## MOBILE CARB PHASE 3 - REFORMULATED GASOLINE AND MTBE PHASEOUT

TRAFFIC IMPACT ANALYSIS

July 2014



### Mobil CARB Phase 3 Reformulated Gasoline and MTBE Phaseout Project Traffic Impact Analysis

Prepared for:

**ENSR** 

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## Chapter 1.0 **INTRODUCTION**

### 1.1 INTRODUCTION

This report presents the results of a traffic analysis performed for the proposed Mobil project to modify their Torrance Refinery to satisfy the California mandated phase out of methyl tertiary butyl ether (MTBE) from gasoline by December 31, 2002 and provide reformulated gasoline that complies with California Air Resources Board (CARB) Phase 3 fuel specifications. This report has been prepared for the Environmental Impact Report on the proposed project.

### 1.2 PROJECT DESCRIPTION

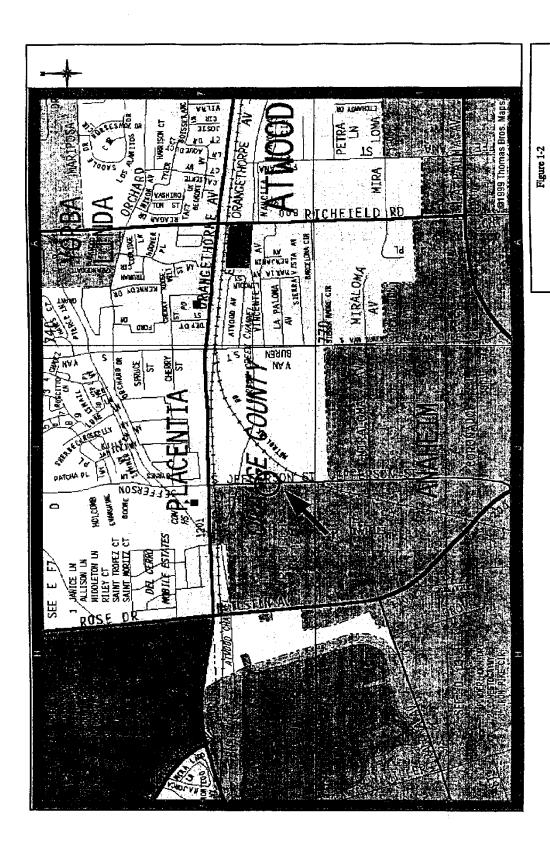
To comply with the CARB Phase 3 fuel specifications and MTBE phase-out requirement, Mobil proposes to modify existing process operating units and install new equipment at its Torrance Refinery. To meet the new CARBoxygenate requirements, ethanol will be blended into the gasoline. The ethanol will not be blended at the refinery, as has been the case with MTBE. Rather ethanol will blended with base gasoline stocks at Mobil's distribution facilities. Therefore, modifications to several existing terminals in Southern California will be required, as well as at the refinery itself. The terminals are located in the cities of Vernon, Anaheim (Atwood Terminal), and on Terminal Island in the Port of Los Angeles (Southwestern Terminal), as illustrated in Figures 1-1 through 1-3. Modifications also will be required at Mobil's Torrance Loading Rack, a distribution terminal located on the property of the Torrance Refinery.

The Torrance Refinery is located at 3700 West 190<sup>th</sup> Street in the City of Torrance. The Torrance Refinery occupies an irregularly shaped parcel between 190<sup>th</sup> Street on the north, Van Ness Avenue on the east, Railroad tracks and Del Amo Boulevard to the south, and Prairie Avenue to the west. A small portion of the refinery property is located to the west of Prairie Avenue. The refinery comprises approximately 660 acres of land, as illustrated in Figure 1-4. The Torrance Loading Rack is located in the central southwestern portion of the Torrance refinery property.

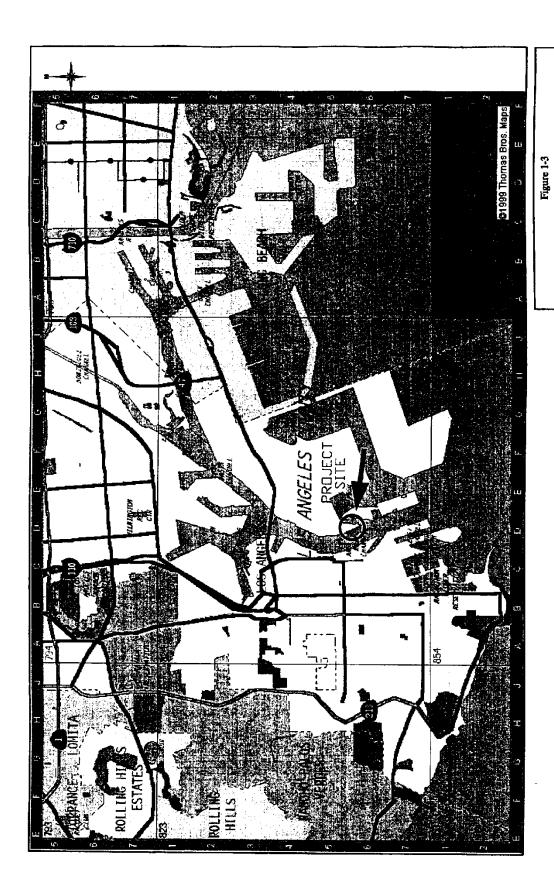
1-2

Mobil CARB Phase 3 Reformulated Gasoline and MTBE Phaseout Traffic Impact Analysis

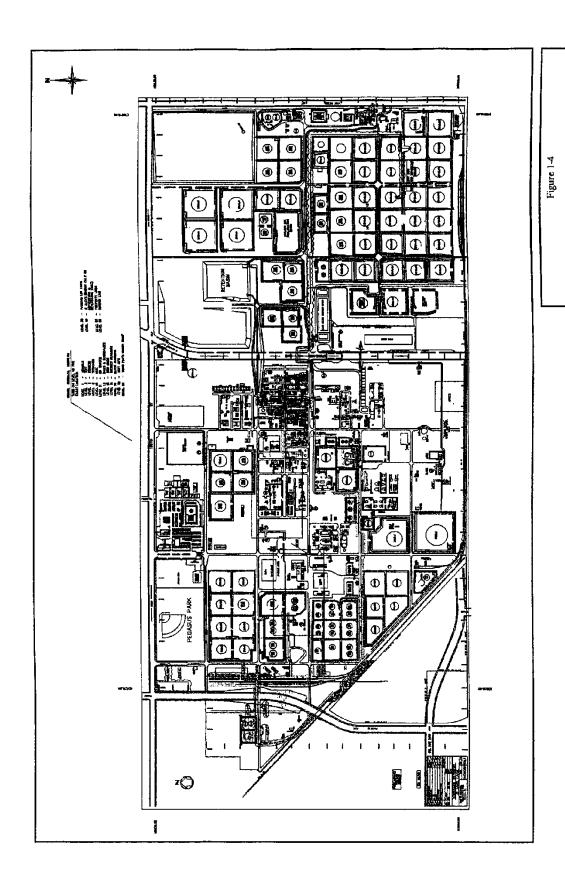
PROJECT VICINITY MAP (Atwood Terminal)



PROJECT VICINITY MAP (Marine Terminal, Terminal Island)



PROJECT SITE PLAN (Torrance Refinery)



The Vernon Terminal is located at 2709 East 37<sup>th</sup> Street in the City of Vernon. It is a distribution terminal and is located in an area zoned "General Industry" and comprises approximately 32 acres of land.

The Atwood Terminal is located at 1477 Jefferson Street in the City of Anaheim. This facility is located in an area zoned "Development Area 1- Northeast Area Specific Plan - Industrial Area" and includes approximately eight acres of land.

The Southwestern Terminal is located at 799 South Seaside Avenue on Terminal Island in the POLA. This marine terminal consists of approximately 14 acres of land, including four berths, and is located in an area zoned "Qualified Manufacturing".

The additions and modifications proposed as part of the CARB Phase 3 project are summarized in the following section.

### 1.2.1 Changes at the Torrance Refinery Site

- Installation of new rail spur and rail car unloading facilities, and new/upgraded storage tankage for fuel ethanol
- Modification of two FCC compressors
- Installation of new C4/C5 splitter and modification of Debutanizer and Deisobutanizer
- Installation of new Merichem unit and modifications to exiting Merox unit, both to reduce the amount of sulfur in gasoline. New piping, pumps, containment dikes, for the new tankage and loading/unloading facilities.

- New unsaturaged gas plan sidstriper equipment
- New rail spur, storage tanks, and loading/unloading facilities for export and return of pentane (C5)
- New truck unloading lane at existing rack, new truck unloading rack, and vapor destruction unit, and modifications to two existing truck loading racks for fuel ethanol blending (all at Torrance Loading Rack, located on the refinery property)

1.2.2 Improvements at the Mobil Terminals

The improvements at the various terminals other than the Torrance Loading Rack (discussed

above with the refinery changes because the Loading Rack is on the refinery property), include

construction of new storage tanks and conversion of existing tanks for ethanol and gasoline storage, as

well as construction of new and modified truck loading and unloading facilities and equipment for storing

fuel ethanol and loading CARB Phase 3 gasoline. The proposed construction also includes new piping,

pumps, containment, etc.

