62.76 | <b>16.11</b> |
| R           | 78.56 | 77.12 | 83.55 | 82.12 | 87.62 | 85.17 | 0.95        | 78.55 | 69.23 | 83.55 | 70.73 | 87.64 | 70.80 | 8.86         |
| Replicate 2 | 78.44 | 77    | 83.43 | 82.01 | 87.58 | 85.23 | 0.90        | 78.39 | 67.67 | 83.38 | 68.71 | 87.55 | 68.60 | 10.14        |
| Replicate 3 | 78.39 | 77.04 | 83.39 | 82.04 | 87.63 | 85.32 | 0.89        | 78.26 | 69.89 | 83.25 | 71.72 | 87.52 | 72.34 | 7.95         |
| Average     | 78.46 | 77.05 | 83.46 | 82.06 | 87.61 | 85.24 | <b>0.91</b> | 78.40 | 68.93 | 83.39 | 70.39 | 87.57 | 70.58 | <b>8.98</b>  |
| S           | 81.70 | 77.67 | 86.82 | 82.69 | 91.23 | 86.05 | 1.90        | 81.63 | 74.14 | 86.75 | 76.13 | 91.17 | 77.38 | 7.34         |
| Replicate 2 | 81.46 | 76.88 | 86.57 | 81.87 | 91.13 | 85.33 | 2.14        | 81.40 | 72.32 | 86.51 | 73.75 | 91.01 | 74.62 | 8.81         |
| Replicate 3 | 81.28 | 76.87 | 86.39 | 81.87 | 91.00 | 85.36 | 2.08        | 81.37 | 70.94 | 86.48 | 71.95 | 91.06 | 72.18 | 10.06        |
| Average     | 81.48 | 77.14 | 86.59 | 82.14 | 91.12 | 85.58 | <b>2.04</b> | 81.47 | 72.47 | 86.58 | 73.94 | 91.08 | 74.73 | <b>8.74</b>  |
| T           | 81.22 | 78.98 | 86.25 | 83.94 | 91.58 | 87.53 | 1.50        | 81.16 | 70.68 | 86.20 | 71.40 | 91.55 | 71.19 | 10.77        |
| Replicate 2 | 80.80 | 77.87 | 85.83 | 82.8  | 91.24 | 86.2  | 1.85        | 80.82 | 70.87 | 85.84 | 71.86 | 91.23 | 72.33 | 9.99         |
| Replicate 3 | 80.65 | 78.12 | 85.67 | 83.06 | 91.15 | 86.69 | 1.65        | 80.64 | 70.89 | 85.65 | 71.93 | 91.11 | 71.98 | 9.99         |
| Average     | 80.89 | 78.32 | 85.92 | 83.27 | 91.32 | 86.81 | <b>1.67</b> | 80.87 | 70.81 | 85.90 | 71.73 | 91.30 | 71.83 | <b>10.25</b> |

Stain Resistance - Gloss

|              | Ketchup - After |            |            |            | Mustard - After |            |            |            | Wine - After |            |            |            | Red Crayon - After |            |            |            |
|--------------|-----------------|------------|------------|------------|-----------------|------------|------------|------------|--------------|------------|------------|------------|--------------------|------------|------------|------------|
|              | 60° M           | 60°SD      | 85° M      | 85°SD      | 60° M           | 60°SD      | 85° M      | 85°SD      | 60° M        | 60°SD      | 85° M      | 85°SD      | 60° M              | 60°SD      | 85° M      | 85°SD      |
| <b>J-Pre</b> | 2.4             | 0.1        | 4.0        | 0.2        | 2.4             | 0.1        | 3.9        | 0.2        | 2.4          | 0.1        | 3.9        | 0.2        | 2.4                | 0.1        | 3.9        | 0.1        |
| Strip 1      | 2.6             | 0.1        | 4.6        | 0.2        | 2.5             | 0.1        | 4.5        | 0.1        | 2.5          | 0.1        | 4.8        | 0.2        | 3.3                | 0.1        | 9.3        | 0.2        |
| Strip 2      | 2.6             | 0.1        | 4.7        | 0.1        | 2.5             | 0.1        | 4.5        | 0.1        | 2.5          | 0.1        | 4.6        | 0.2        | 3.2                | 0.2        | 8.8        | 0.6        |
| Strip 3      | 2.6             | 0.1        | 4.6        | 0.2        | 2.5             | 0.1        | 4.4        | 0.1        | 2.5          | 0.1        | 4.3        | 0.2        | 3.1                | 0.2        | 8.7        | 0.6        |
| Avg          | <b>2.6</b>      | <b>0.1</b> | <b>4.6</b> | <b>0.2</b> | <b>2.5</b>      | <b>0.1</b> | <b>4.5</b> | <b>0.1</b> | <b>2.5</b>   | <b>0.1</b> | <b>4.6</b> | <b>0.2</b> | <b>3.2</b>         | <b>0.2</b> | <b>8.9</b> | <b>0.5</b> |
| <b>K-Pre</b> | 2.0             | 0.1        | 1.8        | 0.1        | 1.9             | 0.1        | 1.8        | 0.1        | 2.0          | 0.1        | 1.8        | 0.1        | 1.9                | 0.1        | 1.8        | 0.1        |
| Strip 1      | 2.1             | 0.1        | 2.7        | 0.2        | 2.1             | 0.1        | 2.6        | 0.1        | 2.0          | 0.1        | 2.7        | 0.1        | 2.3                | 0.1        | 5.2        | 0.1        |
| Strip 2      | 2.1             | 0.1        | 2.5        | 0.2        | 2.1             | 0.1        | 2.5        | 0.1        | 2.0          | 0.1        | 2.7        | 0.1        | 2.4                | 0.1        | 5.5        | 0.2        |
| Strip 3      | 2.1             | 0.1        | 2.5        | 0.2        | 2.1             | 0.1        | 2.5        | 0.1        | 2.0          | 0.1        | 2.6        | 0.1        | 2.4                | 0.1        | 5.6        | 0.2        |
| Avg          | <b>2.1</b>      | <b>0.1</b> | <b>2.6</b> | <b>0.2</b> | <b>2.1</b>      | <b>0.1</b> | <b>2.5</b> | <b>0.1</b> | <b>2.0</b>   | <b>0.1</b> | <b>2.7</b> | <b>0.1</b> | <b>2.4</b>         | <b>0.1</b> | <b>5.4</b> | <b>0.2</b> |
| <b>L-Pre</b> | 2.0             | 0.1        | 3.0        | 0.1        | 2.0             | 0.1        | 3.0        | 0.1        | 2.0          | 0.1        | 3.0        | 0.1        | 2.0                | 0.1        | 3.0        | 0.1        |
| Strip 1      | 2.1             | 0.1        | 4.5        | 0.2        | 2.4             | 0.1        | 4.6        | 0.2        | 2.0          | 0.1        | 4.5        | 0.2        | 3.0                | 0.2        | 9.4        | 1.4        |
| Strip 2      | 2.1             | 0.1        | 4.1        | 0.2        | 2.4             | 0.1        | 4.5        | 0.2        | 2.0          | 0.1        | 4.1        | 0.1        | 2.9                | 0.2        | 9.4        | 0.6        |

|              |            |            |            |            |            |            |            |            |            |            |            |            |            |            |             |            |
|--------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|-------------|------------|
| Strip 3      | 2.1        | 0.1        | 4.1        | 0.2        | 2.3        | 0.1        | 4.3        | 0.1        | 2.0        | 0.1        | 4.1        | 0.2        | 2.5        | 0.2        | 7.5         | 0.6        |
| Avg          | <b>2.1</b> | <b>0.1</b> | <b>4.2</b> | <b>0.2</b> | <b>2.4</b> | <b>0.1</b> | <b>4.5</b> | <b>0.2</b> | <b>2.0</b> | <b>0.1</b> | <b>4.2</b> | <b>0.2</b> | <b>2.8</b> | <b>0.2</b> | <b>8.8</b>  | <b>0.9</b> |
| <b>M-Pre</b> | 1.9        | 0.1        | 1.1        | 0.1        | 1.9        | 0.1        | 0.8        | 0.2        | 1.9        | 0.1        | 1.1        | 0.1        | 1.9        | 0.1        | 1.1         | 0.1        |
| Strip 1      | 1.9        | 0.1        | 1.6        | 0.1        | 1.9        | 0.1        | 1.5        | 0.1        | 1.8        | 0.1        | 1.5        | 0.1        | 2.1        | 0.2        | 3.7         | 0.4        |
| Strip 2      | 1.9        | 0.1        | 1.6        | 0.1        | 1.9        | 0.1        | 1.5        | 0.1        | 1.8        | 0.1        | 1.5        | 0.1        | 2.0        | 0.1        | 3.6         | 0.4        |
| Strip 3      | 1.8        | 0.1        | 1.4        | 0.1        | 1.8        | 0.1        | 1.5        | 0.2        | 1.8        | 0.1        | 1.5        | 0.1        | 2.2        | 0.1        | 3.6         | 0.2        |
| Avg          | <b>1.9</b> | <b>0.1</b> | <b>1.5</b> | <b>0.1</b> | <b>1.9</b> | <b>0.1</b> | <b>1.5</b> | <b>0.1</b> | <b>1.8</b> | <b>0.1</b> | <b>1.5</b> | <b>0.1</b> | <b>2.1</b> | <b>0.1</b> | <b>3.6</b>  | <b>0.3</b> |
| <b>N-Pre</b> | 2.3        | 0.1        | 4.5        | 0.1        | 2.3        | 0.1        | 4.6        | 0.1        | 2.2        | 0.1        | 4.3        | 0.1        | 2.3        | 0.1        | 4.6         | 0.1        |
| Strip 1      | 2.3        | 0.1        | 6.2        | 0.2        | 2.7        | 0.1        | 6.6        | 0.2        | 2.3        | 0.1        | 7.1        | 0.1        | 3.1        | 0.2        | 11.4        | 0.8        |
| Strip 2      | 2.3        | 0.1        | 6.1        | 0.2        | 2.7        | 0.1        | 6.5        | 0.1        | 2.3        | 0.1        | 7.0        | 0.1        | 3.8        | 0.1        | 15.3        | 1.6        |
| Strip 3      | 2.3        | 0.1        | 6.1        | 0.2        | 2.5        | 0.1        | 6.3        | 0.1        | 2.4        | 0.1        | 7.4        | 0.2        | 4.1        | 0.2        | 20.6        | 0.6        |
| Avg          | <b>2.3</b> | <b>0.1</b> | <b>6.1</b> | <b>0.2</b> | <b>2.6</b> | <b>0.1</b> | <b>6.5</b> | <b>0.1</b> | <b>2.3</b> | <b>0.1</b> | <b>7.2</b> | <b>0.1</b> | <b>3.7</b> | <b>0.2</b> | <b>15.8</b> | <b>1.0</b> |
| <b>O-Pre</b> | 2.0        | 0.1        | 2.3        | 0.1        | 2.0        | 0.1        | 2.3        | 0.1        | 2.0        | 0.1        | 2.3        | 0.1        | 2.0        | 0.1        | 2.3         | 0.1        |
| Strip 1      | 2.1        | 0.1        | 3.1        | 0.1        | 2.3        | 0.1        | 3.3        | 0.1        | 2.0        | 0.1        | 3.4        | 0.2        | 2.8        | 0.2        | 9.8         | 0.2        |
| Strip 2      | 2.0        | 0.1        | 2.8        | 0.1        | 2.3        | 0.2        | 3.3        | 0.2        | 2.0        | 0.1        | 3.2        | 0.2        | 3.2        | 0.2        | 11.2        | 0.6        |
| Strip 3      | 2.0        | 0.1        | 3.2        | 0.1        | 2.2        | 0.1        | 3.2        | 0.1        | 2.0        | 0.1        | 3.5        | 0.1        | 2.9        | 0.2        | 10.4        | 0.6        |
| Avg          | <b>2.0</b> | <b>0.1</b> | <b>3.0</b> | <b>0.1</b> | <b>2.3</b> | <b>0.1</b> | <b>3.3</b> | <b>0.1</b> | <b>2.0</b> | <b>0.1</b> | <b>3.4</b> | <b>0.2</b> | <b>3.0</b> | <b>0.2</b> | <b>10.5</b> | <b>0.5</b> |
| <b>P-Pre</b> | 2.2        | 0.1        | 2.1        | 0.1        | 2.2        | 0.1        | 2.1        | 0.1        | 2.2        | 0.1        | 2.1        | 0.1        | 2.2        | 0.1        | 2.0         | 0.1        |
| Strip 1      | 2.4        | 0.1        | 2.5        | 0.1        | 2.5        | 0.1        | 2.6        | 0.1        | 2.3        | 0.2        | 2.7        | 0.1        | 2.8        | 0.1        | 6.2         | 0.4        |
| Strip 2      | 2.4        | 0.1        | 2.5        | 0.1        | 2.5        | 0.1        | 2.6        | 0.1        | 2.2        | 0.1        | 2.5        | 0.2        | 2.7        | 0.1        | 5.3         | 0.4        |
| Strip 3      | 2.3        | 0.1        | 2.5        | 0.1        | 2.4        | 0.1        | 2.4        | 0.1        | 2.2        | 0.1        | 2.6        | 0.1        | 2.6        | 0.1        | 4.8         | 0.4        |
| Avg          | <b>2.4</b> | <b>0.1</b> | <b>2.5</b> | <b>0.1</b> | <b>2.5</b> | <b>0.1</b> | <b>2.5</b> | <b>0.1</b> | <b>2.2</b> | <b>0.1</b> | <b>2.6</b> | <b>0.1</b> | <b>2.7</b> | <b>0.1</b> | <b>5.4</b>  | <b>0.4</b> |
| <b>Q-Pre</b> | 2.0        | 0.1        | 2.5        | 0.1        | 2.0        | 0.1        | 2.5        | 0.1        | 2.0        | 0.1        | 2.5        | 0.1        | 2.0        | 0.1        | 2.5         | 0.1        |
| Strip 1      | 2.2        | 0.1        | 3.2        | 0.1        | 2.4        | 0.1        | 3.6        | 0.1        | 2.1        | 0.1        | 3.6        | 0.1        | 2.8        | 0.2        | 8.8         | 0.2        |
| Strip 2      | 2.2        | 0.1        | 2.9        | 0.2        | 2.6        | 0.1        | 3.5        | 0.1        | 2.1        | 0.1        | 3.3        | 0.2        | 2.5        | 0.2        | 5.9         | 0.4        |
| Strip 3      | 2.1        | 0.1        | 2.9        | 0.2        | 2.5        | 0.1        | 3.4        | 0.1        | 2.0        | 0.1        | 3.2        | 0.2        | 2.6        | 0.1        | 6.6         | 0.4        |
| Avg          | <b>2.2</b> | <b>0.1</b> | <b>3.0</b> | <b>0.2</b> | <b>2.5</b> | <b>0.1</b> | <b>3.5</b> | <b>0.1</b> | <b>2.1</b> | <b>0.1</b> | <b>3.4</b> | <b>0.2</b> | <b>2.6</b> | <b>0.2</b> | <b>7.1</b>  | <b>0.3</b> |
| <b>R-Pre</b> | 2.8        | 0.1        | 1.2        | 0.1        | 2.8        | 0.1        | 1.2        | 0.1        | 2.8        | 0.1        | 1.2        | 0.1        | 2.8        | 0.1        | 1.2         | 0.1        |
| Strip 1      | 2.9        | 0.1        | 1.5        | 0.1        | 3.3        | 0.1        | 1.7        | 0.1        | 3.0        | 0.1        | 1.6        | 0.1        | 2.8        | 0.1        | 2.4         | 0.2        |
| Strip 2      | 3.0        | 0.1        | 1.5        | 0.1        | 3.3        | 0.1        | 1.7        | 0.1        | 2.9        | 0.1        | 1.5        | 0.1        | 2.8        | 0.1        | 2.7         | 0.2        |
| Strip 3      | 2.9        | 0.1        | 1.4        | 0.1        | 3.3        | 0.1        | 1.7        | 0.1        | 2.9        | 0.1        | 1.5        | 0.1        | 2.7        | 0.1        | 1.9         | 0.2        |
| Avg          | <b>2.9</b> | <b>0.1</b> | <b>1.5</b> | <b>0.1</b> | <b>3.3</b> | <b>0.1</b> | <b>1.7</b> | <b>0.1</b> | <b>2.9</b> | <b>0.1</b> | <b>1.5</b> | <b>0.1</b> | <b>2.8</b> | <b>0.1</b> | <b>2.3</b>  | <b>0.2</b> |
| <b>S-Pre</b> | 2.2        | 0.1        | 1.7        | 0.1        | 2.2        | 0.1        | 1.8        | 0.1        | 2.2        | 0.1        | 1.8        | 0.1        | 2.2        | 0.1        | 1.8         | 0.1        |
| Strip 1      | 2.3        | 0.1        | 2.6        | 0.2        | 2.4        | 0.1        | 2.7        | 0.2        | 2.3        | 0.1        | 2.8        | 0.1        | 2.3        | 0.1        | 3.4         | 0.2        |
| Strip 2      | 2.3        | 0.1        | 2.5        | 0.2        | 2.3        | 0.2        | 2.8        | 0.1        | 2.3        | 0.1        | 2.9        | 0.1        | 2.5        | 0.1        | 4.4         | 0.2        |
| Strip 3      | 2.3        | 0.1        | 2.5        | 0.1        | 2.3        | 0.2        | 2.8        | 0.2        | 2.2        | 0.1        | 3.0        | 0.1        | 2.5        | 0.1        | 4.8         | 0.2        |
| Avg          | <b>2.3</b> | <b>0.1</b> | <b>2.5</b> | <b>0.2</b> | <b>2.3</b> | <b>0.2</b> | <b>2.8</b> | <b>0.2</b> | <b>2.3</b> | <b>0.1</b> | <b>2.9</b> | <b>0.1</b> | <b>2.4</b> | <b>0.1</b> | <b>4.2</b>  | <b>0.2</b> |
| <b>T-Pre</b> | 1.9        | 0.1        | 1.2        | 0.1        | 1.9        | 0.1        | 1.2        | 0.1        | 1.9        | 0.1        | 1.2        | 0.1        | 1.9        | 0.1        | 1.2         | 0.1        |
| Strip 1      | 2.0        | 0.1        | 1.9        | 0.1        | 2.2        | 0.1        | 1.9        | 0.1        | 1.9        | 0.1        | 2.1        | 0.1        | 2.1        | 0.1        | 3.6         | 0.4        |
| Strip 2      | 2.0        | 0.1        | 1.9        | 0.1        | 2.0        | 0.1        | 1.8        | 0.1        | 1.9        | 0.1        | 1.9        | 0.1        | 2.1        | 0.1        | 3.1         | 0.2        |

|         |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |
|---------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Strip 3 | 2.0        | 0.1        | 1.9        | 0.1        | 2.1        | 0.1        | 1.8        | 0.1        | 1.9        | 0.1        | 1.9        | 0.1        | 2.1        | 0.1        | 3.2        | 0.1        |
| Avg     | <b>2.0</b> | <b>0.1</b> | <b>1.9</b> | <b>0.1</b> | <b>2.1</b> | <b>0.1</b> | <b>1.8</b> | <b>0.1</b> | <b>1.9</b> | <b>0.1</b> | <b>2.0</b> | <b>0.1</b> | <b>2.1</b> | <b>0.1</b> | <b>3.3</b> | <b>0.2</b> |