1.3 ANALYSIS SCOPE

The traffic analysis examines the impacts of adding construction project generated traffic to

existing traffic on the surrounding arterial network. This project is subject to a Congestion Management

Program (CMP) analysis if the project is not determined to be exempt under the guidelines for the County

of Los Angeles. This methodology requires a project to mitigate the project's traffic impact to level of

service (LOS) "E", the acceptable level of service, or better whenever the traffic generated by the

proposed development causes the level of service (LOS) of identified CMP intersections to change by .02,

causing or worsening to LOS "F".

The project is also subject to the following significance criteria from the South Coast Air Quality

Management District (SCAQMD) (the lead agency for this project).

Impacts to transportation and circulation will be considered significant if the following criteria are met:

A major roadway or railroad is closed to all through traffic and no alternate route is

available.

Peak period levels on major arterials within the vicinity of LAR and terminals are disrupted

to a point where intersections with a LOS of "C" or worse are reduced one full level as a

result of the project for more than four weeks.

The project will increase traffic to and/or from any one facility or site by more than 350

truck trips per day.

Mobile CARB Phase 3 Reformulated Gasoline and MTBE Phaseout

- The project will increase customer traffic to a facility by more than 700 trips per day.
- The volume to capacity ratio increases by two percent for intersections with a LOS rating of "E" or "F" for more than two months.

The traffic analysis material presented here is set out as follows:

Chapter 2.0 - Project Setting

Chapter 3.0 - Traffic Impact Analysis

Chapter 4.0 - Mitigation Measures

### 1.4 **DEFINITIONS**

Certain terms used throughout this report are defined below to clarify their intended meaning:

ADT - Average Daily Traffic.

ICU - Intersection Capacity Utilization. A factor used to measure the volume to capacity ratio for an intersection and determine the level of service.

LOS

- Level of Service. A scale used to evaluate circulation system performance based on intersection ICU values or volume/capacity ratios of arterial segments.

The levels range from "A" to "F", with LOS "A" representing free flow traffic and LOS "F" representing severe traffic congestion.

Peak Hour - This typically refers to the hour during the AM peak period (typically 7 AM - 9 AM) or the PM peak period (typically 3 PM - 6 PM) in which the greatest number of vehicle trips are generated by a given land use or are travelling on a given roadway.

VPD - Vehicles per Day. This has the same meaning as ADT but is generally used in a trip generation context rather than in reference to the highway volume of an arterial segment.

VPH - Vehicles per Hour.

V/C - Volume to Capacity Ratio. This is typically described as a percentage of capacity utilized by existing or projected traffic on a segment of arterial or an intersection turn movement.

# Chapter 2.0 **PROJECT SETTING**

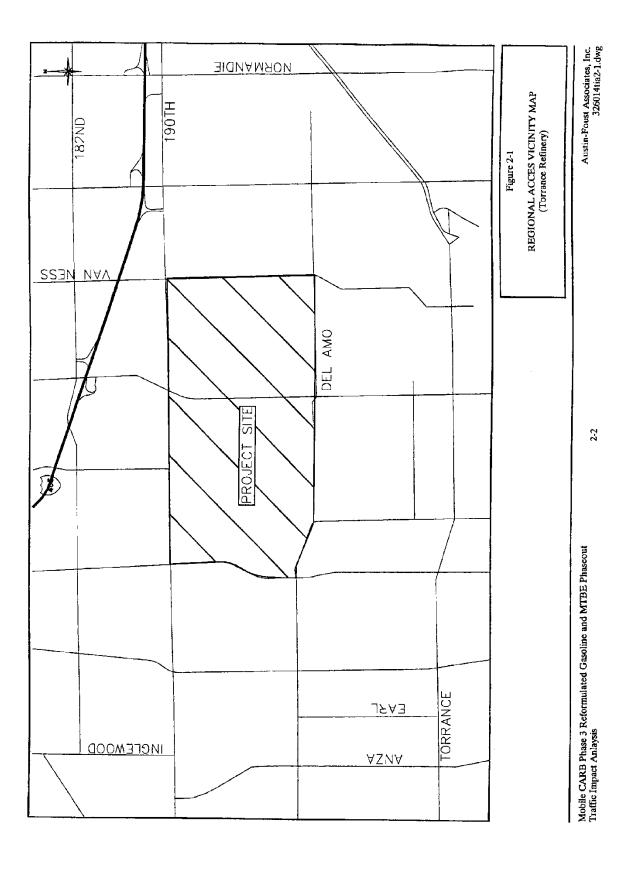
This chapter describes the project site in relation to the transportation setting. The existing circulation system is discussed, and existing traffic volumes and levels of service are summarized.

### 2.1 SURROUNDING HIGHWAY NETWORK

Regional transportation facilities in the vicinity of the Mobil's Torrance site are illustrated in Figure 2-1, and provide excellent accessibility to the entire southern California region. The San Diego Freeway (Interstate 405) lies immediately north of the Torrance Refinery and Torrance Loading Rack, and provides full ramp connections at Crenshaw Boulevard and Western Avenue.

Construction traffic generated by the proposed project at the refinery location will access a 375 space parking area located near the southwest corner of Crenshaw Boulevard and 190<sup>th</sup> Street via a construction gate located on 190<sup>th</sup> Street.

The anticipated construction traffic at the various terminal locations (Vernon, Southwestern, and Atwood) is forecast to be small because of the small construction work force, and will have impacts only during a short (8-10 months) period. Access to these terminal sites is available via direct access routes to regional roadway and freeway facilities. Impacts for the refinery site will be of a longer duration (28 months), and also will include the impacts of the modest construction traffic associated with the modifications to the Torrance Loading Rack, which will overlap with the Torrance Refinery additions and modifications. Therefore, this study focuses on the impacts from construction traffic at the Torrance Refinery location.



Because the proposed project is expected to require no or negligible additional workers at either the refinery or the various terminals during the operational phase, there would be negligible traffic impact potential. Therefore, this study does not address operational phase impacts.

### 2.2 EXISTING TRAFFIC CONDITIONS

As stated earlier, the Torrance Refinery is located at 3700 West 190<sup>th</sup> Street in the City of Torrance. The Torrance Refinery occupies an irregularly shaped parcel between 190<sup>th</sup> Street on the north, Van Ness Avenue on the east, Railroad tracks and Del Amo Boulevard to the south, and Prairie Avenue to the west. A small portion of the refinery property is located to the west of Prairie Avenue. The Torrance Loading Rack is located in the west central portion of the refinery property.

The following 15 intersections have been included in the traffic analysis:

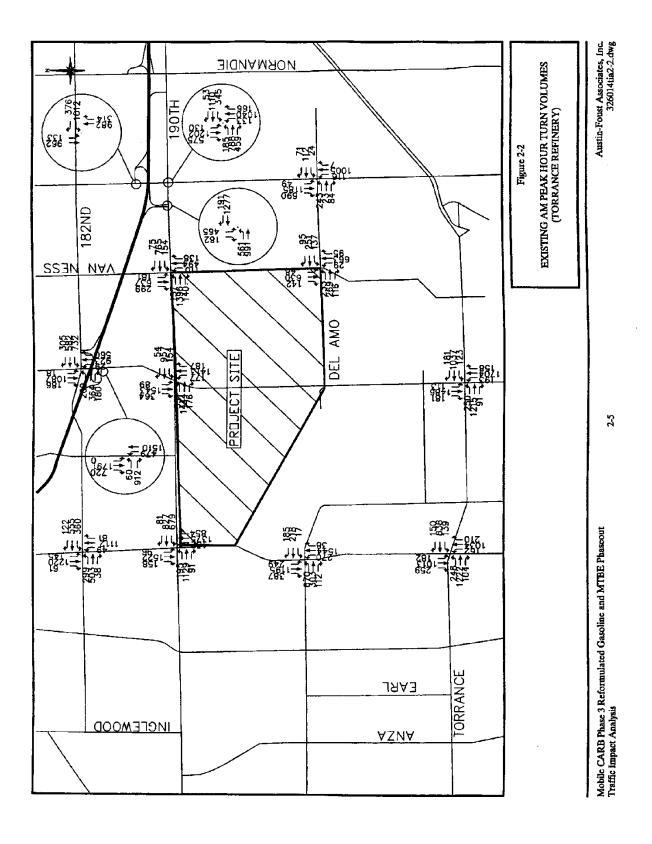
- 1. Prairie Ave & 182<sup>nd</sup> St
- 2. Crenshaw Blvd & 182<sup>nd</sup> Street
- 3. I-405 NB on/off & 182<sup>nd</sup> St Ave
- 4. Prairie Ave & 190<sup>th</sup> Street
- 5. Crenshaw Blvd & 190<sup>th</sup> St
- 6. Van Ness Avenue & 190<sup>th</sup> Street
- 7. Western Avenue & 190<sup>th</sup> Street
- 8. Prairie & Del Amo Boulevard