Touch – Up

|             | Gloss 85°  |            |            |            |            |            |            |            |            |            | Gloss - Visual Rating |           |           | AQMD      |
|-------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|-----------------------|-----------|-----------|-----------|
|             | A1         | A2         | B1         | B2         | C1         | C2         | D1         | D2         | E1         | E2         | C                     | D         | E         | Rating    |
| J           | 3.3        | 3.9        | 3.6        | 3.3        | 4.3        | 3.7        | 3.6        | 3.7        | 3.5        | 4.1        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 3.6        | 4.0        | 3.9        | 3.6        | 4.1        | 3.9        | 3.8        | 3.8        | 4.3        | 4.1        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 3.4        | 3.9        | 3.6        | 3.3        | 3.8        | 3.7        | 3.5        | 3.4        | 3.6        | 3.4        | 10                    | 10        | 10        | 10        |
| Average     | <b>3.4</b> | <b>3.9</b> | <b>3.7</b> | <b>3.4</b> | <b>4.1</b> | <b>3.8</b> | <b>3.6</b> | <b>3.6</b> | <b>3.8</b> | <b>3.9</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| K           | 1.5        | 1.6        | 1.7        | 1.7        | 2.0        | 1.9        | 1.7        | 1.8        | 1.8        | 2.0        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 1.7        | 1.9        | 1.7        | 1.6        | 2.1        | 2.0        | 1.9        | 1.9        | 2.5        | 2.0        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 1.7        | 1.9        | 1.8        | 1.7        | 1.8        | 1.9        | 1.8        | 1.8        | 2.2        | 1.9        | 10                    | 10        | 10        | 10        |
| Average     | <b>1.6</b> | <b>1.8</b> | <b>1.7</b> | <b>1.7</b> | <b>2.0</b> | <b>1.9</b> | <b>1.8</b> | <b>1.8</b> | <b>2.2</b> | <b>2.0</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| L           | 2.3        | 2.7        | 2.5        | 2.6        | 2.5        | 2.6        | 2.5        | 2.6        | 2.4        | 2.3        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 2.3        | 2.6        | 2.4        | 2.4        | 2.5        | 2.5        | 2.5        | 2.6        | 2.6        | 2.5        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 2.5        | 2.6        | 2.5        | 2.5        | 2.7        | 2.6        | 2.4        | 2.5        | 2.4        | 2.3        | 10                    | 10        | 10        | 10        |
| Average     | <b>2.4</b> | <b>2.6</b> | <b>2.5</b> | <b>2.5</b> | <b>2.6</b> | <b>2.6</b> | <b>2.5</b> | <b>2.6</b> | <b>2.5</b> | <b>2.4</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| M           | 0.8        | 1.2        | 1.3        | 0.9        | 1.2        | 0.9        | 1.1        | 1.2        | 1.2        | 1.2        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 0.9        | 1.0        | 1.2        | 0.9        | 1.3        | 0.9        | 1.2        | 1.2        | 1.3        | 1.1        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 0.9        | 1.2        | 1.3        | 0.9        | 1.3        | 0.9        | 1.2        | 1.2        | 1.1        | 1.1        | 10                    | 10        | 10        | 10        |
| Average     | <b>0.9</b> | <b>1.1</b> | <b>1.3</b> | <b>0.9</b> | <b>1.3</b> | <b>0.9</b> | <b>1.2</b> | <b>1.2</b> | <b>1.2</b> | <b>1.1</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| N           | 2.8        | 3.5        | 3.1        | 3.0        | 3.9        | 3.3        | 3.6        | 3.4        | 4.1        | 4.1        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 2.9        | 2.7        | 3.6        | 3.2        | 4.2        | 3.4        | 3.1        | 3.1        | 2.7        | 3.7        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 2.7        | 3.5        | 3.4        | 3.1        | 3.9        | 3.3        | 3.7        | 3.6        | 3.7        | 4.0        | 10                    | 10        | 10        | 10        |
| Average     | <b>2.8</b> | <b>3.2</b> | <b>3.4</b> | <b>3.1</b> | <b>4.0</b> | <b>3.3</b> | <b>3.5</b> | <b>3.4</b> | <b>3.5</b> | <b>3.9</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| O           | 1.8        | 2.1        | 2.0        | 1.8        | 2.1        | 1.9        | 1.9        | 1.9        | 1.9        | 1.8        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 1.7        | 2.2        | 1.9        | 1.8        | 2.2        | 1.9        | 2.1        | 1.9        | 2.0        | 2.0        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 1.6        | 2.1        | 2.0        | 1.7        | 2.1        | 1.7        | 2.0        | 2.1        | 2.0        | 1.9        | 10                    | 10        | 10        | 10        |
| Average     | <b>1.7</b> | <b>2.1</b> | <b>2.0</b> | <b>1.8</b> | <b>2.1</b> | <b>1.8</b> | <b>2.0</b> | <b>2.0</b> | <b>2.0</b> | <b>1.9</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| P           | 1.6        | 2.0        | 2.1        | 1.8        | 2.3        | 1.8        | 2.0        | 2.0        | 1.9        | 1.8        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 1.7        | 2.0        | 2.0        | 1.8        | 2.3        | 1.6        | 2.1        | 2.2        | 2.2        | 2.0        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 1.6        | 2.0        | 2.1        | 1.7        | 2.0        | 1.8        | 2.1        | 2.1        | 1.7        | 1.8        | 10                    | 10        | 10        | 10        |
| Average     | <b>1.6</b> | <b>2.0</b> | <b>2.1</b> | <b>1.8</b> | <b>2.2</b> | <b>1.7</b> | <b>2.1</b> | <b>2.1</b> | <b>1.9</b> | <b>1.9</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| Q           | 2.0        | 2.1        | 2.0        | 2.0        | 2.1        | 2.0        | 1.9        | 2.0        | 2.2        | 1.8        | 10                    | 10        | 10        | 10        |
| Replicate 2 | 1.8        | 2.3        | 2.2        | 1.9        | 2.5        | 1.9        | 2.2        | 2.2        | 1.9        | 1.8        | 10                    | 10        | 10        | 10        |
| Replicate 3 | 1.8        | 2.3        | 2.2        | 1.8        | 2.4        | 1.9        | 2.2        | 2.2        | 2.6        | 2.2        | 10                    | 10        | 10        | 10        |
| Average     | <b>1.9</b> | <b>2.2</b> | <b>2.1</b> | <b>1.9</b> | <b>2.3</b> | <b>1.9</b> | <b>2.1</b> | <b>2.1</b> | <b>2.2</b> | <b>1.9</b> | <b>10</b>             | <b>10</b> | <b>10</b> | <b>10</b> |
| R           | 1.1        | 1.3        | 1.2        | 1.1        | 1.6        | 1.1        | 1.2        | 1.1        | 0.8        | 0.9        | 10                    | 10        | 10        | 10        |

|             |            |            |            |            |            |            |            |            |            |            |           |           |           |           |
|-------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|-----------|-----------|-----------|-----------|
| Replicate 2 | 1.1        | 1.3        | 1.2        | 1.1        | 1.5        | 1.4        | 1.1        | 1.1        | 0.9        | 0.9        | 10        | 10        | 10        | 10        |
| Replicate 3 | 1.1        | 1.2        | 1.1        | 1.2        | 1.1        | 1.2        | 1.1        | 1.1        | 1.0        | 0.9        | 10        | 10        | 10        | 10        |
| Average     | <b>1.1</b> | <b>1.3</b> | <b>1.2</b> | <b>1.1</b> | <b>1.4</b> | <b>1.2</b> | <b>1.1</b> | <b>1.1</b> | <b>0.9</b> | <b>0.9</b> | <b>10</b> | <b>10</b> | <b>10</b> | <b>10</b> |
| S           | 1.2        | 1.4        | 1.5        | 1.2        | 1.2        | 1.1        | 1.5        | 1.5        | 1.6        | 1.4        | 10        | 10        | 10        | 10        |
| Replicate 2 | 1.2        | 1.7        | 1.7        | 1.2        | 1.5        | 1.2        | 1.7        | 1.7        | 1.5        | 1.6        | 10        | 10        | 10        | 10        |
| Replicate 3 | 1.2        | 1.7        | 1.5        | 1.2        | 1.4        | 1.1        | 1.5        | 1.5        | 1.5        | 1.6        | 10        | 10        | 10        | 10        |
| Average     | <b>1.2</b> | <b>1.6</b> | <b>1.6</b> | <b>1.2</b> | <b>1.4</b> | <b>1.1</b> | <b>1.6</b> | <b>1.6</b> | <b>1.5</b> | <b>1.5</b> | <b>10</b> | <b>10</b> | <b>10</b> | <b>10</b> |
| T           | 1.0        | 1.3        | 1.2        | 0.9        | 1.2        | 1.0        | 1.0        | 1.2        | 1.0        | 1.5        | 10        | 10        | 10        | 10        |
| Replicate 2 | 0.9        | 1.3        | 1.2        | 1.0        | 1.3        | 1.0        | 1.1        | 1.2        | 1.0        | 1.0        | 10        | 10        | 10        | 10        |
| Replicate 3 | 0.9        | 1.3        | 1.3        | 1.0        | 1.4        | 1.1        | 1.1        | 1.2        | 1.2        | 1.0        | 10        | 10        | 10        | 10        |
| Average     | <b>0.9</b> | <b>1.3</b> | <b>1.2</b> | <b>1.0</b> | <b>1.3</b> | <b>1.0</b> | <b>1.1</b> | <b>1.2</b> | <b>1.1</b> | <b>1.2</b> | <b>10</b> | <b>10</b> | <b>10</b> | <b>10</b> |

## Tests for Exterior Flat Paints

### Adhesion – Glass

|                    | Cross-Hatch Adhesion - Glass |           |                   | AQMD     |
|--------------------|------------------------------|-----------|-------------------|----------|
|                    | Rating                       | Failure % | Failure Mechanism | Rating   |
| A                  | 4B                           | 4         | Adhesion          | 4        |
| Replicate 2        | 3B                           | 10        | Adhesion          | 3        |
| Replicate 3        | 3B                           | 15        | Adhesion          | 3        |
| <b>Average</b>     | <b>3B</b>                    | <b>10</b> | <b>Adhesion</b>   | <b>3</b> |
| B                  | 5B                           | 0         | -----             | 5        |
| Replicate 2        | 4B                           | 2         | Adhesion          | 4        |
| Replicate 3        | 4B                           | 3         | Adhesion          | 4        |
| <b>Average</b>     | <b>4B</b>                    | <b>2</b>  | <b>Adhesion</b>   | <b>4</b> |
| C                  | 2B                           | 15        | Adhesion          | 2        |
| Replicate 2        | 2B                           | 20        | Adhesion          | 2        |
| Replicate 3        | 3B                           | 25        | Adhesion          | 3        |
| <b>Average</b>     | <b>2B</b>                    | <b>20</b> | <b>Adhesion</b>   | <b>2</b> |
| D                  | 4B                           | 3         | Adhesion          | 4        |
| Replicate 2        | 3B                           | 5         | Adhesion          | 3        |
| Replicate 3        | 4B                           | 4         | Adhesion          | 4        |
| <b>Average</b>     | <b>4B</b>                    | <b>4</b>  | <b>Adhesion</b>   | <b>4</b> |
| <i>E</i>           | <i>4B</i>                    | <i>1</i>  | <i>Adhesion</i>   | <i>4</i> |
| <i>Replicate 2</i> | <i>5B</i>                    | <i>0</i>  | <i>-----</i>      | <i>5</i> |
| <i>Replicate 3</i> | <i>5B</i>                    | <i>0</i>  | <i>-----</i>      | <i>5</i> |
| <b>Average</b>     | <b>5B</b>                    | <b>0</b>  | <b>Adhesion</b>   | <b>5</b> |
| F                  | 2B                           | 20        | Adhesion          | 2        |

|                |           |           |                 |          |
|----------------|-----------|-----------|-----------------|----------|
| Replicate 2    | 2B        | 15        | Adhesion        | 2        |
| Replicate 3    | 2B        | 20        | Adhesion        | 2        |
| <b>Average</b> | <b>2B</b> | <b>18</b> | <b>Adhesion</b> | <b>2</b> |
| G              | 2B        | 20        | Adhesion        | 2        |
| Replicate 2    | 3B        | 10        | Adhesion        | 3        |
| Replicate 3    | 2B        | 20        | Adhesion        | 2        |
| <b>Average</b> | <b>2B</b> | <b>17</b> | <b>Adhesion</b> | <b>2</b> |
| H              | 4B        | 2         | Adhesion        | 4        |
| Replicate 2    | 4B        | 4         | Adhesion        | 4        |
| Replicate 3    | 4B        | 3         | Adhesion        | 4        |
| <b>Average</b> | <b>4B</b> | <b>3</b>  | <b>Adhesion</b> | <b>4</b> |
| I              | 4B        | 1         | Adhesion        | 4        |
| Replicate 2    | 4B        | 1         | Adhesion        | 4        |
| Replicate 3    | 4B        | 1         | Adhesion        | 4        |
| <b>Average</b> | <b>4B</b> | <b>1</b>  | <b>Adhesion</b> | <b>4</b> |
| S              | 2B        | 20        | Adhesion        | 2        |
| Replicate 2    | 2B        | 20        | Adhesion        | 2        |
| Replicate 3    | 2B        | 20        | Adhesion        | 2        |
| <b>Average</b> | <b>2B</b> | <b>20</b> | <b>Adhesion</b> | <b>2</b> |
| T              | 3B        | 5         | Adhesion        | 3        |
| Replicate 2    | 3B        | 5         | Adhesion        | 3        |
| Replicate 3    | 3B        | 10        | Adhesion        | 3        |
| <b>Average</b> | <b>3B</b> | <b>7</b>  | <b>Adhesion</b> | <b>3</b> |

Tannin Stain Resistance

|                   | Cedar-Initial |              |              | Cedar        |              |              |             | Visual Ranking | Leneta-Initial |              |              | Cedar        |             |       |            |
|-------------------|---------------|--------------|--------------|--------------|--------------|--------------|-------------|----------------|----------------|--------------|--------------|--------------|-------------|-------|------------|
|                   | X             | Y            | Z            | X            | Y            | Z            | $\Delta E$  |                | X              | Y            | Z            | X            | Y           | Z     | $\Delta E$ |
| Positive Standard | 71.02         | 75.18        | 75.48        | 71.75        | 75.95        | 74.81        | 1.20        | 5              | 79.25          | 83.76        | 86.81        | 73.96        | 78.20       | 78.71 | 3.01       |
| Replicate 2       | 70.18         | 74.37        | 74.50        | 71.65        | 75.89        | 74.53        | 1.40        |                | 71.46          | 75.62        | 74.82        | 4.55         |             |       |            |
| Replicate 3       | 69.36         | 73.36        | 73.17        | 69.33        | 73.29        | 71.61        | 1.21        |                | 68.80          | 72.63        | 72.30        | 5.56         |             |       |            |
| Replicate 4       | 71.20         | 75.26        | 75.13        | 71.82        | 75.94        | 74.75        | 0.89        |                | 71.95          | 76.00        | 76.03        | 4.04         |             |       |            |
| Replicate 5       | 71.22         | 75.30        | 75.84        | 72.36        | 76.56        | 75.67        | 1.29        |                | 73.02          | 77.16        | 77.43        | 3.50         |             |       |            |
| Replicate 6       | 67.86         | 71.61        | 71.31        | 70.01        | 74.02        | 72.35        | 1.65        |                | 68.76          | 72.52        | 70.75        | 6.19         |             |       |            |
| <b>Average</b>    | <b>70.14</b>  | <b>74.18</b> | <b>74.24</b> | <b>71.15</b> | <b>75.28</b> | <b>73.95</b> | <b>1.27</b> |                | <b>5</b>       | <b>71.33</b> | <b>75.36</b> | <b>75.01</b> | <b>4.48</b> |       |            |
| Negative Standard | 69.67         | 73.29        | 68.49        | 70.37        | 73.98        | 68.73        | 0.49        | 1              | 74.44          | 78.07        | 72.60        | 68.29        | 71.89       | 66.66 | 2.96       |
| Replicate 2       | 69.27         | 72.88        | 68.08        | 70.13        | 73.74        | 68.50        | 0.56        |                | 67.71          | 71.27        | 66.15        | 3.25         |             |       |            |
| Replicate 3       | 67.82         | 71.35        | 66.62        | 69.25        | 72.81        | 67.71        | 0.76        |                | 66.84          | 70.33        | 65.77        | 3.74         |             |       |            |
| Replicate 4       | 68.72         | 72.20        | 67.03        | 70.27        | 73.78        | 68.29        | 0.79        |                | 68.91          | 72.41        | 67.36        | 2.68         |             |       |            |
| Replicate 5       | 70.17         | 73.75        | 68.65        | 71.20        | 74.76        | 69.18        | 0.63        |                | 70.40          | 73.99        | 68.27        | 1.95         |             |       |            |