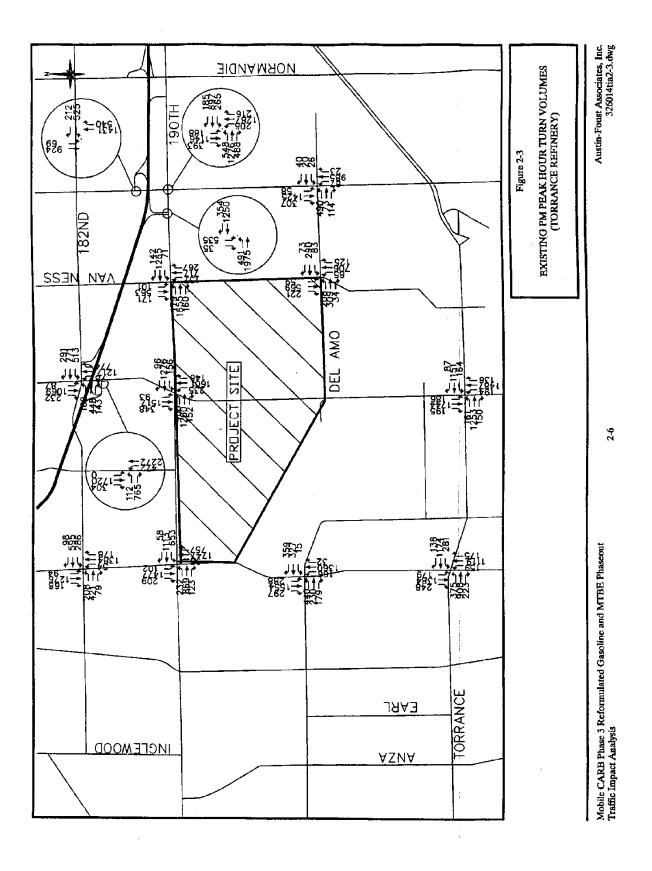
- 9. Crenshaw Blvd & I-405 SN on/off
- 10. Van Ness Ave & Del Amo
- 11. Western Ave & Del Amo Blvd
- 12. IB405 SB on/off & 190<sup>th</sup> Street
- 13. Western Ave & I-405 NB on/off
- 14. Prairie/Madrona & Torrance Boulevard
- 15. Crenshaw Blvd & Torrance Boulevard

Existing AM and PM peak hour turning movement volumes at these intersections were counted by Traffic Data Services, Inc. In December 2000 and are illustrated in Figures 2-2 and 2-3. Intersection capacity utilization (ICU) values are presented in Table 2-1 (actual ICU calculations are included in Appendix A) and are a means of representing peak hour volume/capacity ratios. The ICU is the proportion of an hour required to provide sufficient capacity to accommodate all intersection traffic if all approaches operate at capacity. If an intersection is operating at 80 percent of capacity, then 20 percent of the signal cycle is not used. The signal could show red on all indications 20 percent of the time and the signal would just accommodate approaching traffic. As shown I the following Table 2-1, seven intersections (Crenshaw Boulevard and 182nd Street, I-405 NB on/off and 182nd Street, Prairie Avenue and 190th Street, Crenshaw Boulevard and 190th Street, Van Ness Avenue and 190th Street, Crenshaw

Boulevard and I-405 SB on/off, and I-405 SB on/off and 190<sup>th</sup> Street), are presently operating at an unacceptable level of service during the AM or PM peak hour under existing conditions, based the intersection capacity utilization criteria used by the City of Torrance.

TABLE 2-1 ICU SUMMARY - EXISTING COND	ITIONS	
	EXIST	ING
INTERSECTION	AM	PM
1. Prairie & 182nd	0.94	0.94
2. Crenshaw & 182nd	0.89	1.11 *
3. I-405 & 182nd	0.70	1.18 *
4. Prairie & 190th	1.09 *	1.04 *
5. Crenshaw & 190th	0.94	1.10 *
6. Van Ness & 190th	1.04 *	1.03 *
7. Western & 190th	0.88	0.88
8. Prairie & Del Amo	0.80	0.77
9. Crenshaw & I-405 SB on/off	1.11 *	0.98
10. Van Ness & Del Amo	0.74	0.76
11. Western & Del Amo	0.82	0.86
12. I-405 SB on/off & 190th	1.05 *	0.98
13. Western & I-405 NB on/off	0.93	0.82
14. Prairie/Madrona & Torrance	0.84	0.83
15. Crenshaw & Torrance	0.95	1.00
* Exceeds acceptable LOS 'E'		
Level of Service Ranges: .0060 A		
.6170 B		
.7180 C		
.8190 D		
.91 - 1.00 E		
Above 1.00 F		





## Chapter 3.0 TRAFFIC IMPACT ANALYSIS

This chapter describes the potential impacts of the proposed project upon the surrounding arterial network in the vicinity of the Torrance Refinery and Torrance Loading Rack. As stated in Chapter 2, impacts are discussed for the project construction phase only, because there will be no or negligible additional employment and associated traffic volumes during project operations. As also stated in Chapter 2, the traffic analysis only briefly addresses construction impacts at the Southwestern, Vernon, and Southwestern Terminals, because construction phase traffic will be small and short-term. Because there will be no or negligible increases in employment and traffic at the terminals during operations, no analysis is provided of traffic impacts during operations at the terminals.

In the following section, traffic generated by development of the proposed project is added to the existing conditions presented in the previous chapter and the resulting capacity impacts are assessed.

### 3.1 TRIP GENERATION

As discussed in Chapter 1, the Mobil's Torrance Refinery is proposing to construct or modify a number of process operating units, and to construct some new equipment and facilities. To meet the oxygenate requirements of the CARB Phase 3 fuel specifications, , ethanol will be blended into the gasoline. The ethanol will not be blended at the refinery, as has been the case with MTBE, but rather, ethanol blending will be performed at distribution facilities. Therefore, modifications will be required at the Torrance Refinery, the Torrance Loading Rack (located on the refinery property, and terminals in the cities of Vernon (Vernon Terminal) and Anaheim (Atwood Terminal), and onTerminal Island in the Port of Los Angeles (Southwestern Terminal).

The construction activities at the various terminals will occur between December 2001 and be the end of October 2002. Actual construction start dates will vary at the terminal sites, but construction is anticipated to take place five days per week in a single 8-hour shift, from 7:15 a.m. to 3:45 p.m. The maximum duration for construction at an individual terminal will be ten months.

Construction of the proposed project at the refinery is scheduled to begin September 2001 and be completed by December 2003. Construction is anticipated to take place five days per week in a single 8-hour shift, from 7:15 AM to 3:45 PM.

The following table summarizes the anticipated construction vehicles at the refinery and each terminal site for both the peak and average construction periods.

Location			# Workers	# Vehicles	<b>Est. Construction Time</b>
Torrance Torrance (combined)	Refinery Loading	and Rack	126 (peak)	97 (peak)	2 months (Refinery) and 2 months (Loading Rack)
Torrance Torrance (combined)	Refinery Loading	and Rack	65 (average)	52 (average)	26 months (Refinery) and 8 months (Loading Rack)
Southwester			20 (peak)	10-15 (peak)	8 months
Vernon Terr	minal		50+ (peak)	35-40 (peak)	10 months
Atwood Ter	rminal		30+ (peak)	15-20 (peak)	9 months

An examination of this table indicates that the addition of construction workers will be relatively small at the various terminal locations.

At the Torrance Refinery location, the construction effort is anticipated to require a peak of 97 daily vehicles for a two month period during the project's peak construction time. It is anticipated that 126 construction workers will be needed during peak construction, with this peak occurring during the period when construction is ongoing at both the refinery facilities/equipment and Loading Rack. Using an average of 1.3 persons per vehicle for vehicle occupancy (which was observed at the ARCO Refinery in Carson), results in a forecast of 97 inbound and 97 outbound vehicle trips or 194 vehicle trips per day during the peak construction period for the construction workers.

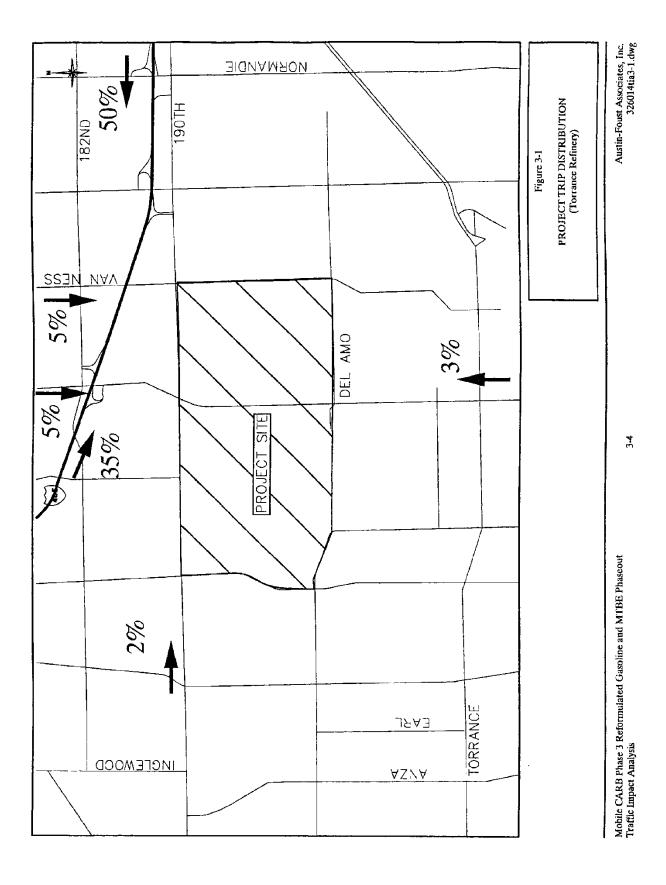
Construction activities at the refinery will occur during a five-day work week beginning at 7:15 AM until 3:45 PM Monday through Friday. This results in an average construction project AM peak hour (6:00 AM to 7:00 AM) of 97 vehicle trips and no trips occurring during the PM peak hour (4:00 PM to 6:00 PM). The AM and PM peak hour of the adjacent street system occurs during the AM peak period of 7:00 AM to 9:00 AM and 4:00 PM to 6:00 PM as indicated in the Congestion Management Program (CMP) Guidelines. Traffic attributable to the construction of the project will leave the site before the PM peak period would begin and will not affect the PM peak hour ICU values. Traffic attributable to the construction of the project will arrive at the site during the AM peak period. Therefore, the analysis examines impacts from traffic attributable to the proposed project only during the AM peak hour.

Materials required to support the construction effort would be delivered to the refinery by truck. Peak truck usage would correspond to the peak manpower periods. Construction materials, heavy construction equipment, piping, and new equipment would be delivered throughout the construction period. Material deliveries would be spread throughout the work day with few deliveries occurring during the peak hour. Therefore, their contribution to the overall traffic impacts would be neglibable.

### 3.2 TRIP DISTRIBUTION

Distribution of project generated traffic was derived from observation of existing travel patterns in the vicinity of the project sites and is illustrated in Figure 3-1. An increase in vehicular movements will occur at the various project sites during the construction period. The anticipated construction traffic at the terminal locations is considered less than significant, ranging from a low of 10 vehicles to a high of 40 vehicles per peak hour over an eight to ten month period. However, construction traffic at the Torrance Refinery is forecast to peak at approximately 97 vehicles. Hence, this analysis is focused on impacts at locations surrounding the Torrance Refinery during the peak construction activity period.

The average daily truck traffic at the refinery during construction is forecast to be approximately 25-30 trucks per day Since these would mainly consist of material deliveries, they would be spread throughout the work day, with few deliveries occurring during the peak hour. Therefore, their contribution to overall traffic impacts would be negligible. As a conservative or "worst case" analysis, the peak number of construction employees at the construction site was assumed to occur daily.



### 3.3 2000/EXISTING PLUS PROJECT TRAFFIC IMPACTS

For analysis purposes, a change of two percent at an intersection caused by the addition of project traffic is considered a significant impact. A typical four-legged intersection, operating at an acceptable level of service, will have approximately 3,000 to 6,000 vehicles using the intersection during a peak hour. To effect a two percent change in the intersection capacity utilization (ICU), a minimum of 60 vehicles during the peak hour would be required (3,000 vehicles X .02= 60 vehicles). The addition of 15-40 vehicle trips at intersections surrounding the terminals is below the minimum of 60 vehicles identified above and will not cause a two percent (.02) change in the ICU value at these intersections. Therefore project traffic at intersections surrounding the terminal locations will not have significant impacts. Additionally, the estimated 10-40 vehicle trips is below the threshold (50 peak hour trips) required by the CMP guidelines. Hence, no additional traffic analysis is required for these locations.

To estimate the project-related traffic volumes at various points on the transportation system adjacent to the refinery and thereby establish the magnitude and extent of traffic impacts, a three-step process was utilized. First, the amount of traffic which would be generated during construction was determined. Second, the construction traffic was geographically distributed to appropriate residential, commercial, and industrial areas. Finally, the trips were assigned to specific roadways and the traffic increases were evaluated on a route-by-route basis.

The proposed project would generate short-term impacts on traffic and circulation in the project vicinity during the construction period. The project would temporarily affect the present pattern of circulation of the labor force as well as rail and truck traffic associated with the construction and operation phases of the project.

Construction traffic related to the project will utilize an existing 375 space parking area located at the refinery near the southwest corner of Crenshaw Boulevard and 190<sup>th</sup> Street during construction. It would not affect the existing refinery facilities or the shipping and receiving facilities at the project site

Roadways in the vicinity of the project would be impacted by the project's construction-related traffic. Project related construction traffic would contribute less than two percent of the daily traffic volume on these roadways.

To more carefully assess the impacts on the surrounding roadways, an intersection capacity utilization (ICU) analysis was conducted for the 15 intersections which would be most directly impacted by project construction traffic.

Analysis year-plus-project intersection volumes for the project were generated by adding the project intersection volumes to the existing Year 2000 background intersection volumes. PM peak hour 2000-plus-project turn volumes are illustrated in Figure 3-2, and corresponding ICUs based on existing lane configurations are summarized in Table 3-1 (actual ICU calculations are included in Appendix A). An examination of Table 3-1 reveals that project construction traffic does cause a significant change (i.e., < .02 change in LOS) on the forecast AM peak hour level of service at two study area locations (Crenshaw Boulevard and 190<sup>th</sup> Street and Western Avenue and I-405 NB on/off ramp). However, project construction traffic is not forecast to cause a significant impact under the CMP guidelines at any of the study area locations (i.e., causing them to become LOS "F") and therefore no off-site mitigation is proposed for these locations.

### 3.4 ON-SITE CIRCULATION AND PARKING

Sufficient on-site parking is available to accommodate the increased parking demand from construction workers at the various terminals. The physical site of the refinery provides a 375 space parking area near the southwest corner of Crenshaw Boulevard and 190<sup>th</sup> Street. The capacity of this lot is well beyond the current operational requirements, which should accommodate both refinery and Torrance Loading Rack construction workers. It is forecast that the total number of parking spaces (375 spaces) will exceed the maximum number of vehicles from construction workers (97 vehicles) and allow for fluctuations in manpower and provide ample maneuvering space for heavy trucks.

3.7

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### TABLE 3-1 ICU SUMMARY - EXISTING PLUS PROJECT CONDITIONS (USING NUMBER OF PEAK WORKERS)

		EXISTING+	
	EXISTING	PROJECT	%
INTERSECTION	AM	AM	CHG
1. Prairie & 182nd	0.94	0.94	-NC-
2. Crenshaw & 182nd	0.89	0.89	-NC-
3. I-405 & 182nd	0.70	0.70	-NC-
4. Prairie & 190th	1.09 *	1.09 *	-NC-
5. Crenshaw & 190th	0.94	0.96	.02
6. Van Ness & 190th	1.04 *	1.04 *	-NC-
7. Western & 190th	0.88	0.89	.01
8. Prairie & Del Amo	0.80	0.80	-NC-
9. Crenshaw & I-405 SB on/off	1.11 *	1.12 *	.01
<ol><li>Van Ness &amp; Del Amo</li></ol>	0.74	0.74	-NC-
<ol><li>Western &amp; Del Amo</li></ol>	0.82	0.82	-NC-
12. I-405 SB on/off & 190th	1.05 *	1.06 *	.01
13. Western & I-405 NB on/off	0.93	0.95	.02
14. Prairie/Madrona & Torrance	0.84	0.84	-NC-
15. Crenshaw & Torrance	0.95	0.95	-NC-

<sup>\*</sup> Exceeds acceptable LOS 'E'

Level of Service Ranges: .00 - .60 A

.61 - .70 B

.71 - .80 C .81 - .90 D

.91 - 1.00 E

Above 1.00 F

Definition of Significant Impact = % change > 2%

# Chapter 4.0 MITIGATION MEASURES

This chapter addresses the capacity deficiencies identified in the project impact analysis presented in the previous chapter.

Project construction traffic does not significantly impact the ICU values at the study locations under the CMP guidelines or the guidelines from SCAQMD, therefore no mitigation is required because of project impacts.

No mitigation measures are proposed for the small increase in truck traffic to and from the refinery related to the transportation of ethanol required for blending with the base gasoline stock.

Adequate off-street parking inside the refinery and at the terminals will be provided to accommodate the peak construction labor force.

The entry point to the refinery for construction, commuter and delivery vehicles minimizes impacts on traffic and circulation patterns on the street system near the refinery, and maintains access for pedestrians, bicyclists, and motor vehicle traffic.

Scheduling of truck operations will disperse deliveries throughout the off-peak hours to minimize peak hour traffic impacts.

If required, truck operations for the delivery of over-size equipment and materials will be conducted to the maximum extent possible during off-peak hours to minimize traffic impacts.