|             |              |              |              |              |              |              |             |           |       |       |       |              |              |              |             |
|-------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|-----------|-------|-------|-------|--------------|--------------|--------------|-------------|
| Replicate 6 | 70.16        | 73.74        | 68.54        | 71.68        | 75.28        | 69.71        | 0.78        |           |       |       |       | 70.20        | 73.77        | 68.40        | 2.03        |
| Average     | <b>69.30</b> | <b>72.87</b> | <b>67.90</b> | <b>70.48</b> | <b>74.06</b> | <b>68.69</b> | <b>0.67</b> | <b>1</b>  |       |       |       | <b>68.73</b> | <b>72.28</b> | <b>67.10</b> | <b>2.77</b> |
| A           | 74.23        | 78.49        | 79.49        | 75.51        | 79.77        | 79.83        | 0.95        | 10        | 84.64 | 89.57 | 91.98 | 75.53        | 79.77        | 80.07        | 4.44        |
| Replicate 2 | 73.43        | 77.72        | 77.81        | 75.88        | 80.26        | 79.61        | 1.30        | 9         |       |       |       | 75.77        | 80.13        | 79.58        | 4.51        |
| Replicate 3 | 73.50        | 77.60        | 78.70        | 75.86        | 80.08        | 80.46        | 1.27        | 9         |       |       |       | 76.04        | 80.27        | 80.75        | 4.19        |
| Average     | <b>73.72</b> | <b>77.94</b> | <b>78.67</b> | <b>75.75</b> | <b>80.04</b> | <b>79.97</b> | <b>1.17</b> | <b>9</b>  |       |       |       | <b>75.78</b> | <b>80.06</b> | <b>80.13</b> | <b>4.38</b> |
| B           | 77.04        | 81.62        | 79.76        | 77.62        | 82.03        | 79.28        | 0.80        | 3         | 85.52 | 90.55 | 93.66 | 77.62        | 82.01        | 79.36        | 5.42        |
| Replicate 2 | 76.64        | 81.05        | 79.24        | 78.69        | 83.10        | 80.93        | 0.97        | 3         |       |       |       | 78.57        | 82.98        | 80.91        | 4.81        |
| Replicate 3 | 78.80        | 83.46        | 81.79        | 79.55        | 84.06        | 81.85        | 0.61        | 3         |       |       |       | 79.42        | 83.92        | 81.80        | 4.57        |
| Average     | <b>77.49</b> | <b>82.04</b> | <b>80.26</b> | <b>78.62</b> | <b>83.06</b> | <b>80.69</b> | <b>0.79</b> | <b>3</b>  |       |       |       | <b>78.54</b> | <b>82.97</b> | <b>80.69</b> | <b>4.93</b> |
| C           | 74.54        | 79.13        | 78.79        | 75.98        | 80.50        | 79.53        | 0.85        | 4         | 84.89 | 89.87 | 92.20 | 76.20        | 80.71        | 79.71        | 4.52        |
| Replicate 2 | 74.02        | 78.52        | 77.60        | 75.80        | 80.29        | 78.92        | 0.90        | 4         |       |       |       | 75.85        | 80.33        | 78.79        | 4.87        |
| Replicate 3 | 76.25        | 80.90        | 80.58        | 78.14        | 82.80        | 82.19        | 0.90        | 4         |       |       |       | 78.62        | 83.30        | 82.61        | 3.45        |
| Average     | <b>74.94</b> | <b>79.52</b> | <b>78.99</b> | <b>76.64</b> | <b>81.20</b> | <b>80.21</b> | <b>0.88</b> | <b>4</b>  |       |       |       | <b>76.89</b> | <b>81.45</b> | <b>80.37</b> | <b>4.28</b> |
| D           | 77.16        | 81.69        | 79.22        | 77.46        | 81.78        | 78.65        | 0.67        | 2         | 84.76 | 89.70 | 92.14 | 77.56        | 81.87        | 78.78        | 5.15        |
| Replicate 2 | 76.49        | 80.86        | 78.75        | 78.16        | 82.53        | 80.32        | 0.76        | 2         |       |       |       | 77.43        | 81.71        | 79.21        | 4.87        |
| Replicate 3 | 77.28        | 81.79        | 79.95        | 79.03        | 83.44        | 80.87        | 1.00        | 2         |       |       |       | 79.06        | 83.47        | 81.01        | 4.33        |
| Average     | <b>76.98</b> | <b>81.45</b> | <b>79.31</b> | <b>78.22</b> | <b>82.58</b> | <b>79.95</b> | <b>0.81</b> | <b>2</b>  |       |       |       | <b>78.02</b> | <b>82.35</b> | <b>79.67</b> | <b>4.78</b> |
| E           | 75.04        | 79.50        | 81.97        | 76.24        | 80.72        | 82.32        | 0.88        | 12        | 78.79 | 83.56 | 86.26 | 76.26        | 80.73        | 82.29        | 1.48        |
| Replicate 2 | 74.11        | 78.49        | 80.35        | 75.74        | 80.20        | 81.38        | 0.94        | 12        |       |       |       | 75.26        | 79.68        | 80.91        | 1.99        |
| Replicate 3 | 75.25        | 79.69        | 82.19        | 76.87        | 81.39        | 83.26        | 0.92        | 12        |       |       |       | 76.91        | 81.41        | 83.20        | 1.16        |
| Average     | <b>74.80</b> | <b>79.23</b> | <b>81.50</b> | <b>76.28</b> | <b>80.77</b> | <b>82.32</b> | <b>0.91</b> | <b>12</b> |       |       |       | <b>76.14</b> | <b>80.61</b> | <b>82.13</b> | <b>1.54</b> |
| F           | 74.22        | 78.63        | 80.73        | 75.34        | 79.72        | 80.75        | 0.99        | 13        | 78.76 | 83.50 | 85.76 | 75.22        | 79.59        | 80.67        | 1.92        |
| Replicate 2 | 73.84        | 78.12        | 79.53        | 75.66        | 80.00        | 80.90        | 0.96        | 13        |       |       |       | 75.58        | 79.90        | 80.90        | 1.85        |
| Replicate 3 | 74.83        | 79.25        | 81.43        | 76.48        | 80.93        | 82.23        | 1.04        | 13        |       |       |       | 76.49        | 80.93        | 82.27        | 1.32        |
| Average     | <b>74.30</b> | <b>78.67</b> | <b>80.56</b> | <b>75.83</b> | <b>80.22</b> | <b>81.29</b> | <b>1.00</b> | <b>13</b> |       |       |       | <b>75.76</b> | <b>80.14</b> | <b>81.28</b> | <b>1.70</b> |
| G           | 74.54        | 78.86        | 79.20        | 76.05        | 80.42        | 80.08        | 0.90        | 9         | 83.51 | 88.37 | 90.15 | 75.64        | 80.00        | 79.82        | 3.84        |
| Replicate 2 | 74.18        | 78.52        | 77.72        | 76.25        | 80.67        | 79.29        | 1.08        | 8         |       |       |       | 76.36        | 80.78        | 79.38        | 3.94        |
| Replicate 3 | 75.66        | 80.01        | 80.43        | 77.39        | 81.83        | 81.56        | 0.97        | 7         |       |       |       | 77.03        | 81.42        | 81.12        | 3.30        |
| Average     | <b>74.79</b> | <b>79.13</b> | <b>79.12</b> | <b>76.56</b> | <b>80.97</b> | <b>80.31</b> | <b>0.98</b> | <b>8</b>  |       |       |       | <b>76.34</b> | <b>80.73</b> | <b>80.11</b> | <b>3.69</b> |
| H           | 78.45        | 83.04        | 83.46        | 79.64        | 84.19        | 83.97        | 0.73        | 8         | 85.37 | 90.34 | 92.72 | 79.83        | 84.39        | 84.20        | 3.04        |
| Replicate 2 | 75.21        | 79.43        | 79.77        | 77.20        | 81.49        | 81.56        | 0.95        | 11        |       |       |       | 77.57        | 81.88        | 82.08        | 3.88        |
| Replicate 3 | 78.85        | 83.39        | 83.82        | 80.82        | 85.44        | 85.67        | 0.90        | 10        |       |       |       | 81.07        | 85.67        | 85.65        | 2.53        |
| Average     | <b>77.50</b> | <b>81.95</b> | <b>82.35</b> | <b>79.22</b> | <b>83.71</b> | <b>83.73</b> | <b>0.86</b> | <b>10</b> |       |       |       | <b>79.49</b> | <b>83.98</b> | <b>83.98</b> | <b>3.15</b> |
| I           | 72.26        | 76.46        | 77.98        | 74.47        | 78.75        | 79.20        | 1.37        | 11        | 84.12 | 89.07 | 91.61 | 74.19        | 78.45        | 79.00        | 4.77        |
| Replicate 2 | 73.97        | 78.27        | 77.88        | 76.42        | 80.82        | 79.67        | 1.30        | 10        |       |       |       | 76.14        | 80.50        | 79.44        | 4.43        |
| Replicate 3 | 75.07        | 79.42        | 80.73        | 77.20        | 81.65        | 81.76        | 1.37        | 11        |       |       |       | 77.25        | 81.70        | 81.97        | 3.48        |
| Average     | <b>73.77</b> | <b>78.05</b> | <b>78.86</b> | <b>76.03</b> | <b>80.41</b> | <b>80.21</b> | <b>1.35</b> | <b>11</b> |       |       |       | <b>75.86</b> | <b>80.22</b> | <b>80.14</b> | <b>4.23</b> |
| S           | 75.52        | 80.01        | 80.44        | 76.46        | 80.90        | 80.65        | 0.69        | 6         | 85.32 | 90.38 | 92.75 | 76.85        | 81.32        | 81.13        | 4.21        |
| Replicate 2 | 73.83        | 78.21        | 78.55        | 76.75        | 81.27        | 80.89        | 1.51        | 6         |       |       |       | 75.90        | 80.34        | 80.02        | 4.64        |

|             |              |              |              |              |              |              |             |          |       |       |       |              |              |              |             |
|-------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|----------|-------|-------|-------|--------------|--------------|--------------|-------------|
| Replicate 3 | 76.64        | 81.12        | 81.54        | 78.39        | 82.89        | 82.43        | 1.05        | 8        |       |       |       | 78.46        | 82.96        | 82.67        | 3.61        |
| Average     | <b>75.33</b> | <b>79.78</b> | <b>80.18</b> | <b>77.20</b> | <b>81.69</b> | <b>81.32</b> | <b>1.08</b> | <b>7</b> |       |       |       | <b>77.07</b> | <b>81.54</b> | <b>81.27</b> | <b>4.15</b> |
| T           | 74.20        | 78.64        | 80.47        | 75.65        | 80.04        | 80.54        | 1.25        | 7        | 85.59 | 90.67 | 93.85 | 75.84        | 80.24        | 80.63        | 4.80        |
| Replicate 2 | 73.27        | 77.64        | 78.79        | 74.44        | 78.75        | 78.72        | 1.09        | 7        |       |       |       | 73.84        | 78.10        | 78.05        | 5.81        |
| Replicate 3 | 76.29        | 80.78        | 82.73        | 77.51        | 81.97        | 82.30        | 1.35        | 6        |       |       |       | 77.39        | 81.82        | 82.04        | 4.23        |
| Average     | <b>74.59</b> | <b>79.02</b> | <b>80.66</b> | <b>75.87</b> | <b>80.25</b> | <b>80.52</b> | <b>1.23</b> | <b>7</b> |       |       |       | <b>75.69</b> | <b>80.05</b> | <b>80.24</b> | <b>4.95</b> |