## APPENDIX A INTERSECTION CAPACITY UTILIZATION

### 1. Prairie & 182nd

			AM PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	NOT	V/C	AOT	V/C
NBL	1	1600	49	.03	54	.03
nbt	2	3200	1112	.35*	1384	.43#
NBR	1	1600	81	.05	178	.11
SBL	1	1600	145	.09*	94	.06*
SBT	2	3200	1220	.38	1276	.40
SBR	1	1600	61	.04	168	.11
EBL	1	1600	299	.19	208	.13*
EBT	2	3200	503	.17*	421	.16
EBR	0	0	38		79	
WBL	1	1600	360	.23*	286	.18
WBT	2	3200	555	.21	595	.224
WBR	0	0	122		98	
Clear	rance In	terval		.10*		.10*

	ALD) ATT	Y UTILIZA	mraw.	.94		.94
Clear	ance Int	erval		.10*		.10*
WBR	0	0	122		98	
WBT	2	3200	555	.21	595	.22*
WBL	1	1600	360	.23*	286	.18
EBR	0	0	38		79	
KBT	2	3200	503	.17*	421	.16
KBL	1	1600	299	.19	208	.13*
SBR	1	1600	61	.04	168	.11
SBT	2	3200	<b>122</b> 0	.38	1276	.40
SBL	1	1600	145	.09*	94	.06*
NBR	1	1600	81	.05	178	.11
NBT	2	3200	1112			.43*
NOL	1	1000	47	.03	24	

Existing+Project (Peak #Workers)

1600

NBL

LANES CAPACITY AM PK HOUR V/C

PH PK HOUR VOL V/C

.03

.03

			AM PR	HOUR	PH PK	HOUR
	LANES	CAPACITY	VOL	V/C	AOT	V/C
NBL	1	1600	49	.03	54	.03
nbt	2	3200	1112	.35*	1384	.43
NBR	1	1600	81	.05	178	.11
SBL	1	1600	145	.09±	94	.06
SBT	2	3200	1220	.38	1276	.40
SBR	1	1600	61	.04	168	.11
EBL	1	1600	299	.19	208	.13
EBT	2	3200	503	.17*	421	.16
EBR	0	0	38		79	
WBL	1	1600	360	.23*	286	.18
WBT	2	3200	555	.21	595	.22
WBR	0	0	122		98	

TOTAL CAPACITY UTILIZATION .94

### 2. Crenshaw & 182nd

Exist	ing					
			AM PK	HOUR	PH PK	HOUR
	LANES	CAPACITY	YOL	V/C	VOL	V/C
NBL	1	1600	29	.02	78	.05
NBT	2	3200	923	.29*	1217	.38*
NBR	1	1600	560	.35	774	.48
SBL	1	1600	18	.01*	87	.05*
SBT	3	4800	1087	.27	1069	.27
SBR	0	0	186		232	
EBL	i	1600	209	.13*	162	.10*
EBT	2	3200	364	.17	448	.18
EBR	0	0	180		143	
WBL	2	3200	732	.23	513	.16
WBT	1	1600	582	.36*	771	.48*
WBR	1	1600	305	.19	291	.18
Clear	ance In	terval		.10*		.10*

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		·
TOTAL CAPACITY UTILIZATION	.89	1.11

Existing+Project (Peak #Workers)								
			am pk	HOUR	PM PK	HOUR		
	Lanes	CAPACITY	VOL	V/C	WOL	V/C		
NBL	1	1600	29	.02	78	.05		
NBT	2	3200	923	.29*	1222	.38*		
NBR	1	1600	560	.35	807	.50		
SBL	1	1600	18	.01*	87	.05*		
SBT	3	4800	1092	.27	1069	.27		
SBR	0	0	186		232			
EBL	1	1600	209	.13*	162	.10*		
EBT	2	3200	364	.17	448	.18		
EBR	0	0	180		143			
WBL	2	3200	732	.23	513	.16		
WBT	1	1600	582	.36*	771	. 48		
WBR	1	1600	305	.19	291	.18		
Clear	rance In	terval		.10*		.10		

TOTAL CAPACITY UTILISATION

1.11

.89

			AM PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	29	.02	78	.05
NBT	2	3200	923	.29*	1220	.38
NBR	1	1600	560	.35	792	.50
SBL	1	1600	18	.01*	87	.05
SBT	3	4800	1090	.27	1069	.27
SBR	0	0	186		232	
EBL	1	1600	209	.13*	162	.10
EBT	2	3200	364	.17	448	.18
EBR	0	0	180		143	
WBL	2	3200	732	.23	513	.16
WBT	1	1600	582	.36*	771	.48
WBR	1	1600	305	.19	291	.18
Clear	ance In	terval		.10*		.10

### 3. I-405 & 182nd

			AM P	K HOUR	PN P	K BOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1.5		810	{.25}*	1235	{.39}*
NBT	0	3200	0	.25	0	.39
NBR	0.5		5		11	
SBL	0	0	0		0	
SBT	0	0	0		0	
SBR	0	0	0		0	
EBL	0	0	0		0	
EBT	2	3200	440	.28*	686	.43*
EBR	0	0	443	.28	956	.60
WBL	1	1600	115	.07*	419	.26
WBT	2	3200	710	.22	1024	.32
WBR	0	0	0		0	
Clear	ance Inf	terval		.10*		.10*

TOTAL CAPACITY	UTILIZATION	.70	1.18

			AM P	K HOUR	PH P	K HOUR
	Lanes	CAPACITY	AOT	V/C	VOL	V/C
NBL	1.5		810	{.25}*	1235	(.39)*
NBT	0	3200	0	.25	0	.39
NBR	0.5		5		11	
SBL	0	0	0		0	
SBT	0	0	0		0	
SBR	0	0	0		0	
EBL	0	0	0		0	
EBT	2	3200	440	.28*	686	.43
EBR	0	0	443	.28	974	.61
WBL	1	1600	115	.07*	419	.26
WBT	2	3200	710	.22	1024	.32
WBR	0	0	0		0	

TOTAL CAPACITY UTILIZATION .70 1.	ROTAL C	CAPACITY (	UTILIZATION	.70	1.18
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			AM PK HOUR		PM P	K HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1.5		810	(.25}*	1235	{.39}*
NBT	0	3200	0	.25	0	.39
NBR	0.5		5		11	
SBL	0	0	0		0	
SBT	0	0	0		0	
SBR	0	0	0		0	
KBL.	0	0	0		0	
EBT	2	3200	440	.28*	686	.43*
EBR	0	0	443	.28	989	.62
WBL	1	1600	115	.07*	419	.26
WBT	2	3200	710	.22	1024	.32
WBR	0	0	0		0	

TOTAL CAPACITY UTILIZATION .70 1.18

### 4. Prairie & 190th

			AM PK	BOUR	PH PK	HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	132	.08*	93	.06
MBT	3	4800	1375	. 29	1747	.36*
NBR	1	1600	854	53ء	757	.47
SBL	1	1600	96	.06	102	.06*
SBT	3	4800	1522	.35*	1477	.35
SBR	0	0	158		209	
EBL	1	1600	195	.12	232	.15
EBT	2	3200	1129	.35*	869	.27
EBR	1	1600	91	.06	123	.08
WBL	2	3200	679	.21*	653	.20
WBT	2	3200	827	.28	1113	.374
WBR	0	0	81		58	

TOTAL CAPACITY	UTILIZATION	1.09	1.04

Exist	ing+Proj	ect (Peak	<b>#</b> Workers	3)		
			AN PR	HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	132	*80.	93	.06
NBT	3	4800	1375	.29	1747	.36*
NBR	1	1600	854	.53	757	.47
SBL	1	1600	96	.06	102	.06*
SBT	3	4800	1522	.35*	1477	.35
SBR	0	0	158		209	
EBL	1	1600	195	.12	232	.15*
EBT	2	3200	1131	.35*	869	.27
EBR	1	1600	91	.06	123	.08
WBL	2	3200	679	.21*	653	.20
WBT	2	3200	827	. 28	1115	.37*
WBR	0	0	81		58	
Clear	cance In	terval		.10*		.10
TOTAL	CAPACI	TY UTILISAT	TON	1.09		1.04

			AM PK	HOUR	PM PK	EOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	132	.08*	93	.06
NBT	3	4800	1375	.29	1747	.364
NBR	1	1600	854	.53	757	.47
SBL	1	1600	96	.06	102	.061
SBT	3	4800	1522	.35*	1477	.35
SBR	0	0	158		209	
EBL	1	1600	195	.12	232	.15
EBT	2	3200	1130	.35*	869	.27
EBR	1	1600	91	.06	123	.08
WBL	2	3200	679	.21*	653	.20
WBT	2	3200	827	.28	1114	.37
WBR	0	0	81		58	
Clear	ance In	terval		.10*		.10

### 5. Crenshaw & 190th

Exist	ing					
		am pk hour		HOUR	PM PK HOUR	
	LANES	CAPACITY	VOL	V/C	AOT	V/C
NBL	1	1600	177	.11*	235	.15*
NBT	3	4800	1413	.29	1601	.33
NBR	1	1600	187	.12	146	.09
SBL	1	1600	89	.06	93	.06
SBT	3	4800	1543	.32*	1517	.32*
SBR	1	1600	364	.23	348	.22
EBL	2	3200	357	.11*	405	.13*
EBT	3	4800	1444	.34	1260	.29
EBR	0	0	176		152	
WBL	2	3200	154	.05	156	.05
WBT	2	3200	957	.30*	1276	. 40
WBR	1	1600	54	.03	96	.06
Clear	rance In	terval		.10*		.10

TOTAL CAPACIT	V IPTITIZATION	.94	1.10

			AN PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	AOL	V/C
NBL	1	1600	177	.11*	236	.15
NBT	3	4800	1413	.29	1621	.34
NBR	1	1600	187	.12	146	.09
SBL	1	1600	89	.06	93	.06
SBT	3	4800	1563	.33*	1517	.32
SBR	1	1600	364	.23	348	.22
EBL	2	3200	357	.11*	405	.13
EBT	3	4800	1444	.34	1260	.29
EBR	0	0	177		152	
WBL	2	3200	154	.05	156	.05
WBT	2	3200	957	.30*	1276	.40
WBR	1	1600	54	.03	96	.06
Clear	ance In	terval		.10*		.10