### Alkalinity

|                | 0 Days       |              |              | Day 1        |              |              |             | Day 2        |              |              |             | Day 3        |              |              |             |
|----------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|-------------|
|                | X            | Y            | Z            | X            | Y            | Z            | $\Delta E$  | X            | Y            | Z            | $\Delta E$  | X            | Y            | Z            | $\Delta E$  |
| A              | 66.12        | 60.60        | 48.17        | 66.37        | 61.10        | 48.23        | 0.78        | 66.57        | 61.56        | 48.18        | 1.62        | 67.13        | 62.85        | 48.28        | 3.74        |
| Replicate 2    | 65.60        | 60.03        | 47.44        | 65.83        | 60.92        | 47.36        | 1.90        | 65.98        | 61.41        | 47.12        | 2.96        | 66.91        | 63.32        | 47.67        | 5.70        |
| Replicate 3    | 65.87        | 60.40        | 47.93        | 65.80        | 60.83        | 47.97        | 1.25        | 66.07        | 61.35        | 47.78        | 2.11        | 66.28        | 61.94        | 47.92        | 3.12        |
| <b>Average</b> | <b>65.86</b> | <b>60.34</b> | <b>47.85</b> | <b>66.00</b> | <b>60.95</b> | <b>47.85</b> | <b>1.31</b> | <b>66.21</b> | <b>61.44</b> | <b>47.69</b> | <b>2.23</b> | <b>66.77</b> | <b>62.70</b> | <b>47.96</b> | <b>4.19</b> |
| B              | 68.24        | 62.88        | 51.24        | 68.09        | 63.10        | 51.25        | 0.86        | 67.69        | 62.72        | 50.56        | 1.01        | 67.88        | 63.14        | 50.99        | 1.48        |
| Replicate 2    | 68.37        | 62.92        | 51.16        | 67.99        | 63.00        | 50.98        | 1.05        | 67.91        | 63.05        | 50.70        | 1.43        | 68.18        | 63.55        | 51.11        | 1.97        |
| Replicate 3    | 68.24        | 62.92        | 51.33        | 68.14        | 63.23        | 51.40        | 0.95        | 67.57        | 62.80        | 50.63        | 1.32        | 68.12        | 63.56        | 51.23        | 1.86        |
| <b>Average</b> | <b>68.28</b> | <b>62.91</b> | <b>51.24</b> | <b>68.07</b> | <b>63.11</b> | <b>51.21</b> | <b>0.95</b> | <b>67.72</b> | <b>62.86</b> | <b>50.63</b> | <b>1.25</b> | <b>68.06</b> | <b>63.42</b> | <b>51.11</b> | <b>1.77</b> |
| C              | 66.65        | 62.07        | 50.35        | 66.30        | 62.36        | 50.48        | 1.45        | 66.30        | 63.97        | 50.00        | 5.58        | 67.39        | 66.68        | 50.92        | 9.65        |
| Replicate 2    | 68.14        | 63.03        | 50.87        | 67.73        | 62.88        | 50.71        | 0.58        | 67.75        | 63.71        | 50.60        | 2.58        | 67.06        | 63.37        | 50.32        | 3.29        |
| Replicate 3    | 68.10        | 63.05        | 50.89        | 67.70        | 63.05        | 50.84        | 0.89        | 67.17        | 62.75        | 50.18        | 1.45        | 67.27        | 63.28        | 50.35        | 2.47        |
| <b>Average</b> | <b>67.63</b> | <b>62.72</b> | <b>50.70</b> | <b>67.24</b> | <b>62.76</b> | <b>50.68</b> | <b>0.97</b> | <b>67.07</b> | <b>63.48</b> | <b>50.26</b> | <b>3.20</b> | <b>67.24</b> | <b>64.44</b> | <b>50.53</b> | <b>5.14</b> |
| D              | 68.07        | 62.53        | 51.09        | 67.50        | 62.15        | 50.75        | 0.44        | 66.81        | 61.59        | 50.13        | 0.81        | 67.07        | 61.88        | 50.48        | 0.79        |
| Replicate 2    | 67.71        | 62.16        | 50.75        | 67.46        | 62.26        | 50.65        | 0.81        | 67.18        | 62.14        | 50.19        | 1.25        | 67.34        | 62.44        | 50.47        | 1.57        |
| Replicate 3    | 67.62        | 62.19        | 50.94        | 67.42        | 62.29        | 50.87        | 0.72        | 67.25        | 62.24        | 50.54        | 1.05        | 67.29        | 62.56        | 50.55        | 1.76        |
| <b>Average</b> | <b>67.80</b> | <b>62.29</b> | <b>50.93</b> | <b>67.46</b> | <b>62.23</b> | <b>50.76</b> | <b>0.66</b> | <b>67.08</b> | <b>61.99</b> | <b>50.29</b> | <b>1.04</b> | <b>67.23</b> | <b>62.29</b> | <b>50.50</b> | <b>1.37</b> |
| E              | 67.77        | 64.87        | 56.77        | 67.61        | 65.11        | 56.62        | 0.96        | 67.63        | 66.09        | 55.89        | 3.62        | 69.32        | 69.69        | 57.13        | 8.43        |
| Replicate 2    | 67.24        | 64.38        | 56.24        | 67.46        | 65.06        | 56.47        | 1.11        | 67.34        | 65.68        | 55.78        | 3.20        | 67.78        | 66.85        | 56.13        | 5.00        |
| Replicate 3    | 67.80        | 64.90        | 56.78        | 67.76        | 65.29        | 56.78        | 1.02        | 67.68        | 66.04        | 56.07        | 3.29        | 68.25        | 67.53        | 56.30        | 5.66        |
| <b>Average</b> | <b>67.60</b> | <b>64.72</b> | <b>56.60</b> | <b>67.61</b> | <b>65.15</b> | <b>56.62</b> | <b>1.03</b> | <b>67.55</b> | <b>65.94</b> | <b>55.91</b> | <b>3.37</b> | <b>68.45</b> | <b>68.02</b> | <b>56.52</b> | <b>6.36</b> |
| F              | 65.55        | 62.07        | 53.52        | 66.88        | 64.35        | 54.20        | 2.85        | 66.98        | 65.42        | 53.67        | 5.47        | 68.51        | 68.48        | 54.87        | 9.38        |
| Replicate 2    | 66.22        | 62.65        | 53.98        | 66.64        | 63.89        | 54.16        | 2.17        | 66.82        | 64.76        | 53.77        | 4.14        | 67.72        | 66.71        | 54.53        | 6.82        |
| Replicate 3    | 66.35        | 62.73        | 53.98        | 66.54        | 63.44        | 54.14        | 1.32        | 66.74        | 64.16        | 53.93        | 2.81        | 68.63        | 68.55        | 54.89        | 9.37        |
| <b>Average</b> | <b>66.04</b> | <b>62.48</b> | <b>53.83</b> | <b>66.69</b> | <b>63.89</b> | <b>54.17</b> | <b>2.11</b> | <b>66.85</b> | <b>64.78</b> | <b>53.79</b> | <b>4.14</b> | <b>68.29</b> | <b>67.91</b> | <b>54.76</b> | <b>8.52</b> |
| G              | 64.07        | 57.65        | 43.28        | 63.94        | 57.78        | 43.36        | 0.62        | 63.35        | 57.38        | 42.94        | 1.03        | 63.37        | 57.47        | 43.03        | 1.18        |
| Replicate 2    | 64.65        | 58.07        | 43.56        | 64.71        | 59.08        | 43.69        | 2.50        | 65.12        | 60.42        | 43.60        | 5.16        | 66.63        | 63.79        | 44.38        | 10.31       |
| Replicate 3    | 64.12        | 57.70        | 43.36        | 64.99        | 59.88        | 43.78        | 3.80        | 65.28        | 61.06        | 43.59        | 6.34        | 66.22        | 62.95        | 43.98        | 9.09        |
| <b>Average</b> | <b>64.28</b> | <b>57.81</b> | <b>43.40</b> | <b>64.55</b> | <b>58.91</b> | <b>43.61</b> | <b>2.31</b> | <b>64.58</b> | <b>59.62</b> | <b>43.38</b> | <b>4.18</b> | <b>65.41</b> | <b>61.40</b> | <b>43.80</b> | <b>6.86</b> |
| H              | 67.64        | 62.58        | 50.52        | 67.42        | 62.90        | 50.64        | 1.23        | 67.44        | 63.20        | 50.36        | 2.02        | 67.75        | 64.12        | 50.45        | 3.65        |

|                |              |              |              |              |              |              |             |              |              |              |             |              |              |              |              |
|----------------|--------------|--------------|--------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|--------------|
| Replicate 2    | 68.29        | 63.08        | 50.84        | 68.01        | 63.14        | 50.80        | 0.74        | 67.71        | 63.16        | 50.36        | 1.57        | 68.10        | 64.00        | 50.52        | 2.79         |
| Replicate 3    | 68.07        | 63.00        | 50.96        | 67.95        | 63.49        | 50.94        | 1.46        | 67.80        | 63.56        | 50.50        | 2.10        | 68.45        | 65.02        | 50.82        | 4.32         |
| <b>Average</b> | <b>68.00</b> | <b>62.89</b> | <b>50.77</b> | <b>67.79</b> | <b>63.18</b> | <b>50.79</b> | <b>1.14</b> | <b>67.65</b> | <b>63.31</b> | <b>50.41</b> | <b>1.90</b> | <b>68.10</b> | <b>64.38</b> | <b>50.60</b> | <b>3.59</b>  |
| I              | 66.18        | 60.62        | 46.23        | 66.15        | 61.06        | 46.35        | 1.15        | 66.26        | 61.84        | 46.15        | 2.97        | 67.25        | 63.63        | 46.69        | 5.30         |
| Replicate 2    | 66.30        | 60.79        | 46.46        | 66.05        | 61.02        | 46.46        | 1.12        | 66.26        | 61.77        | 46.38        | 2.61        | 67.14        | 63.59        | 46.74        | 5.28         |
| Replicate 3    | 66.17        | 60.71        | 46.44        | 66.33        | 61.55        | 46.56        | 1.79        | 66.74        | 62.67        | 46.53        | 3.80        | 67.77        | 64.76        | 46.85        | 6.87         |
| <b>Average</b> | <b>66.22</b> | <b>60.71</b> | <b>46.38</b> | <b>66.18</b> | <b>61.21</b> | <b>46.46</b> | <b>1.35</b> | <b>66.42</b> | <b>62.09</b> | <b>46.35</b> | <b>3.13</b> | <b>67.39</b> | <b>63.99</b> | <b>46.76</b> | <b>5.82</b>  |
| S              | 67.73        | 62.39        | 50.33        | 67.52        | 62.51        | 50.55        | 0.76        | 68.13        | 64.30        | 50.37        | 3.96        | 71.04        | 70.29        | 52.10        | 12.07        |
| Replicate 2    | 67.08        | 61.82        | 49.81        | 67.01        | 62.04        | 50.11        | 0.67        | 66.82        | 62.28        | 49.16        | 1.97        | 68.79        | 66.14        | 50.84        | 6.94         |
| Replicate 3    | 67.68        | 62.44        | 50.43        | 67.91        | 63.08        | 50.63        | 1.08        | 67.96        | 63.55        | 50.15        | 2.39        | 69.60        | 67.05        | 51.19        | 7.34         |
| <b>Average</b> | <b>67.50</b> | <b>62.22</b> | <b>50.19</b> | <b>67.48</b> | <b>62.54</b> | <b>50.43</b> | <b>0.84</b> | <b>67.64</b> | <b>63.38</b> | <b>49.89</b> | <b>2.77</b> | <b>69.81</b> | <b>67.83</b> | <b>51.38</b> | <b>8.78</b>  |
| T              | 66.46        | 60.53        | 47.17        | 66.94        | 61.65        | 47.40        | 1.83        | 67.89        | 64.44        | 47.41        | 6.96        | 70.76        | 70.42        | 49.26        | 15.01        |
| Replicate 2    | 66.47        | 60.21        | 46.49        | 66.01        | 60.17        | 46.44        | 0.93        | 66.89        | 62.22        | 46.51        | 4.28        | 71.12        | 71.10        | 48.87        | 16.58        |
| Replicate 3    | 66.71        | 60.62        | 47.08        | 66.88        | 61.65        | 47.27        | 2.20        | 68.05        | 64.24        | 47.36        | 6.39        | 71.64        | 72.08        | 49.45        | 17.31        |
| <b>Average</b> | <b>66.55</b> | <b>60.45</b> | <b>46.91</b> | <b>66.61</b> | <b>61.16</b> | <b>47.04</b> | <b>1.65</b> | <b>67.61</b> | <b>63.63</b> | <b>47.09</b> | <b>5.88</b> | <b>71.17</b> | <b>71.20</b> | <b>49.19</b> | <b>16.30</b> |

|                | Day 4        |              |              |             | Day 5        |              |              |              | Day 6        |              |              |              | Day 7        |              |              |              |
|----------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
|                | X            | Y            | Z            | ΔE          | X            | Y            | Z            | ΔE           | X            | Y            | Z            | ΔE           | X            | Y            | Z            | ΔE           |
| A              | 67.88        | 64.38        | 48.59        | 5.95        | 68.28        | 65.32        | 48.59        | 7.52         | 68.68        | 66.33        | 48.68        | 9.17         | 69.11        | 67.22        | 48.83        | 10.42        |
| Replicate 2    | 68.06        | 65.22        | 48.26        | 7.96        | 67.70        | 65.57        | 47.92        | 9.61         | 68.89        | 67.63        | 48.51        | 12.04        | 69.20        | 68.23        | 48.59        | 12.86        |
| Replicate 3    | 66.72        | 62.86        | 48.07        | 4.52        | 66.64        | 63.08        | 47.95        | 5.28         | 66.85        | 63.45        | 48.00        | 5.76         | 67.16        | 64.00        | 47.97        | 6.57         |
| <b>Average</b> | <b>67.55</b> | <b>64.15</b> | <b>48.31</b> | <b>6.14</b> | <b>67.54</b> | <b>64.66</b> | <b>48.15</b> | <b>7.47</b>  | <b>68.14</b> | <b>65.80</b> | <b>48.40</b> | <b>8.99</b>  | <b>68.49</b> | <b>66.48</b> | <b>48.46</b> | <b>9.95</b>  |
| B              | 67.97        | 63.56        | 50.93        | 2.36        | 67.90        | 63.56        | 50.79        | 2.55         | 67.82        | 63.47        | 50.82        | 2.48         | 67.78        | 63.50        | 50.71        | 2.66         |
| Replicate 2    | 68.32        | 63.92        | 51.17        | 2.58        | 68.28        | 64.28        | 50.99        | 3.62         | 68.11        | 64.02        | 50.85        | 3.35         | 67.87        | 63.91        | 50.62        | 3.67         |
| Replicate 3    | 67.94        | 63.53        | 51.06        | 2.19        | 68.03        | 63.84        | 51.05        | 2.80         | 68.05        | 63.96        | 51.03        | 3.07         | 67.74        | 63.66        | 50.75        | 3.06         |
| <b>Average</b> | <b>68.08</b> | <b>63.67</b> | <b>51.05</b> | <b>2.38</b> | <b>68.07</b> | <b>63.89</b> | <b>50.94</b> | <b>2.99</b>  | <b>67.99</b> | <b>63.82</b> | <b>50.90</b> | <b>2.97</b>  | <b>67.80</b> | <b>63.69</b> | <b>50.69</b> | <b>3.13</b>  |
| C              | 68.84        | 69.51        | 51.94        | 13.17       | 68.44        | 69.10        | 51.53        | 13.11        | 69.10        | 69.50        | 51.67        | 12.76        | 68.66        | 68.87        | 51.36        | 12.24        |
| Replicate 2    | 67.45        | 64.63        | 50.34        | 5.56        | 67.88        | 65.64        | 50.78        | 7.00         | 68.17        | 66.58        | 51.01        | 8.60         | 67.96        | 66.61        | 50.77        | 9.20         |
| Replicate 3    | 67.23        | 63.36        | 50.31        | 2.77        | 67.07        | 63.33        | 50.17        | 3.07         | 66.61        | 63.20        | 49.61        | 3.91         | 66.71        | 63.42        | 49.85        | 4.16         |
| <b>Average</b> | <b>67.84</b> | <b>65.83</b> | <b>50.86</b> | <b>7.17</b> | <b>67.80</b> | <b>66.02</b> | <b>50.83</b> | <b>7.73</b>  | <b>67.96</b> | <b>66.43</b> | <b>50.76</b> | <b>8.42</b>  | <b>67.78</b> | <b>66.30</b> | <b>50.66</b> | <b>8.53</b>  |
| D              | 67.00        | 61.92        | 50.52        | 1.02        | 66.66        | 61.62        | 50.20        | 1.14         | 66.96        | 61.88        | 50.45        | 1.02         | 66.91        | 61.91        | 50.35        | 1.21         |
| Replicate 2    | 67.53        | 62.93        | 50.54        | 2.36        | 67.49        | 63.01        | 50.46        | 2.69         | 67.65        | 63.34        | 50.52        | 3.16         | 67.19        | 62.96        | 50.06        | 3.33         |
| Replicate 3    | 67.60        | 63.11        | 50.72        | 2.43        | 67.33        | 63.14        | 50.39        | 3.19         | 67.32        | 63.12        | 50.38        | 3.17         | 67.31        | 63.35        | 50.21        | 3.84         |
| <b>Average</b> | <b>67.38</b> | <b>62.65</b> | <b>50.59</b> | <b>1.94</b> | <b>67.16</b> | <b>62.59</b> | <b>50.35</b> | <b>2.34</b>  | <b>67.31</b> | <b>62.78</b> | <b>50.45</b> | <b>2.45</b>  | <b>67.14</b> | <b>62.74</b> | <b>50.21</b> | <b>2.79</b>  |
| E              | 70.91        | 72.97        | 58.67        | 12.38       | 71.60        | 75.07        | 59.23        | 15.60        | 71.79        | 75.62        | 59.37        | 16.41        | 71.62        | 75.82        | 59.12        | 17.25        |
| Replicate 2    | 68.98        | 69.30        | 57.16        | 8.12        | 69.34        | 69.97        | 57.49        | 8.88         | 69.04        | 69.93        | 57.15        | 8.78         | 69.64        | 70.80        | 57.56        | 10.21        |
| Replicate 3    | 69.32        | 69.71        | 57.10        | 8.45        | 69.87        | 71.02        | 57.63        | 10.23        | 69.59        | 70.19        | 57.66        | 8.84         | 69.79        | 71.25        | 57.45        | 10.98        |
| <b>Average</b> | <b>69.74</b> | <b>70.66</b> | <b>57.64</b> | <b>9.65</b> | <b>70.27</b> | <b>72.02</b> | <b>58.12</b> | <b>11.57</b> | <b>70.14</b> | <b>71.91</b> | <b>58.06</b> | <b>11.34</b> | <b>70.35</b> | <b>72.62</b> | <b>58.04</b> | <b>12.81</b> |
| F              | 70.26        | 72.70        | 56.45        | 15.19       | 70.42        | 73.48        | 56.51        | 16.62        | 70.25        | 73.11        | 56.23        | 16.23        | 70.43        | 74.18        | 56.32        | 18.26        |
| Replicate 2    | 68.68        | 68.87        | 55.23        | 9.83        | 68.30        | 68.16        | 54.96        | 8.98         | 69.43        | 71.20        | 55.60        | 13.69        | 68.25        | 68.76        | 54.77        | 10.56        |