Exist	ing+Proj	ect (Peak	Workers	)		
				AM PK HOUR		HOUR
	Lanes	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	177	.11*	237	.15*
NBT	3	4800	1413	. 29	1639	.34
NBR	1	1600	187	.12	146	.09
SBL	1	1600	89	.06	93	.06
SBT	3	4800	1581	.33*	1517	.32*
SBR	1	1600	364	.23	348	.22
EBL	2	3200	357	.11*	405	.13
EBT	3	4800	1444	.34	1260	.29
EBR	0	0	178		152	
WBL	2	3200	154	.05	156	.05
WBT	2	3200	957	.30*	1276	.40
WBR	1	1600	54	.03	96	.06
Clear	rance In	terval		,10*		.10

TOTAL CAPACITY UTILIZATION

1.10

.95

### 5. Crenshaw & 190th

Rxist	ing					
			AH PK	HOUR	PH PK	HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	177	.11*	235	.15*
NBT	3	4800	1413	.29	1601	.33
NBR	1	1600	187	.12	146	.09
SBL	1	1600	89	.06	93	.06
SBT	3	4800	1543	.32*	1517	.32*
SBR	1	1600	364	.23	348	.22
EBL	2	3200	357	.11*	405	.13*
EBT	3	4800	1444	.34	1260	. 29
EBR	0	0	176		152	
WBL	2	3200	154	.05	156	.05
WBT	2	3200	957	.30*	1 <b>2</b> 76	.404
WBR	1	1600	54	.03	96	06
Clea	rance I	nterval		.10*		.10
TYYFA	I. CAPAC	TY UTILIZA	TTON	.94		1.10

			AM PK	HOUR	PM PK	
	LANES	CAPACITY	VOL	V/C	<b>NOP</b>	V/C
NBL	1	1600	180	.11*	235	.15*
NBT	3	4800	1413	.29	1601	.33
HBR	1	1600	187	.12	146	.09
SBL	1	1600	89	.06	93	.06
SBT	3	4800	1543	.32*	1517	.32*
SBR	1	1600	402	.25	348	.22
EBL	2	3200	357	.11*	443	.14
EBT	3	4800	1444	.34	1313	.31
EBR	0	0	176		155	
WBL	2	3200	154	.05	156	.05
WBT	2	3200	1010	.32*	1276	.40
WBR	1	1600	54	.03	96	.06
Clea	rance In	terval		.10*		.10

			AN PK	HOUR	PN PK	HOUR
	LANES	CAPACITY	AOT	V/C	VOL	V/C
NBL	1	1600	179	.11*	235	.15*
NBT	3	4800	1413	.29	1601	.33
NBR	1	1600	187	.12	146	.09
SBL	1	1600	89	.06	93	.06
SBT	3	4800	1543	.32*	1517	.32
SBR	1	1600	384	.24	348	.22
EBL	2	3200	357	.11*	425	.13
EBT	3	4800	1444	.34	1288	.30
EBR	0	0	176		154	
WBL	2	3200	154	.05	156	.05
WBT	2	3200	985	.31*	1276	. 40
WBR	1	1600	54	.03	96	.06
Clear	ance In	terval		.10≠		.10

### 6. Van Ness & 190th

Exist.						
			AH PK	HOUR	PM PK	HOUR
	LANKS	CAPACITY	AOF	V/C	AOF	V/C
NBL	1	1600	110	.07*	137	.09*
NBT	2	3200	494	.15	717	.22
MBR	1	1600	138	.09	267	.17
SBL	ì	1600	181	.11	101	.06
SBT	2	3200	637	.29*	563	.23*
SBR	0	0	299		171	
EBL	1	1600	137	.09	179	.11
EBT	2	3200	1396	.48*	1655	.57
EBR	Q	0	140		160	
WBL	1	1600	154	.10*	71	.04
WBT	2	3200	765	. 26	1265	.44
WER	0	6	75		142	
Clear	rance In	forma!		.10*		.10

TOTAL CAPACITY	UTILIZATION	1.04	1.03

			AM PK HOUR		PH PK	HOUR
	LANES	CAPACITY	AOP	V/C	AOT	V/C
NBL	1	1600	110	-07*	137	.091
nbt	2	3200	494	.15	717	.22
nbr	1	1600	138	.09	267	.17
SBL	1	1600	181	.11	101	.06
SBT	2	3200	637	-29*	563	.23
SBR	0	0	302		173	
EBL	1	1600	137	.09	182	.11
EBT	2	3200	1396	,48±	1681	.58
KBR	0	0	140		160	
WBL	1	1600	154	.10*	71	.04:
WBT	2	3200	791	.27	1265	.44
WBR	0	0	75		142	

TOTAL CAPACITE UTILIZATION T.U4 1.U4	TOTAL CAPACITY	UTILIZATION	1.04	1.04
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Kristi	ing+Proj	ect (Peak)				
			AN PK	HOUR	PH PK	HOUR
	Lanes	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	110	.07*	137	.09+
nbt	2	3200	494	.15	717	.22
MBR	1	1600	138	.09	267	.17
SBL	1	1600	181	.11	101	.06
SBT	2	3200	637	.29*	563	.23*
SBR	0	0	304		171	
KBL	1	1600	137	.09	184	.12
<b>RBT</b>	2	3200	1396	.48*	1703	,58*
EBR	0	0	140		160	
WEL	1	1600	154	.10*	71	.04×
WBT	2	3200	813	.28	1265	.44
WBR	0	0	75		142	
Clear	ance In	terval		.104		.10#

TOTAL CAPACITY UTILIZATION 1.04 1.04

### 7. Western & 190<sup>th</sup>

Exist	ing					
			an pk	HOUR	PN PK	ROUR
	Lanes	CAPACITY	VOL	₹/C	VOL	V/C
NBL	2	3200	133	.04*	206	.06*
het	3	4800	1040	,22	1287	.27
NBR	1	1600	166	.10	216	.14
SBL	2	3200	130	.04	188	.06
SBT	3	4800	1202	.37*	1146	.32*
SBR	0	0	575		393	
EBL	2	3200	185	.06*	548	.17*
EBT	3	4800	788	.16	1276	.27
EBR	1	1600	459	.29	488	.31
WBL	2	3200	345	.11	265	.08
WBT	3	4800	1110	.24*	897	.23
WBR	0	0	53		185	
Right	Turn A	djustment	EBR	.07*		
Clear	ance In	terval		.10*		.10
most i		TY UTILIZA	·····	.88		.88

				AM PK HOUR		PM PK BOUR	
	LANES	CAPACITY	VOL	V/C	VOL	V/C	
NBL	2	3200	133	.04*	206	.06	
NBT	3	4800	1040	.22	1287	.27	
HBR	1	1600	166	.10	216	.14	
SBL	2	3200	130	•04	188	.06	
SBT	3	4800	1202	.3B*	1146	.32	
SBR	0	0	601		393		
EBL	2	3200	185	•06≉	548	.17	
EBT	3	4800	788	.16	1276	. 27	
EBR	1	1600	459	. 29	488	. 31	
WBL	2	3200	345	.11	265	.08	
WBT	3	4800	1110	.24*	897	. 23	
WBR	0	0	<b>5</b> 3		185		

TOTAL CAPACITY UTILIZATION .89 .88

			AM PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	2	3200	133	.04*	206	.06*
NBT	3	4800	1040	. 22	1287	. 27
NBR	1	1600	166	.10	216	.14
SBL	2	3200	130	.04	188	.06
SBT	3	4800	1202	.38*	1146	.32*
SBR	0	0	623	.39	393	
EBL	2	3200	185	.06*	548	.17
ebt	3	4800	788	.16	1276	. 27
EBR	1	1600	459	. 29	488	.31
WBL	2	3200	345	.11	265	.08
WET	3	4800	1110	.24*	897	.23
WBR	0	0	53		185	

.89

.88

TOTAL CAPACITY UTILIZATION

### 8. Prairie & Del Amo

Exist	ing					
			AM PK	HOUR	PM PK HOUR	
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	270	.17*	166	.10*
NBT	3	4800	1544	.32	1360	.28
NBR	1	1600	38	.02	32	.02
SBL	2	3200	249	.08	288	.09
SBT	3	4800	1195	.25*	1554	.32*
SBR	- 1	1600	387	.24	297	.19
EBL	2	3200	670	.21*	440	.14*
EBT	2	3200	303	.13	230	.13
EBR	0	0	112		179	
WBL	2	3200	17	.01	15	.00
WBT	2	3200	218	.07*	327	.10*
WBR	1	1600	185	.12	359	.22
Right	t Turn A	djustment			WBR	.01*
	rance In			.10*		.10*

TOTAL	CAPACITY	UTILIZATION	.80	.77

			AM PK HOUR		PH PK HOUR	
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	270	.17*	166	.10
NBT	3	4800	1544	.32	1360	.28
NBR	1	1600	38	.02	32	.02
SBL	2	3200	249	.08	288	.09
SBT	3	4800	1195	.25*	1554	.32
SBR	1	1600	387	.24	297	.19
EBL	2	3200	670	.21*	440	.14
EBT	2	3200	303	.13	230	.13
EBR	0	0	112		179	
WBL	2	3200	17	.01	15	.00
WBT	2	3200	218	.07*	327	.10
WBR	1	1600	185	.12	359	.2:
Right	Turn A	] justment			WBR	.03
Clear	ance In	terval		.10*		.10

TOTAL	CAPACIT	Y UTILIZA	TION	.80		.77
Cleara	nce Int	erval		.10*		.10*
Right	Turn Ad	ljustment			WBR	.01*
WBR	1	1600	185	.12	359	.22
WBT	2	3200	218	.07*	327	.10*
WBL	2	3200	17	.01	15	.00
EBR	0	0	112		179	
ebt	2	3200	303	.13	230	.13
EBL	2	3200	670	.21*	440	.14*
SBR	1	1600	387	.24	297	.19
SBT	3	4800	1195	.25*	1554	.32*
SBL	2	3200	249	.08	288	.09
NBR	1	1600	38	.02	32	.02
nbt	3	4800	1544	.32	1360	.28
NBL	1	1600	270	.17*	166	.10*

LANES CAPACITY VOL V/C PH PK HOUR

Existing+Project (Peak #Workers)

### 9. Crenshaw & I-405 SB on/off

Exist	ing					
			AM P	K HOUR	HOUR PM P	
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	479	.30*	472	.29
nbt	3	4800	1510	.31	2272	.47
MBR	0	0	0		0	
SBL	0	0	0		0	
SBT	3	4800	1791	.52*	1720	.42
SBR	0	0	720		304	
EBL	0.5		60		112	
EBT	0	3200	0	{.19}*	0	{.17}
EBR	1.5		912		765	, ,
WBL	0	0	0		0	
WBT	0	0	0		0	
WBR	0	0	0		0	
Ø1	ance Int	1		,10*		.10

TOTAL CAPACITY UTILIZATION	1.11	.98
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			AM P	K HOUR	PM PK HOUR		
	LANES	CAPACITY	AOT	V/C	AOT	V/C	
NBL	1	1600	479	.30*	472	.29	
MBT	3	4800	1510	.31	2292	.48	
NBR	0	0	0		0		
SBL	0	0	0		0		
SBT	3	4800	1791	.52*	1720	.42	
SBR	0	0	720		304		
EBL	0.5		60		112		
EBT	0	3200	0	{.20}*	0	(.17)	
EBR	1.5		930		765	. ,	
WBL	0	0	0		0		
WBT	0	0	0		0		
WBR	0	0	0		0		

TOTAL CAPACITY	UTILITATION	1.12	
TAIND CULUCITY	ATTREBUTION	1116	

.98

Exist	ing+Proj	ject (Peak	#Worker	s)		
	AN PK HOUR			K HOUR	PN P	K HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	479	.30*	472	.29*
NBT	3	4800	1510	.31	2310	.48
NBR	0	0	0		0	
SBL	0	0	0		0	
SBT	3	4800	1791	.52*	1720	.42*
SBR	0	0	720		304	
EBL	0.5		60		112	
<b>KBT</b>	0	3200	0	{.20}*	0	{.17}*
EBR	1.5		945	` .	765	` ,
WBL	0	0	0		0	
WBT	0	0	0		0	
WBR	0	0	0		Ō	
Clear	ance Int	erval		.10*		.10*

1.12

.98

TOTAL CAPACITY UTILIZATION

### 10. Van Hess & Del Amo

			AN PK	HOUR	PN PK	HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	29	.02	85	.05*
KBT	2	3200	663	.24*	706	.26
HBR	0	0	95		125	
SBL	1	1600	48	.03±	59	.04
SBT	2	3200	630	. 24	569	,25*
SBR	0	0	142		221	
EBL	1	1600	233	,15*	208	.13*
EBT	1	1600	269	.17	309	.19
EBR	1	1600	116	.07	34	.02
WBL	1	1600	137	.09	83	.05
WBT	1	1600	251	.22*	290	.23*
WBR	Ō	0	95		73	
Clea	rance In	terval		.10*		.10*

earance Interval	.10*	.10*	Clearance Interval	·10*	
TAL CAPACITY UTILIZATION	.74	.76	TOTAL CAPACITY UTILITATION	.74	

.76

Existing+Project (Peak)

1

2

0

1

1

1

NBL

net

NBR

SBL

SBT

SBR

EBL

EBT

EBR

WBL

WBT

WBR

LANES CAPACITY

1600

3200

0

1600

3200 0

1600

1600

1600

1600

1600

0

AM PK HOUR

VOL

29

663

95

48

630

142

233

269

116

137

251 95

V/C

.02

.24\*

.03\*

.24

.15\*

.17

.07

.09

.22\*

PN PK BOUR V/C

.05\*

. 26

.04

.25\*

.13\*

.19

.02

.05

.23\*

.10\* .76

VOL

85

706

125

59

569

221

208

30<del>9</del>

34

83

290

73

			AN PK HOUR		PH PK	HOUR
	Lanes	CAPACITY	VOL	V/C	NOT	V/C
NBL	1	1600	29	.02	85	.05*
NBT	2	3200	663	.24±	706	.26
NBR	0	0	95		125	
SBL	1	1600	48	.03*	59	-04
SBT	2	3200	630	.24	569	. 25
SBR	0	0	142		221	
BBL	1	1600	233	.15*	208	.13
EBT	1	1600	269	.17	309	.19
KBR	1	1600	116	.07	34	.02
WBL	1	1600	137	.09	83	.05
WBT	1	1600	251	.22*	290	.23
WBR	Ö	0	<b>9</b> 5		73	

.74 TOTAL CAPACITY UTILIZATION

### 11. Western & Del Amo

			AM PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	AOT	V/C	VOL	V/C
NBL	1	1600	116	.07*	67	,04×
NBT	3	4800	1005	.21	985	.21
NBR	0	0	7		23	
SBL	1	1600	49	.03	58	.04
SBT	3	4800	1185	.37*	1425	.36*
SBR	0	0	690	.43	307	
EBL	1	1600	243	.15*	490	.31*
EBT	1	1600	. 23	.01	73	.05
BBR	1	1600	84	.05	114	.07
WBL	0	0	24		26	
WBT	1	1600	112	.13*	20	.051
WBR	0	0	71		40	
Clear	rance In	terval		.10*		.10

			AM PK	HOUR	PM PK	HOUR
	Lanes	CAPACITY	VOL	V/C	VOL	V/C
NEL	1	1600	116	.07*	67	.04*
nbt	3	4800	1005	.21	985	.21
NBR	0	0	7		23	
SBL	1	1600	49	.03	58	.04
SBT	3	4800	1185	.37÷	1425	.36*
SBR	0	0	690	.43	307	
EBL	1	1600	243	,15 <del>t</del>	490	.31*
EBT	1	1600	23	.01	73	.05
ebr	1	1600	84	.05	114	.07
WBL	0	0	24		26	
WET	1	1600	112	.13*	20	.05#
WBR	0	0	71		40	
Clear	rance In	terval		.10*		.10

			AM PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	1	1600	116	.07*	67	.04
NBT	3	4800	1005	.21	985	-21
MBR	0	0	7		23	
SBL	1	1600	49	.03	58	.04
SBT	3	4800	1185	.37*	1425	. 36
SBR	0	0	690	.43	307	
EBL	1	1600	243	.15*	490	.31
EBT	1	1600	23	.01	73	.05
YBR	1	1600	84	.05	114	.07
WEL	0	0	24		26	
WBT	1	1600	112	.13*	20	.05
WER	0	0	71		40	
Clear	ance Int	erval		.10*		.10

12. I-405 SB on/off & 190th

			AN PK	HOUR	PH PK	HOUR
	LANES	CAPACITY	VOL	₹/C	AOF	V/C
NBL	0	0	0		0	
nbt	0	0	0		0	
NBR	0	Đ	0		0	
SBL	1.5		465		535	
SBT	0	3200	0	.20*	0	.18*
SBR	0.5		182		35	
EBL	1	1600	561	.35*	491	.31*
EBT	3	4800	· <b>9</b> 91	.21	1975	,41
EBR	0	0	0		0	
WBL	0	0	0		0	
WBT	2	3200	1277	.40#	1250	.39
WBR	1	1600	191	.12	354	.22
Clear	ance In	terval		.10*		.10

TOTAL CAPACITY	WILLIZATION	1.05	.98

			AM DV	TOUR	DI DE	DADD
	TANDE	CAPACTTY	VOL.	HOUR V/C	PN PK VOL	V/C
	وعاللان	CAFACIII	100	V/C	100	٧,٠
NBL	0	0	0		0	
nbt	0	0	0		0	
NBR	0	0	0		0	
SBL	1.5		465		535	
SBT	0	3200	0	.20*	0	.18
SBR	0.5		182		35	
EBL	1	1600	561	.35*	491	.31
BBT	3	4800	991	.21	1975	.41
EBR	0	0	0		0	
WBL	0	0	0		48	
WBT	2	3200	1325	.41*	1250	.41
WBR	1	1600	191	.12	354	. 22
Clear	rance In	terval		.10*		.10

TOTAL	CAPACITY	UTILIZATION	1.06	1.00
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			AM PR	HOUR	UR PM PK H	
	LANES	CAPACITY	VOL	V/C	VOL	V/C
NBL	0	0	0		0	
NDT	0	0	0		0	
NER	0	0	0		0	
SBL	1.5		465		535	
SBT	0	3200	0	.20×	0	.18
SBR	0.5		182		35	
EBL	1	1600	561	.35*	491	.31
EBT	3	4800	991	.21	1975	.41
EBR	0	0	0		0	
WBL	0	0	0		26	
WBT	2	3200	1303	.41*		.40
WBR	1	1600	191	.12	354	.22