|             |              |              |              |              |              |              |              |              |              |              |              |              |              |              |              |              |
|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Replicate 3 | 69.65        | 70.92        | 55.82        | 12.59        | 70.29        | 72.73        | 56.28        | 15.35        | 70.69        | 74.01        | 56.63        | 17.34        | 70.62        | 74.11        | 56.57        | 17.72        |
| Average     | <b>69.53</b> | <b>70.83</b> | <b>55.83</b> | <b>12.54</b> | <b>69.67</b> | <b>71.46</b> | <b>55.92</b> | <b>13.65</b> | <b>70.12</b> | <b>72.77</b> | <b>56.15</b> | <b>15.75</b> | <b>69.77</b> | <b>72.35</b> | <b>55.89</b> | <b>15.51</b> |
| G           | 63.54        | 57.70        | 43.05        | 1.38         | 63.10        | 57.41        | 42.64        | 1.73         | 63.16        | 57.71        | 42.76        | 2.31         | 62.79        | 57.29        | 42.39        | 2.19         |
| Replicate 2 | 68.60        | 67.63        | 45.41        | 15.40        | 69.42        | 69.64        | 45.74        | 18.42        | 70.06        | 70.96        | 46.17        | 20.13        | 70.12        | 71.66        | 45.88        | 21.74        |
| Replicate 3 | 66.78        | 64.63        | 44.43        | 11.93        | 68.18        | 67.19        | 45.07        | 15.16        | 68.26        | 67.71        | 45.08        | 16.24        | 68.36        | 68.06        | 45.10        | 16.86        |
| Average     | <b>66.31</b> | <b>63.32</b> | <b>44.30</b> | <b>9.57</b>  | <b>66.90</b> | <b>64.75</b> | <b>44.48</b> | <b>11.77</b> | <b>67.16</b> | <b>65.46</b> | <b>44.67</b> | <b>12.89</b> | <b>67.09</b> | <b>65.67</b> | <b>44.46</b> | <b>13.60</b> |
| H           | 69.07        | 66.73        | 51.14        | 7.19         | 69.93        | 68.92        | 51.46        | 10.62        | 70.03        | 69.10        | 51.46        | 10.86        | 70.42        | 69.82        | 51.55        | 11.78        |
| Replicate 2 | 68.81        | 65.32        | 50.86        | 4.52         | 69.37        | 66.72        | 51.01        | 6.77         | 69.49        | 67.70        | 50.99        | 7.41         | 69.76        | 68.11        | 50.93        | 9.41         |
| Replicate 3 | 69.46        | 67.11        | 51.38        | 7.22         | 69.77        | 68.36        | 51.10        | 9.73         | 70.37        | 69.40        | 51.82        | 10.72        | 70.51        | 70.31        | 51.42        | 12.77        |
| Average     | <b>69.11</b> | <b>66.39</b> | <b>51.13</b> | <b>6.31</b>  | <b>69.69</b> | <b>68.00</b> | <b>51.19</b> | <b>9.04</b>  | <b>69.96</b> | <b>68.73</b> | <b>51.42</b> | <b>9.66</b>  | <b>70.23</b> | <b>69.41</b> | <b>51.30</b> | <b>11.32</b> |
| I           | 69.46        | 68.42        | 48.11        | 12.04        | 70.82        | 72.31        | 49.08        | 18.08        | 71.15        | 73.16        | 49.35        | 19.29        | 71.22        | 73.58        | 49.17        | 20.18        |
| Replicate 2 | 68.11        | 65.29        | 47.29        | 7.38         | 69.30        | 66.01        | 47.32        | 8.73         | 68.82        | 67.50        | 47.70        | 11.15        | 69.24        | 68.22        | 47.73        | 12.05        |
| Replicate 3 | 68.91        | 66.92        | 47.57        | 9.61         | 69.88        | 69.95        | 48.12        | 14.68        | 70.08        | 69.94        | 48.07        | 14.32        | 69.92        | 70.01        | 47.97        | 14.82        |
| Average     | <b>68.83</b> | <b>66.88</b> | <b>47.66</b> | <b>9.68</b>  | <b>70.00</b> | <b>69.42</b> | <b>48.17</b> | <b>13.83</b> | <b>70.02</b> | <b>70.20</b> | <b>48.37</b> | <b>14.92</b> | <b>70.13</b> | <b>70.60</b> | <b>48.29</b> | <b>15.68</b> |
| S           | 73.69        | 76.25        | 53.91        | 19.92        | 74.81        | 79.01        | 54.59        | 23.62        | 75.19        | 79.85        | 54.77        | 24.65        | 74.85        | 79.65        | 54.30        | 25.01        |
| Replicate 2 | 70.17        | 68.80        | 51.68        | 10.34        | 72.96        | 75.78        | 53.47        | 20.34        | 73.77        | 76.92        | 54.01        | 21.17        | 73.49        | 77.48        | 53.57        | 23.06        |
| Replicate 3 | 70.83        | 69.68        | 52.09        | 10.88        | 71.58        | 71.65        | 52.37        | 13.94        | 71.53        | 71.42        | 52.45        | 13.45        | 71.30        | 71.42        | 51.95        | 14.10        |
| Average     | <b>71.56</b> | <b>71.58</b> | <b>52.56</b> | <b>13.71</b> | <b>73.12</b> | <b>75.48</b> | <b>53.48</b> | <b>19.30</b> | <b>73.50</b> | <b>76.06</b> | <b>53.74</b> | <b>19.76</b> | <b>73.21</b> | <b>76.18</b> | <b>53.27</b> | <b>20.72</b> |
| T           | 72.40        | 73.62        | 50.38        | 18.83        | 73.45        | 76.80        | 51.01        | 23.65        | 73.77        | 77.69        | 51.10        | 24.97        | 73.45        | 77.77        | 50.85        | 25.82        |
| Replicate 2 | 73.76        | 76.38        | 50.44        | 22.97        | 74.86        | 78.92        | 51.00        | 26.26        | 75.00        | 79.66        | 50.96        | 27.61        | 74.55        | 79.55        | 50.51        | 28.34        |
| Replicate 3 | 74.13        | 77.55        | 51.05        | 24.28        | 74.54        | 78.80        | 51.08        | 26.22        | 75.39        | 79.88        | 51.52        | 26.85        | 74.69        | 80.08        | 51.25        | 28.59        |
| Average     | <b>73.43</b> | <b>75.85</b> | <b>50.62</b> | <b>22.03</b> | <b>74.28</b> | <b>78.17</b> | <b>51.03</b> | <b>25.38</b> | <b>74.72</b> | <b>79.08</b> | <b>51.19</b> | <b>26.48</b> | <b>74.23</b> | <b>79.13</b> | <b>50.87</b> | <b>27.58</b> |

|             | X            | Y            | Z            | $\Delta E$  | Visual   |
|-------------|--------------|--------------|--------------|-------------|----------|
| A           | 68.03        | 65.98        | 48.01        | 9.83        | 0        |
| Replicate 2 | 68.19        | 67.06        | 47.89        | 12.29       | 0        |
| Replicate 3 | 65.79        | 61.84        | 47.29        | 4.14        | 0        |
| Average     | <b>67.34</b> | <b>64.96</b> | <b>47.73</b> | <b>8.75</b> | <b>0</b> |
| B           | 67.70        | 63.33        | 50.48        | 2.51        | 2        |
| Replicate 2 | 67.47        | 63.62        | 50.04        | 3.98        | 0        |
| Replicate 3 | 67.27        | 63.20        | 50.20        | 3.11        | 0        |
| Average     | <b>67.48</b> | <b>63.38</b> | <b>50.24</b> | <b>3.20</b> | <b>1</b> |
| C           | 68.32        | 68.29        | 50.73        | 11.78       | 0        |
| Replicate 2 | 67.88        | 66.72        | 50.45        | 9.72        | 0        |
| Replicate 3 | 66.42        | 63.37        | 49.24        | 4.87        | 0        |
| Average     | <b>67.54</b> | <b>66.13</b> | <b>50.14</b> | <b>8.79</b> | <b>0</b> |
| D           | 66.27        | 61.38        | 49.80        | 1.51        | 4        |
| Replicate 2 | 66.72        | 62.21        | 49.72        | 2.54        | 0        |
| Replicate 3 | 66.19        | 61.99        | 49.14        | 3.20        | 0        |
| Average     | <b>66.39</b> | <b>61.86</b> | <b>49.55</b> | <b>2.42</b> | <b>1</b> |

|             |              |              |              |              |          |
|-------------|--------------|--------------|--------------|--------------|----------|
| E           | 70.56        | 74.46        | 58.14        | 16.55        | 0        |
| Replicate 2 | 69.43        | 71.15        | 57.23        | 11.52        | 0        |
| Replicate 3 | 69.29        | 70.61        | 56.86        | 10.69        | 0        |
| Average     | <b>69.76</b> | <b>72.07</b> | <b>57.41</b> | <b>12.92</b> | <b>0</b> |
| F           | 69.61        | 72.93        | 55.37        | 17.34        | 0        |
| Replicate 2 | 67.93        | 68.61        | 54.22        | 11.05        | 0        |
| Replicate 3 | 70.00        | 73.38        | 55.71        | 17.57        | 0        |
| Average     | <b>69.18</b> | <b>71.64</b> | <b>55.10</b> | <b>15.32</b> | <b>0</b> |
| G           | 61.65        | 56.51        | 41.54        | 3.04         | 2        |
| Replicate 2 | 69.39        | 70.43        | 45.08        | 20.64        | 0        |
| Replicate 3 | 68.30        | 68.69        | 44.64        | 18.69        | 0        |
| Average     | <b>66.45</b> | <b>65.21</b> | <b>43.75</b> | <b>14.12</b> | <b>1</b> |
| H           | 70.00        | 70.05        | 51.13        | 13.26        | 0        |
| Replicate 2 | 70.08        | 69.23        | 51.17        | 11.32        | 0        |
| Replicate 3 | 69.54        | 68.61        | 50.49        | 11.04        | 0        |
| Average     | <b>69.87</b> | <b>69.30</b> | <b>50.93</b> | <b>11.87</b> | <b>0</b> |
| I           | 70.77        | 73.35        | 48.75        | 20.66        | 0        |
| Replicate 2 | 69.13        | 68.45        | 47.66        | 12.82        | 0        |
| Replicate 3 | 68.25        | 66.93        | 46.50        | 11.38        | 0        |
| Average     | <b>69.38</b> | <b>69.58</b> | <b>47.64</b> | <b>14.95</b> | <b>0</b> |
| S           | 74.35        | 79.17        | 54.10        | 24.95        | 0        |
| Replicate 2 | 72.21        | 75.51        | 52.87        | 21.34        | 0        |
| Replicate 3 | 71.79        | 72.93        | 52.03        | 16.60        | 0        |
| Average     | <b>72.78</b> | <b>75.87</b> | <b>53.00</b> | <b>20.96</b> | <b>0</b> |
| T           | 72.98        | 76.76        | 50.43        | 24.66        | 0        |
| Replicate 2 | 74.59        | 79.33        | 50.00        | 28.05        | 0        |
| Replicate 3 | 74.99        | 79.34        | 50.64        | 26.78        | 0        |
| Average     | <b>74.19</b> | <b>78.48</b> | <b>50.36</b> | <b>26.50</b> | <b>0</b> |