TOTAL CAPACITY UTILIZATION

1.06 .99

### 12. I-405 SB on/off & 190th

Krist	ing					
			AH PK	HOUR	PH PK	HOUR
	LANES	CAPACITY	VOL	V/C	AOF	V/C
NBL	0	0	0		0	
NBT	0	0	0		0	
NBR	0	0	0		0	
SBL	1.5		465		535	
SBT	0	3200	0	.20*	0	.18*
SBR	0.5		182		35	
EBL	1	1600	561	.35*	491	.31*
<b>EBT</b>	3	4800	991	.21	1975	.41
EBR	0	0	0		0	
WBL	0	0	0		0	
WBT	2	3200	1277	.40*	1250	.394
WBR	1	1600	191	.12	354	. 22
Clear	ance In	terval		.10±		.10*
TCBOR.	ותומות	7V IFFILIZAT	TOT	1.05		.98

			an PK	HOUR	PM PK	HOUR
	LANES	CAPACTTY	AOF	V/C	VOL	V/C
NBL	0	0	0		0	
nbt	0	0	0		0	
NBR	0	0	0		0	
SBL	1.5		465		535	
SBT	0	3200	0	.20*	0	.181
SBR	0.5		182		35	
EBL	1	1600	561	.35*	491	.31
EBT	3	4800	991	.21	1975	.41
EBR	0	0	0		0	
WBL	0	0	0		48	
WBT	2	3200	1325	.41*	1250	.41
WBR	1	1600	191	.12	354	. 22
Clear	rance In	terval		.10 <del>4</del>		.10

			AM PK	HOUR	PN PI	HOUR
	Lanes	CAPACITY	VOL		VOL	V/C
NBL	0	0	0		0	
NBT	0	0	0		O.	
NBR	0	0	0		0	
SBL	1.5		465		535	
SBT	0	3200	0	.20±	0	.18
SBR	0.5		182		35	
EBL	1	1600	561	.35*	491	.31
EBT	3	4800	991	.21	1975	.41
EBR	0	0	0		0	
WBL	0	0	0		26	
WBT	2	3200	1303	.41*	1250	.40
WBR	1	1600	191	.12	354	.22

TOTAL CAPACITY UTILIZATION 1.06

.99

### 13. Western & I-405 NB on/off

Exist	ing					
			AM PI	K HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	AOT	V/C
NBL	0	0	12		2	
NBT	2	3200	982	.31*	1431	.45*
NBR	1	1600	314	.20	540	.34
SBL	1	1600	133	.08*	69	.04*
SBT	2	3200	962	.30	924	.29
SBR	0	0	8		1	
EBL	0	0	9	<pre>{.01}*</pre>	0	
EBT	1	1600	0	.01	0	.00
EBR	0	0	7		0	
WBL	1.5		1012		525	
WBT	0	3200	0	.43*	0	.231
WBR	0.5		376		212	
Clear	ance In	terval		.10*		.10

TOTAL	CAPACITY	UTILIZATION	.93	.82
10190	CHECTIT	OTTHIBUTION	173	142

			AM PI	K HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	AOT	V/C
NBL	0	0	12		2	
NBT	2	3200	982	.31*	1431	.45
NBR	1	1600	314	.20	540	.34
SBL	1	1600	133	.08*	69	.04
SBT	2	3200	962	.30	924	. 29
SBR	0	0	8		1	
EBL	0	0	9	<pre>{.01}*</pre>	0	
EBT	1	1600	0	.01	0	.00
EBR	0	0	7		0	
WBL	1.5		1038		525	
WBT	0	3200	0	.44*	0	.23
WBR	0.5		376		212	

TOTAL CAPACITY U	TILIZATION	.94	.82
			***

			AM P	K HOUR	PM PK HOUR	
	Lanes	CAPACITY	VOL	V/C	AOT	V/C
NBL	0	0	12		2	
NBT'	2	3200	982	.31*	1431	.45*
NBR	1	1600	314	.20	540	.34
SBL	1	1600	133	*80.	69	.04*
SBT	2	3200	962	.30	924	.29
SBR	0	0	8		1	
EBL	0	0	9	<pre>{.01}*</pre>	0	
EBT	1	1600	0	.01	0	.00
KBR	0	0	7		0	
WBL	1.5		1060		525	
WBT	0	3200	0	.45*	0	.23
WBR	0.5		376		212	

.82

.95

TOTAL CAPACITY UTILIZATION

### 14. Prairie/Madrona & Torrance

Exist	,					
			AM PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	VOL	V/C	AOT	V/C
NBL	2	3200	162	.05	159	.05*
NBT	3	4800	1034	.26*	1119	.27
NBR	0	0	210		175	
SBL	2	3200	182	.06*	179	.06
SBT	3	4800	1013	.21	1384	.29*
SBR	1	1600	259	.16	248	.16
EBL	2	3200	248	.08	375	.12*
EBT	2	3200	1222	.38*	908	.28
EBR	1	1600	104	.07	223	.14
WBL	2	3200	139	.04*	281	.09
WBT	3	4800	838	.21	1174	. 27
WBR	0	0	150		138	
Clear	rance In	terval		.10*		.10

OZDALENOD INGO			
TOTAL CAPACITY	TEPTI.TEATTON	.84	.83
TATION AND WATER	4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		

			AM PK	HOUR	PN PK	HOUR
	LANES	CAPACITY	VOL	V/C	AOT	V/C
NBL	2	3200	162	.05	159	.05
NBT	3	4800	1034	.26*	1119	.27
NBR	0	0	210		175	
SBL	2	3200	182	.06*	179	.06
SBT	3	4800	1013	.21	1384	.29
SBR	1	1600	259	.16	248	.16
EBL	2	3200	248	.08	375	.12
EBT	2	3200	1222	.38*	908	.28
EBR	1	1600	104	.07	223	.14
WBL	2	3200	139	.04*	281	.09
WBT	3	4800	838	.21	1174	.27
WBR	0	0	150		138	
Clear	ance In	terval		<b>10</b> *		.10

Exist	ing+Proj	ect (Peak	#Workers	)		
			am Pk	HOUR	PM PK	HOUR
	LANES	CAPACITY	AOT	V/C	AOT	V/C
NBL	2	3200	162	.05	159	.05*
NBT	3	4800	1034	. 26*	1119	.27
MBR	0	0	210		175	
SBL	2	3200	182	.06*	179	.06
SBT	3	4800	1013	.21	1384	.29*
SBR	1	1600	259	.16	248	.16
KBL	2	3200	248	.08	375	.12*
EBT	2	3200	1222	.38*	908	.28
EBR	1	1600	104	.07	223	.14
WBL	2	3200	139	.04*	281	.09
WBT	3	4800	838	.21	1174	.27*
WBR	0	0	150		138	
Clear	ance Int	erval		.10*		.10*

TOTAL CAPACITY UTILIZATION

.84

.83

### 15. Crenshaw & Torrance

			AM PK	HOUR	PM PK	HOUR
	LANES	CAPACITY	AOF	V/C	VOL	V/C
IBL	2	3200	193	.06	194	.06*
ΒT	3	4800	1704	.39*	1487	.34
IBR	0	0	158		136	
SBL	2	3200	113	.04*	186	.06
BT	3	4800	1486	.35	1744	.40*
BR	0	0	181		195	
BL	2	3200	250	.08	161	.05
BT	2	3200	1215	.38*	1253	.39*
BR	1	1600	91	.06	150	.09
WBL	2	3200	123	.04*	164	.05*
WBT	2	3200	1037	.32	1151	.36
WBR	1	1600	181	.11	87	.05
Clear	rance In	terval		.10*		.10*
OTAI	CAPACI'	ry otilizat	ION	.95		1.00

TOTAL	CAPACIT	Y DTILIZA	TION	.95		1.00	
Clear	ance Int	erval		.10*		.10*	
WBR	1	1600	181	.11	87	.05	
WBT	2	3200	1037	.32	1151	.36	
WBL	2	3200	123	.04*	164	.05*	
EBR	1	1600	91	.06	150	.09	
ebt	2	3200	1215	.38*	1253	.39*	
EBL	2	3200	250	.08	161	.05	
SBR	0	0	181		195		
SBT	3	4800	1486	.35	1747	.40*	
SBL	2	3200	113	.04*	186	.06	
NBR	0	0	158		136		
NBT	3	4800	1707	.39*	1487	.34	
NBL	2	3200	193	.06	194	.06*	

LANES CAPACITY VOL V/C PM PK HOUR V/C

Existing+Project (Peak #Workers)

				AM PK HOUR		PM PK HOUR	
	LANES	CAPACITY	VOL	V/C	VOL	V/C	
NBL	2	3200	193	.06	194	.06	
NBT	3	4800	1706	.39*	1487	.34	
NBR	0	0	158		136		
SBL	2	3200	113	.04*	186	.06	
SBT	3	4800	1486	.35	1746	.40	
SBR	0	0	181		195		
KBL	2	3200	250	.08	161	.05	
EBT	2	3200	1215	.38*	1253	.39	
EBR	1	1600	91	.06	150	.09	
WBL	2	3200	123	.04*	164	.05	
WBT	2	3200	1037	.32	1151	.36	
WBR	1	1600	181	.11	87	.05	
Clear	ance In	terval		.10*		.10	